

3. 일광터널 안전성평가 자료

3.1 안전성평가 자료

구조물의 안전성 평가는 그 기능과 역할을 유지할 수 있는 구조적 및 사용상의 안전성에 대한 확보여부를 평가하는 것이므로 설계도서 검토 및 시공방법과 사용재료에 대한 검토, 부재별 상태 평가 결과 및 각종 계측·측정·조사·시험 등을 통한 충분한 기초자료를 확보하여 이를 바탕으로 수치해석에 의해 안전성 여부를 판단하여야 한다.

상태평가 결과 및 각종 계측·측정·조사·시험 등을 실시한 결과, 전회(2019년) 정밀안전진단과 해당 구조물의 현황이 이전과 근소한 차이 외 변화가 없는 것으로 확인되어 구조계산서 및 터널해석보고서 등 기초 자료를 활용하여 안전성여부를 판단하였고, 일부 자료를 발췌하여 첨부하였다.

I. 개작식 터널

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1. 설계조건

1. 1 일반사항

- 1) 형식 : Precast Arch Box 13.450 m * 5.429 m
지 간 : L = 13.450 m
총 연 장 : 140 m
토 피 고 : 3.000 m
지하수위 : 1.000 m
사각(skew) : 90 °
기초형식 : 전면기초

2) 사용재료 및 설계기준강도

① 콘크리트

- 본체 Precast Arch Box
 $f_{ck} = 400 \text{ kgf/cm}^2$
 $E_c = 10,500 * \sqrt{f_{ck}} + 70,000 = 280,000 \text{ kgf/cm}^2$
- 기초 : 현장타설
 $f_{ck} = 270 \text{ kgf/cm}^2$
 $E_c = 15,000 * \sqrt{f_{ck}} = 246,475 \text{ kgf/cm}^2$

② 철근

- * 본체 · Precast Arch Box
 $f_y = 4000 \text{ kgf/cm}^2$ (Deformed Steel : 이형 철근)
 $E_s = 2000000 \text{ kgf/cm}^2$
- * 기초 · 현 장 타 설
 $f_y = 4000 \text{ kgf/cm}^2$ (Deformed Steel : 이형 철근)
 $E_s = 2000000 \text{ kgf/cm}^2$

3) 설 계 방 법

① P.A.B 본체 및 현장 타설 기초

- * 단 면 검 토 : 극한 강도 설계법
- * 사용성 검토 : 허용 응력 설계법
a) 처짐 검토
b) 균열 검토
c) 피로 응력 검토

② 배력근 (온도 철근) 규정

A. 도로교설계기준 4.7 바닥판 적용시.

4.7.5.7 배력철근

1) 주철근이 차량진행방향에 직각인 경우 (본 구조물의 기초 슬래브에 해당)

$$\text{백분율} = \frac{120}{\sqrt{L}} \quad \text{과 } 67\% \text{ 중 작은 값 이상}$$

$$= 120 / \sqrt{15.25} = 30.7 \% \quad (L = 30.5 / 2 = 15.25 \text{ m})$$

$$= \text{MIN}(30.7\%, 67\%) = 30.7\% \text{ 이므로 } A_{s, \text{req}} * 0.307 \text{을 배근함.}$$

단, 온도철근 이상으로 배근함.

B. P.A.B 본체의 수축 및 온도 철근 (콘크리트 구조 설계 기준(1999) - 5.7 p103)

$$\text{철근비 } \rho = 0.0020$$

$$\rho = \frac{A_s}{b * d} \text{ 에서, } \quad \begin{array}{ll} b = & 100 \text{ cm} \\ d = & 50 \text{ cm} \end{array}$$

$$A_s = \rho * b * d = 0.0020 * 100 * 50 \\ = 10.00 \text{ cm}^2/\text{m} \text{ 이상으로 하여야 한다.}$$

수축 및 온도철근 간격은 슬래브 두께의 5배 이하 40cm이하로 하여야 한다.

C. 현장 타설 벽체의 최소수평철근비 (콘크리트 구조 설계 기준(1999) - 11.3 p221)

$$\text{철근비 } \rho = 0.002$$

$$\rho = \frac{A_s}{b * d} \text{ 에서, } \quad \begin{array}{ll} b = & 100 \text{ cm} \\ d = & 85 \text{ cm} \end{array}$$

$$A_s = \rho * b * d = 0.0020 * 100 * 85 \\ = 17.00 \text{ cm}^2/\text{m} \text{ 이상으로 하여야 한다.}$$

철근 배근 간격은 벽두께의 3배 이하, 40cm이하로 하여야 한다.

4) P.A.B 철근 덮개 기준 규정

: 콘크리트 구조 설계기준 5.4.2 프리캐스트 콘크리트 규정 참조

1.2 하중 조건

1) 고정 하중

- ① 철근 $\text{Con}'c$: 2.50 t/m'
- ② 토피 흙 : 1.90 t/m'
- ③ γ_{sub} : 0.90 t/m'

2) 활하중 (한국 도로공사 교량 설계 기준 VI. 설계 일반사항 참조)

지중 RC RAHMEN교의 노면 활하중 적용

재하 방법

① 충격계수

토피두께 D(m)	충격계수 (i)
$0.15 \leq D \leq 1$	0.30
$1 < D < 2$	0.20
$2 < D < 3$	0.10
$3 < D$	0.00

② 노면 활하중 (P_{vl})

노면 활하중 P_{vl} 은 라멘을 단순보로 가정하여 활하중이 라멘 전폭에 작용한 경우와 $2D + 0.2$ m의 분포폭에 재하되는 경우와 모멘트가 같다고 보아 등가 등분포 활하중 P_{vl} 을 산출한 값임.

③ 활하중 영향 범위

활하중 분포폭이 라멘 전폭(B0)을 초과하는 부분의 활하중 영향은 무시.

④ 전륜하중 영향 범위

전륜하중은 무시하고 후륜하중에 대해서만 고려.

3) 토질 조건

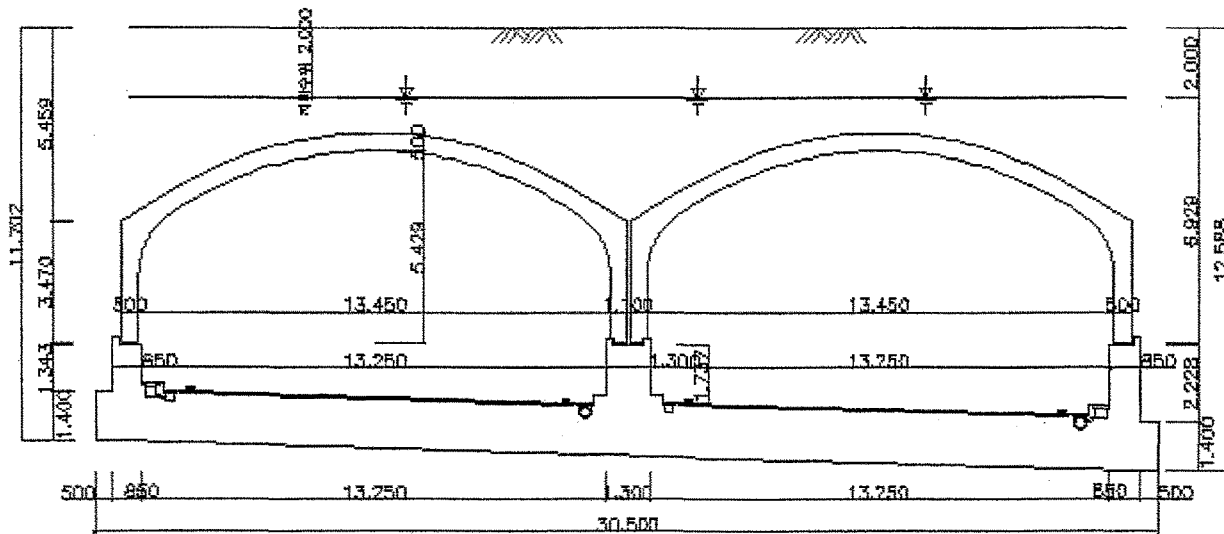
- 흙 내부 마찰각 $\phi = 30^\circ$
- 정지 토압 계수 $K_0 = 1 - \sin\phi = 0.500$
- 뒷채움, 토피 흙 $\gamma_s = 1.9$ t/m'

1.3 참고 문헌

- ↳ 도로교 설계 기준 (2000) - 건설 교통부
- ↳ 콘크리트구조설계기준(1999)-건설교통부
- ↳ 콘크리트 표준 시방서 (1999) - 건설 교통부
- ↳ 고속도로 암거 표준도 설계 기준 (1999) - 한국 도로 공사
- ↳ AASHTO (16th Edition, 1996)
- ↳ 한국도로공사 설계 실무 자료집

2. 단면 가정

1) 설계 단면



P.A.B 본체 제원		기초 구조물 제원	
P.A.B Span	13.450 m	외측 P/W 두께	0.850 m
P.A.B 높이	5.429 m	중앙부 P/W 두께	1.300 m
토피고	3.000 m	기초내측거리	13.250 m
H.W.L	1.000 m	기초 두께	1.400 m
벽체 두께	0.500 m	기초 전폭	30.500 m
슬래브 두께	0.500 m	외측 P/W 높이	2.228 m
$f_{ck} =$	400 kg/cm ²	중앙부 P/W 높이	1.737 m
$f_y =$	4000 kg/cm ²	$f_{ck} =$	270 kg/cm ²
1 Seg. 길이	1.500 m	$f_y =$	4000 kg/cm ²

2) 단면특성

P.A.B 본체	부재 번호	단면적(A) (m ²)				단면2차모멘트(I) (m ⁴)				단면두께 (m)		
	1	1.0	*	0.500	= 0.500	1 / 12	*	1.0	*	0.500 ³	= 0.010	0.500
	2	1.0	*	0.500	= 0.500	1 / 12	*	1.0	*	0.500 ³	= 0.010	0.500
	3	1.0	*	0.500	= 0.500	1 / 12	*	1.0	*	0.500 ³	= 0.010	0.500
	4	1.0	*	0.500	= 0.500	1 / 12	*	1.0	*	0.500 ³	= 0.010	0.500
	5	1.0	*	0.542	= 0.542	1 / 12	*	1.0	*	0.542 ³	= 0.013	0.542
	6	1.0	*	0.675	= 0.675	1 / 12	*	1.0	*	0.675 ³	= 0.026	0.675
	7	1.0	*	0.916	= 0.916	1 / 12	*	1.0	*	0.916 ³	= 0.064	0.916
	8	1.0	*	0.680	= 0.680	1 / 12	*	1.0	*	0.680 ³	= 0.026	0.680
	9	1.0	*	0.553	= 0.553	1 / 12	*	1.0	*	0.553 ³	= 0.014	0.553
	10	1.0	*	0.511	= 0.511	1 / 12	*	1.0	*	0.511 ³	= 0.011	0.511
	11	1.0	*	0.500	= 0.500	1 / 12	*	1.0	*	0.500 ³	= 0.010	0.500
	12	1.0	*	0.500	= 0.500	1 / 12	*	1.0	*	0.500 ³	= 0.010	0.500
	13	1.0	*	0.500	= 0.500	1 / 12	*	1.0	*	0.500 ³	= 0.010	0.500
	14	1.0	*	0.500	= 0.500	1 / 12	*	1.0	*	0.500 ³	= 0.010	0.500
	15	1.0	*	0.500	= 0.500	1 / 12	*	1.0	*	0.500 ³	= 0.010	0.500
	16	1.0	*	0.500	= 0.500	1 / 12	*	1.0	*	0.500 ³	= 0.010	0.500
	17	1.0	*	0.500	= 0.500	1 / 12	*	1.0	*	0.500 ³	= 0.010	0.500
	18	1.0	*	0.511	= 0.511	1 / 12	*	1.0	*	0.511 ³	= 0.011	0.511
	19	1.0	*	0.553	= 0.553	1 / 12	*	1.0	*	0.553 ³	= 0.014	0.553
	20	1.0	*	0.680	= 0.680	1 / 12	*	1.0	*	0.680 ³	= 0.026	0.680
	21	1.0	*	0.916	= 0.916	1 / 12	*	1.0	*	0.916 ³	= 0.064	0.916
	22	1.0	*	0.675	= 0.675	1 / 12	*	1.0	*	0.675 ³	= 0.026	0.675
	23	1.0	*	0.542	= 0.542	1 / 12	*	1.0	*	0.542 ³	= 0.013	0.542
	24	1.0	*	0.500	= 0.500	1 / 12	*	1.0	*	0.500 ³	= 0.010	0.500
	25	1.0	*	0.500	= 0.500	1 / 12	*	1.0	*	0.500 ³	= 0.010	0.500
	26	1.0	*	0.500	= 0.500	1 / 12	*	1.0	*	0.500 ³	= 0.010	0.500
	27	1.0	*	0.500	= 0.500	1 / 12	*	1.0	*	0.500 ³	= 0.010	0.500

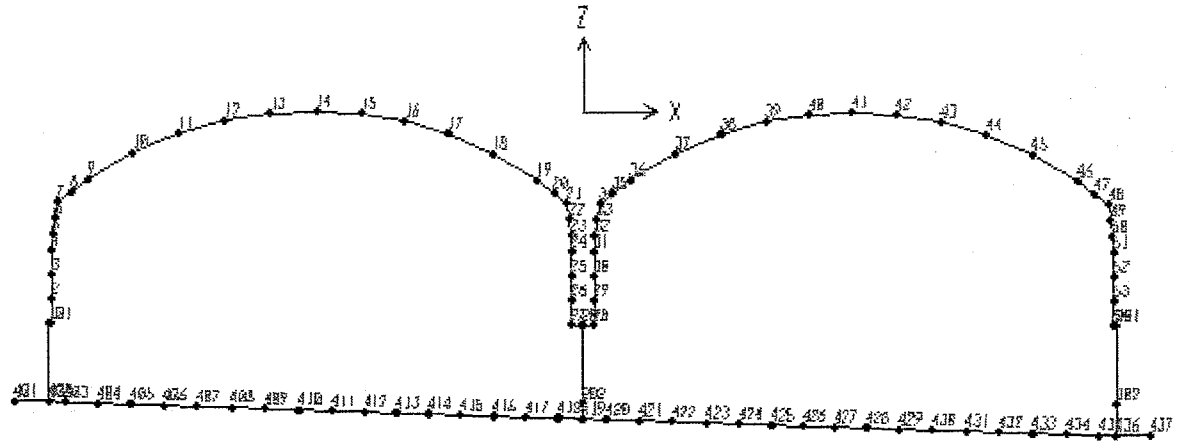
부재	101	1.0	*	0.850	= 0.850	1 / 12	*	1.0	* 0.850 ³	= 0.051	0.850
	102	1.0	*	0.850	= 0.850	1 / 12	*	1.0	* 0.850 ³	= 0.051	0.850
	201	1.0	*	1.300	= 1.300	1 / 12	*	1.0	* 1.300 ³	= 0.183	1.300
	202	1.0	*	1.300	= 1.300	1 / 12	*	1.0	* 1.300 ³	= 0.183	1.300

기초슬래브	401	1.0	*	1.400	= 1.400	1 / 12	*	1.0	* 1.400 ³	= 0.229	1.400
	402	1.0	*	1.400	= 1.400	1 / 12	*	1.0	* 1.400 ³	= 0.229	1.400
	403	1.0	*	1.400	= 1.400	1 / 12	*	1.0	* 1.400 ³	= 0.229	1.400
	404	1.0	*	1.400	= 1.400	1 / 12	*	1.0	* 1.400 ³	= 0.229	1.400
	405	1.0	*	1.400	= 1.400	1 / 12	*	1.0	* 1.400 ³	= 0.229	1.400
	406	1.0	*	1.400	= 1.400	1 / 12	*	1.0	* 1.400 ³	= 0.229	1.400
	407	1.0	*	1.400	= 1.400	1 / 12	*	1.0	* 1.400 ³	= 0.229	1.400
	408	1.0	*	1.400	= 1.400	1 / 12	*	1.0	* 1.400 ³	= 0.229	1.400
	409	1.0	*	1.400	= 1.400	1 / 12	*	1.0	* 1.400 ³	= 0.229	1.400
	410	1.0	*	1.400	= 1.400	1 / 12	*	1.0	* 1.400 ³	= 0.229	1.400
	411	1.0	*	1.400	= 1.400	1 / 12	*	1.0	* 1.400 ³	= 0.229	1.400
	412	1.0	*	1.400	= 1.400	1 / 12	*	1.0	* 1.400 ³	= 0.229	1.400
	413	1.0	*	1.400	= 1.400	1 / 12	*	1.0	* 1.400 ³	= 0.229	1.400
	414	1.0	*	1.400	= 1.400	1 / 12	*	1.0	* 1.400 ³	= 0.229	1.400
	415	1.0	*	1.400	= 1.400	1 / 12	*	1.0	* 1.400 ³	= 0.229	1.400
	416	1.0	*	1.400	= 1.400	1 / 12	*	1.0	* 1.400 ³	= 0.229	1.400
	417	1.0	*	1.400	= 1.400	1 / 12	*	1.0	* 1.400 ³	= 0.229	1.400
	418	1.0	*	1.400	= 1.400	1 / 12	*	1.0	* 1.400 ³	= 0.229	1.400

3. 상시해석

3.1 해석 모델링

1) P.A.B 단면 모델링



2) 절점좌표

절점	X	Z	절점	X	Z	절점	X	Z	절점	X	Z
1	-14.250	-5.679	25	-0.300	-4.372	49	14.166	-2.860	413	-5.067	-8.042
2	-14.250	-5.026	26	-0.300	-5.026	50	14.230	-3.293	414	-4.184	-8.069
3	-14.250	-4.372	27	-0.300	-5.679	51	14.250	-3.719	415	-3.300	-8.098
4	-14.250	-3.719	28	0.300	-5.679	52	14.250	-4.372	416	-2.417	-8.122
5	-14.230	-3.293	29	0.300	-5.026	53	14.250	-5.026	417	-1.534	-8.148
6	-14.166	-2.860	30	0.300	-4.372	54	14.250	-5.679	418	-0.650	-8.175
7	-14.107	-2.444	31	0.300	-3.719	101	-14.325	-5.679	419	0.000	-8.194
8	-13.748	-2.165	32	0.318	-3.293	102	-14.325	-7.052	420	0.650	-8.214
9	-13.294	-1.832	33	0.369	-2.860	201	0.000	-5.679	421	1.534	-8.241
10	-12.092	-1.131	34	0.443	-2.444	202	0.000	-7.475	422	2.417	-8.267
11	-10.887	-0.608	35	0.795	-2.165	301	14.325	-5.679	423	3.300	-8.291
12	-9.683	-0.256	36	1.256	-1.832	302	14.325	-7.938	424	4.184	-8.320
13	-8.479	-0.057	37	2.458	-1.131	401	-15.250	-7.764	425	5.067	-8.347
14	-7.275	0.000	38	3.663	-0.608	402	-14.325	-7.764	426	5.950	-8.373
15	-6.071	-0.057	39	4.867	-0.256	403	-13.900	-7.777	427	6.834	-8.400
16	-4.867	-0.256	40	6.071	-0.057	404	-13.017	-7.804	428	7.717	-8.426
17	-3.663	-0.608	41	7.275	0.000	405	-12.133	-7.830	429	8.600	-8.453
18	-2.458	-1.131	42	8.479	-0.057	406	-11.250	-7.857	430	9.484	-8.479
19	-1.256	-1.832	43	9.683	-0.256	407	-10.367	-7.883	431	10.367	-8.506
20	-0.795	-2.165	44	10.887	-0.608	408	-9.484	-7.910	432	11.250	-8.532
21	-0.443	-2.444	45	12.092	-1.131	409	-8.600	-7.936	433	12.133	-8.559
22	-0.369	-2.860	46	13.294	-1.832	410	-7.717	-7.963	434	13.017	-8.585
23	-0.318	-3.293	47	13.748	-2.165	411	-6.834	-7.989	435	13.900	-8.612
24	-0.300	-3.719	48	14.107	-2.444	412	-5.950	-8.016	436	14.325	-8.625
									437	15.250	-8.625

3) SPRING 계수

$$BV = \sqrt{Av} = \sqrt{1500 \times 3050} = 2138.925 \text{ cm} \quad \left\{ \begin{array}{l} \text{신축이음거리 : 1500 cm} \\ \text{기초전폭:3050 cm} \end{array} \right.$$

$$Kv = Kvo \times (Bv / 30)^{-3/4}$$

여기서,

Kv = 연직방향 지반 반력 계수 (kgf/cm^2)

Kvo = 지름 30cm 의 강체윤판에 의한 평판재하 시험에 상당하는 연직 방향 지반반력 계수(kgf/cm^2)

Bv = 기초의 환산재하 폭 (m)

$Eo = 80,000 \text{ kgf/cm}^2$

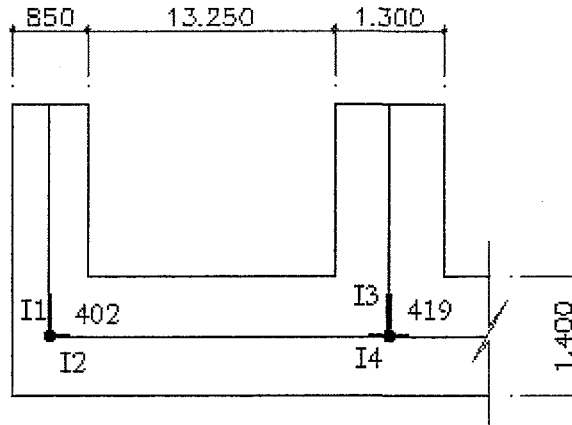
$\alpha = 4.0$ (지반반력 추정계수)

$$Kv = 1/30 \times 4 \times 80000 \times (2138.925/30)^{-3/4} = 434.7334 \text{ kgf/cm}^2 \\ = 434733.4 \text{ t/m}^2$$

절점	분담폭	스프링계수
401	0.463	201064.2
402	0.675	293445.0
403	0.654	284315.6
404	0.884	384087.0
405	0.884	384087.0
406	0.883	383869.6
407	0.883	383869.6
408	0.884	384087.0
409	0.884	384087.0
410	0.883	383869.6
411	0.884	384087.0
412	0.884	384087.0
413	0.883	383869.6
414	0.884	384087.0
415	0.884	384087.0
416	0.883	383869.6
417	0.884	384087.0
418	0.767	333440.5
419	0.650	282576.7

수평 지반 반력 계수 : $Kh = 10000 \text{ ton/m}^2$

4) 기초 슬래브 절점부 강역 (도로교 설계 기준 (2000) ,라멘교 P377)



$$I1 = 0.700 - 0.25 \times 0.85 = 0.4875 \text{ m}$$

$$I2 = 0.425 - 0.25 \times 1.40 = 0.075 \text{ m}$$

$$I3 = 0.700 - 0.25 \times 1.30 = 0.375 \text{ m}$$

$$I4 = 0.650 - 0.25 \times 1.40 = 0.3 \text{ m}$$

3.2 하중의 산정

1) 구조물 자중 산정

구조해석 입력값(SAP2000 input file) 참조

2) 상부에 작용하는 활하중

- * 활하중은 작용하지 않으므로 고려하지 않음.
- * 단 가설시 하중으로 활하중을 고려하여 적용함.
- 안전측 검토를 위해 가설하중에 의한 수평 토압은 고려하지 않음.

① 부분 등분포 하중 작용시

토피고 $D = 1.0 \text{ m}$

충격계수 $I = 0.3 \text{ (} 0.15 \leq D \leq 1 \text{)}$

$B0 = 14.45 \text{ m}$

$W = (2D + 0.2 + 4 - 2D + D + 0.1) \times 2$

$= (2 \times 1 + 0.2 + 4 - 2 \times 1 + 1 + 0.1) \times 2 = 10.6 \text{ m}$

그러므로, $B0 > W$ 일 경우

종방향 단위 길이당 하중(DB-18)

$P1 = (2 \times 7.2) / 3.0 = 4.8 \text{ tonf/m}$

전쪽에 작용하는 노면활하중

$$PvI = \frac{8 \times P1 (1 + I) (0.75 B0 - 0.25D - 4.225)}{B0^2}$$

$$= \frac{8 \times 4.8 (1 + 0.3) (0.75 \times 14.45 - 0.25 \times 1.0 - 4.225)}{14.45^2} = 1.521$$

㉠ 연직 토압 + 활하중

$$= 2.0 \times 1.0 \times 1.5 + 1.521 \times 2.15 = 6.27 \text{ t/m}$$

② 등분포 하중 작용시

토피고 $D = 3.0 \text{ m}$

충격계수 $I = 0.1 \quad (2.0 \leq D \leq 3.0)$

$B_0 = 14.45 \text{ m}$

$$W = (4.2 + 2D - 4 + 4.1 - D) \times 2 \\ = (4.20 + 2 \times 3.0 - 4 + 4.1 - 3) \times 2 = 14.6 \text{ m}$$

그러므로, $B_0 < W$ 일 경우

종방향 단위 길이당 하중 (DB-18)

$$P_1 = (2 \times 7.2) / 3.0 = 4.8 \text{ tonf/m}$$

분포폭당 작용하는 하중 (접지폭 0.2m , 분포각 45°)

$$P_{v1} = \{P_1(1+I)\} / (2D+0.2) = \{4.8 \times (1+0.1)\} / (2 \times 3 + 0.2) = 0.852$$

$$P_{v2} = \{2P_1(1+I)\} / (2D+0.2) = \{2 \times 4.8 \times (1+0.1)\} / (2 \times 3 + 0.2) = 1.703$$

전폭(B_0)에 작용하는 노면 노면 활하중

$$P_{vl} = \frac{8 \times P_{v1} \{0.125 B_0^2 + 2 \times B_0 - 8.4 - (B_0 - 4.2)D\}}{B_0^2} \\ + \frac{8 \times P_{v2} \{8.4 - 2 B_0 + (B_0 - 4.2)D\}}{B_0^2} \\ = \frac{0.852 \{0.125 \times 14.45^2 + 2 \times 14.45 - 8.4 - (14.45 - 4.2) \times 3\}}{14.45^2} \\ + \frac{8 \times 1.703 \times \{8.4 - 2 \times 14.45 + (14.45 - 4.2) \times 3.0\}}{14.45^2} \\ = \frac{108.036 + 139.646}{208.803} = 1.186$$

⊙ 연직 토압 + 활하중

$$= 2.0 \times 3.0 \times 1.5 + 1.186 \times 2.15 = 11.55 \text{ t/m}$$

■ 비교 결과

$11.55 \text{ t/m} > 6.27 \text{ t/m}$ 이므로,

토피고 3.00m 의 경우가 더 불리한 경우 이므로 가설시 활하중은 토피고 3m 일 때를 고려하여 $P_{vl} = 1.186 \text{ t/m}^2$ 을 적용함.

$$* P_{vl} = 1.186 \text{ t/m}^2 \quad (\text{P.A.B 슬래브에 재하})$$

3) 연직토압(Pv) - 지하수 없을때

$$P_v = \alpha * \gamma * D$$

γ : 상재토의 단위중량(t/m^3)

D : 암거상면의 토피 및 포장층 두께(m)

B_0 : 암거 외측 폭(m)

* 흙의 자중 및 연직토압

근입계수(α) : 암거 근입 특성에 따른 계수

$$\alpha = 1.0 + 0.2(D / B_0) \leq 1.15$$

$$= 1.0 + 0.2 * (3 / (13.45 + 0.5 * 2)) = 1.042 \leq 1.15 \quad \alpha = 1.042$$

절점 번호		$\gamma * D$ t/m^2	$P_v = \alpha * \gamma * D$ t/m^2
5	23	1.9 * 6.293 = 11.957	1.042 * 11.957 = 12.459
6	22	1.9 * 5.860 = 11.134	1.042 * 11.134 = 11.602
7	21	1.9 * 5.444 = 10.344	1.042 * 10.344 = 10.778
8	20	1.9 * 5.165 = 9.814	1.042 * 9.814 = 10.226
9	19	1.9 * 4.832 = 9.181	1.042 * 9.181 = 9.566
10	18	1.9 * 4.131 = 7.849	1.042 * 7.849 = 8.179
11	17	1.9 * 3.608 = 6.855	1.042 * 6.855 = 7.143
12	16	1.9 * 3.256 = 6.186	1.042 * 6.186 = 6.446
13	15	1.9 * 3.057 = 5.808	1.042 * 5.808 = 6.052
14	-	1.9 * 3.000 = 5.700	1.042 * 5.700 = 5.939

4) 연직토압 (Pvw) - 지하수 있을때

$$P_v = \alpha * \gamma * D$$

$$\alpha = 1.042$$

$$\gamma_{\text{t}} = 1.9 \quad t/m^3$$

$$\gamma_{\text{sub}} = 0.9 \quad t/m^3$$

절점 번호	지하수위	지하수 아래	α	$\sum P_{vw}$	
5	23	3.80	3.864	1.042	7.986
6	22	3.80	3.474	1.042	7.580
7	21	3.80	3.100	1.042	7.189
8	20	3.80	2.849	1.042	6.928
9	19	3.80	2.549	1.042	6.615
10	18	3.80	1.918	1.042	5.958
11	17	3.80	1.447	1.042	5.468
12	16	3.80	1.130	1.042	5.137
13	15	3.80	0.951	1.042	4.951
14	-	3.80	0.900	1.042	4.897

ex) 5 번 절점

$$\text{지하수 위} : \gamma * h = 1.9 * 2.0 = 3.8$$

$$\text{지하수 아래} : \gamma * h = 0.9 * (3.293 + 1.0) = 3.864$$

$$P_{vw} = 1.042 * (3.8 + 3.864) = 7.986$$

5) 수평토압(Ph) - 지하수 없을때

절점 번호		수평토압 t/m ²				
1	27	0.500	*	1.9	*	8.929 = 8.483
2	26	0.500	*	1.9	*	8.276 = 7.862
3	25	0.500	*	1.9	*	7.622 = 7.241
4	24	0.500	*	1.9	*	6.969 = 6.621
5	23	0.500	*	1.9	*	6.543 = 6.216
6	22	0.500	*	1.9	*	6.110 = 5.805
7	21	0.500	*	1.9	*	5.694 = 5.409
8	20	0.500	*	1.9	*	5.415 = 5.144
9	19	0.500	*	1.9	*	5.082 = 4.828
10	18	0.500	*	1.9	*	4.381 = 4.162
11	17	0.500	*	1.9	*	3.858 = 3.665
12	16	0.500	*	1.9	*	3.506 = 3.331
13	15	0.500	*	1.9	*	3.307 = 3.142
14		0.500	*	1.9	*	3.250 = 3.088
101		0.500	*	1.9	*	8.929 = 8.483
102		0.500	*	1.9	*	10.302 = 9.787
401		0.500	*	1.9	*	11.014 = 10.463
301		0.500	*	1.9	*	8.929 = 8.483
302		0.500	*	1.9	*	11.188 = 10.629
437		0.500	*	1.9	*	11.875 = 11.281

ex) 1 번 절점

$$K_o * \gamma * (h_1 + h_2 + t/2) = 0.5 * 1.9 * (5.679 + 3.0 + 0.5/2) = 8.483$$

h₁ : 1번절점 z축좌표 (5.679 m), h₂ : 토피고 (3.0 m), t : PAB 슬래브 두께 (0.5 m)

6) 수평토압(Phw) - 지하수 있을때

절점 번호	지하수 위	지하수 아래	Σ Phw
1 27	1.900	3.118	5.018
2 26	1.900	2.824	4.724
3 25	1.900	2.530	4.430
4 24	1.900	2.236	4.136
5 23	1.900	2.044	3.944
6 22	1.900	1.850	3.750
7 21	1.900	1.662	3.562
8 20	1.900	1.537	3.437
9 19	1.900	1.387	3.287
10 18	1.900	1.071	2.971
11 17	1.900	0.836	2.736
12 16	1.900	0.678	2.578
13 15	1.900	0.588	2.488
14 14	1.900	0.563	2.463
101	1.900	3.118	5.018
102	1.900	3.736	5.636
401	1.900	4.056	5.956
301	1.900	3.118	5.018
302	1.900	4.135	6.035
435	1.900	4.444	6.344

ex) 1 번 절점

$$\text{지하수 위} : K_o * \gamma * h = 0.5 * 1.9 * 2.0 = 1.90$$

$$\text{지하수 아래} : K_o * \gamma * (h_1 + h_2 + t/2) =$$

$$0.5 * 0.9 * (5.679 + 1 + 0.5/2) = 3.118$$

h₁ : 1번절점 z축좌표 (5.679 m)

h₂ : 구조물 상단에서의 지하수위 (1.0 m)

t : PAB 슬래브 두께 (0.5 m)

7) 수압 (Pw) (GL - 2.0 m)

① 상판과 측벽에 작용하는 수압

절점 번호	지하수위
1 27	6.929
2 26	6.276
3 25	5.622
4 24	4.969
5 23	4.543
6 22	4.110
7 21	3.694
8 20	3.415
9 19	3.082
10 18	2.381
11 17	1.858
12 16	1.506
13 15	1.307
14	1.250
101	6.929
102	8.302
401	9.014
301	6.929
302	9.188
435	9.875

ex) 1 번 절점

$$P_w = \gamma * (h_1 + h_2 + t/2) = 1.0 * (5.679 + 1.0 + 0.5/2) = 6.929$$

h1 : 1번절점 z축좌표 (5.679 m)

h2 : 구조물 상단에서의 지하수위 (1.0 m)

t : PAB 슬래브 두께 (0.5 m)

② 기초 슬래브 저판에 작용하는 수압

절점	$\gamma w * H$	절점	$\gamma w * H$
401	9.714	420	10.164
402	9.714	421	10.191
403	9.727	422	10.217
404	9.754	423	10.241
405	9.780	424	10.270
406	9.807	425	10.297
407	9.833	426	10.323
408	9.860	427	10.350
409	9.886	428	10.376
410	9.913	429	10.403
411	9.939	430	10.429
412	9.966	431	10.456
413	9.992	432	10.482
414	10.019	433	10.509
415	10.048	434	10.535
416	10.072	435	10.562
417	10.098	436	10.575
418	10.125	437	10.575
419	10.144		

$$H = \text{각절점의 Z축좌표} + \text{기초두께}(1.4)/2 + \text{PAB두께}(0.5)/2 + \text{HWL}(1.0)$$

8) 기초 슬래브에 작용하는 활하중 (PL)

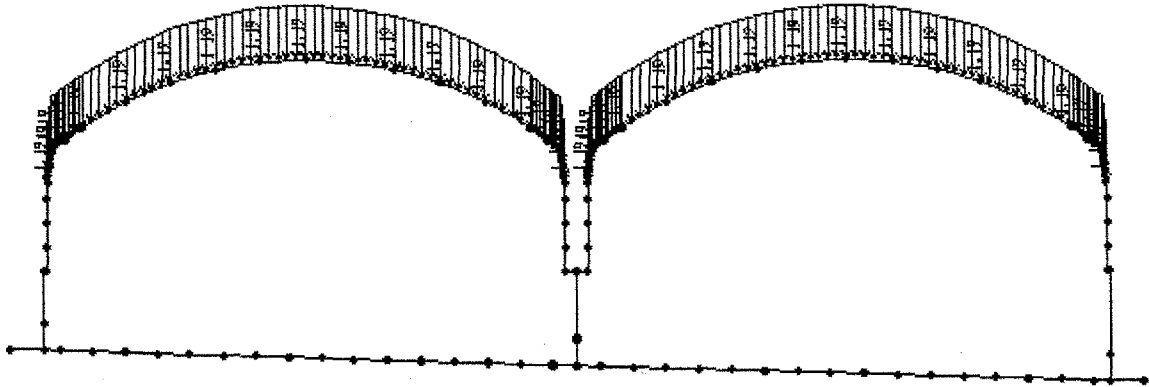
: 기초 슬래브에 작용하는 차량하중은 기초 부모멘트를 감소시키므로 설계시에는 고려할 필요가 없고 지지력 계산시에만 고려한다. 그러므로 재하 하중은 접지면의 분담폭을 고려할 필요 없이 9.6 ton을 그대로 사용한다.

3.3 하중재하

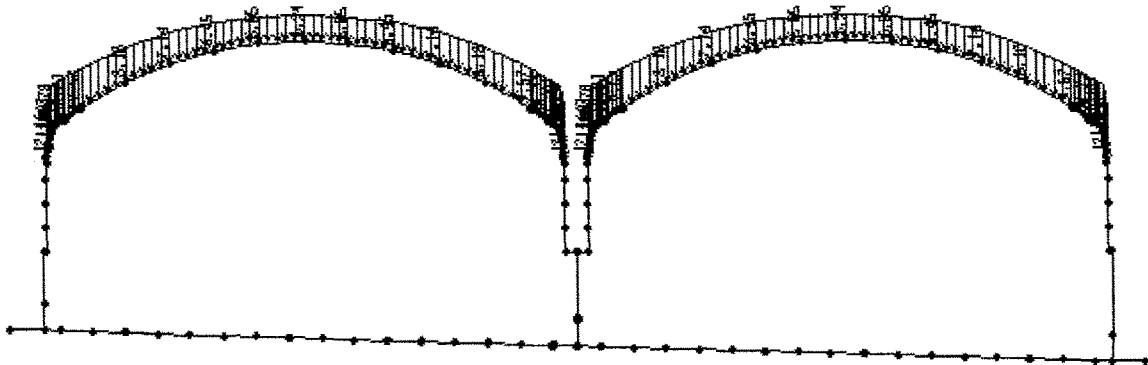
1) 구조물 자중

구조해석 PROGRAM내에 포함.

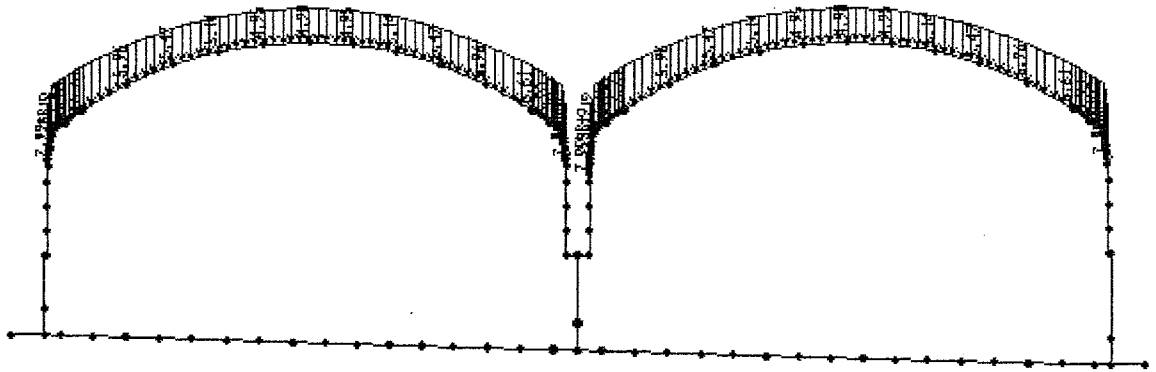
2) 상부에 작용하는 활하중 (가설 활하중 PVL)



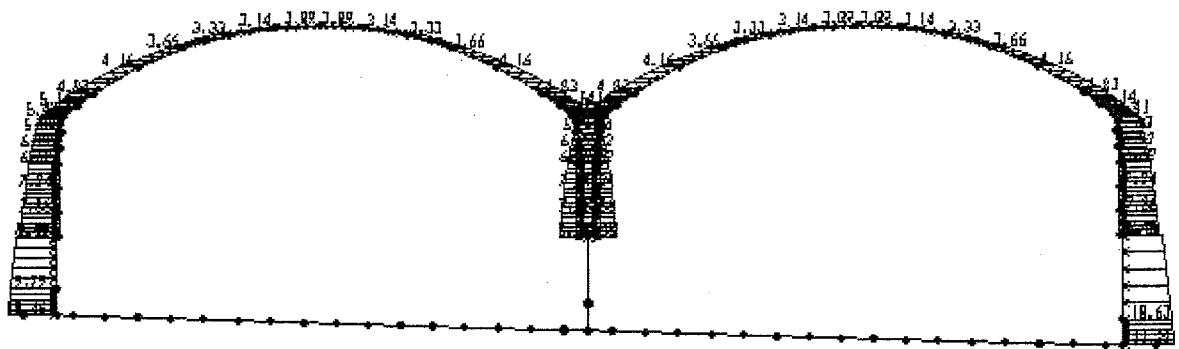
3) 연직토압(Pv) - 지하수 없을때



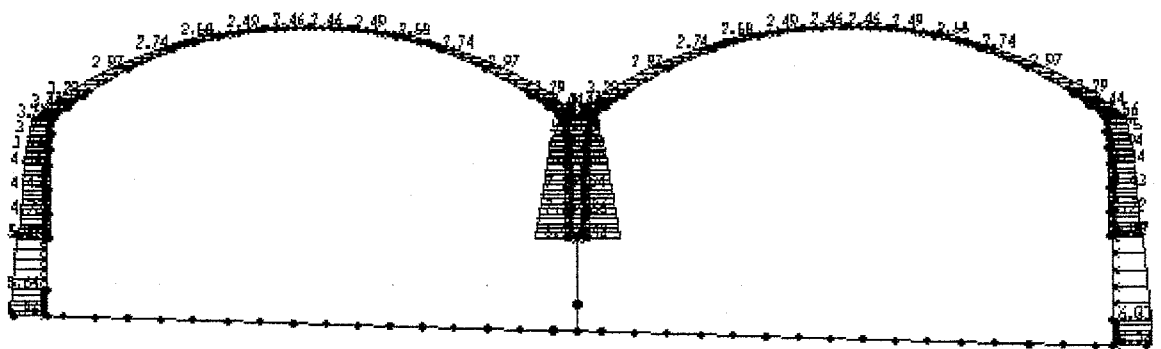
4) 연직토압 (P_{vw}) - 지하수 있을때



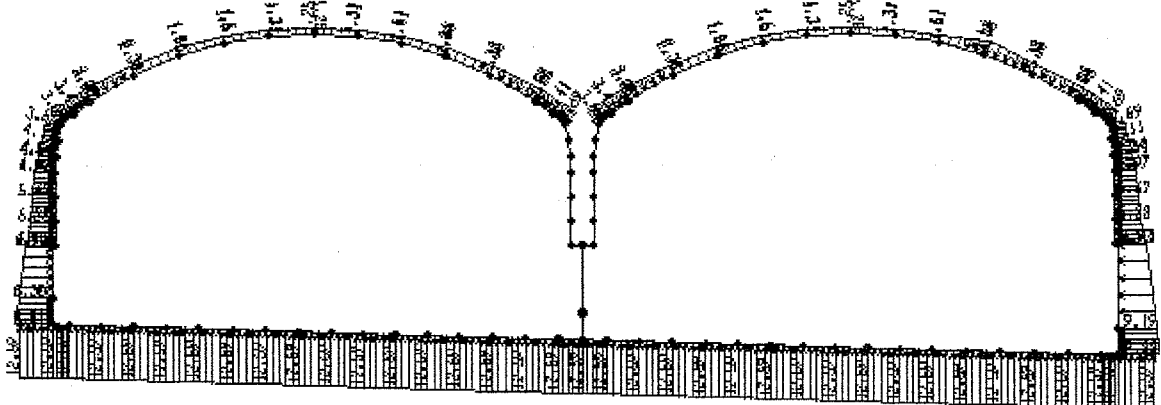
5) 수평토압(P_h) - 지하수 없을때



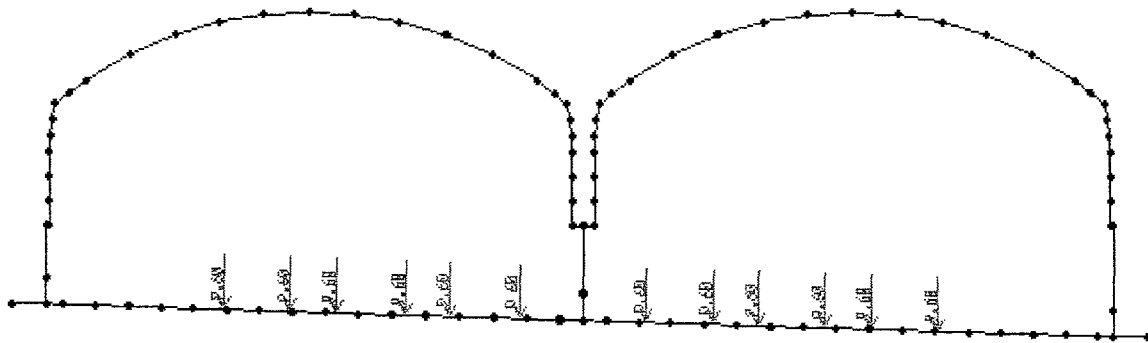
6) 수평토압(P_{hw}) - 지하수 있을때



7) 수압 (P_w)



8) 기초 슬래브에 작용하는 활하중 (PL)



9) 온도 및 건조 수축의 영향

온도는 지하 50cm정도 까지 일변화가 있으나 지중의 온도 변화량은 깊이에 따라 급격히 감소하므로 토피가 1m 이상인 터널에 대해서는 온도 변화의 영향이 미소하여 무시할 수 있을 정도이며 터널 입출구부의 온도차에 의한 영향을 고려하여 별도로 검토하였음.

10) 내진 검토

부산 - 울산의 개착식 터널은 풍화암층 이상의 균질한 지반에 위치하고 있으며 최소 토피고가 3.00m 이상으로 지진발생시 구조물이 지반과 거의 같은 진동을 하므로 지진의 영향을 크게 받지 않는다. 그러므로 내진검토는 제외함.

3.4 하중조합

3.4.1 도로교설계기준

1) 극한하중 검토시

하중조합	구체자중 (SW)	연직토압 (Pv) -수압 없을때	수평토압 (Ph) -수압 없을때	연직토압 (Pvw) -수압 있을때	수평토압 (Phw) -수압 있을때	수압 (PW)	활하중(가설시 PVL)
COMB.1	1.3	1.5	1.7				
COMB.2	1.3	1.5	0.65				
COMB.3	1.3			1.5	1.7	1.3	
COMB.4	1.3			1.5	0.65	1.3	
COMB.5	1.3	1.5	1.7				1.3
COMB.6	1.3	1.5	0.65				1.3

2) 사용하중 검토시

하중조합	구체자중 (SW)	연직토압 (Pv) -수압 없을때	수평토압 (Ph) -수압 없을때	연직토압 (Pvw) -수압 있을때	수평토압 (Phw) -수압 있을때	수압 (PW)	활하중 (PL)
COMB.7	1	1	1				
COMB.8	1	1	1				1
COMB.9	1	1	0.5				
COMB.10	1	1	0.5				1
COMB.11	1			1	1	1	
COMB.12	1			1	1	1	1

* 참조 SAP2000 Input File

하중 조합	Input File	하중 조합	Input File
COMB.1	MAT1.\$2K	COMB.7	MAT1.\$2K
COMB.2	MAT1.\$2K	COMB.8	MAT1.\$2K
COMB.3	MAT3.\$2K	COMB.9	MAT1.\$2K
COMB.4	MAT4.\$2K	COMB.10	MAT1.\$2K
COMB.5	MAT1.\$2K	COMB.11	MAT1.\$3K
COMB.6	MAT6.\$2K	COMB.12	MAT1.\$4K

3.5 해석 결과

1) 모멘트 하중조합 결과

극한 하중 상태							
절점	COMB.1	COMB. 2	COMB. 3	COMB. 4	COMB. 5	COMB. 6	MAX
1	0.00	0.00	0.00	0.00	0.00	0.00	0.00
2	10.69	21.64	6.71	12.73	14.33	25.27	25.27
3	27.11	45.50	20.36	30.28	34.39	52.77	52.77
4	48.76	71.33	40.31	52.15	59.67	82.24	82.24
5	63.21	86.89	54.35	66.45	76.24	99.92	99.92
6	75.19	98.78	66.58	78.21	89.83	113.42	113.42
7	89.23	111.64	81.03	91.50	105.50	127.91	127.91
8	70.46	91.39	63.72	73.26	84.30	105.23	105.23
9	51.20	69.45	45.94	53.79	62.24	80.49	80.49
10	13.99	23.21	11.09	13.28	18.39	27.61	27.61
11	6.94	7.57	8.89	12.85	7.69	8.32	12.85
12	18.40	27.41	20.01	29.04	22.86	31.87	31.87
13	24.07	38.69	25.37	37.44	30.79	45.41	45.41
14	26.30	42.76	26.90	39.21	33.82	50.27	50.27
15	24.07	38.68	23.43	33.23	30.78	45.40	45.40
16	18.38	27.39	16.14	20.62	22.84	31.84	31.84
17	6.91	7.53	3.09	0.22	7.66	8.28	8.28
18	14.03	23.27	18.83	30.13	18.44	27.67	30.13
19	51.29	69.55	55.65	74.88	62.34	80.60	80.60
20	71.18	92.12	74.78	96.57	85.12	106.06	106.06
21	89.35	111.78	92.08	115.46	105.63	128.05	128.05
22	76.83	100.43	79.03	103.52	91.66	115.26	115.26
23	63.43	87.12	65.05	89.53	76.49	100.17	100.17
24	48.75	71.32	49.97	73.21	59.66	82.23	82.23
25	27.11	45.50	27.92	46.75	34.38	52.77	52.77
26	10.69	21.64	11.10	22.27	14.32	25.27	25.27
27	0.00	0.00	0.00	0.00	0.00	0.00	0.00
28	0.00	0.00	0.00	0.00	0.00	0.00	0.00
29	10.74	21.57	11.91	23.00	14.35	25.19	25.19
30	27.20	45.36	29.55	48.21	34.44	52.60	52.60
31	48.89	71.12	52.41	75.40	59.75	81.98	81.98
32	63.60	86.87	68.05	92.22	76.59	99.86	99.86
33	77.03	100.13	82.76	106.88	91.78	114.89	114.89
34	89.58	111.44	96.41	119.38	105.77	127.63	127.63
35	71.44	91.77	79.12	100.45	85.28	105.61	105.61
36	14.40	22.84	22.79	33.51	18.68	27.12	33.51
37	6.51	8.01	0.28	2.50	7.39	8.89	8.89

38	17.97	27.92	13.58	18.75	22.57	32.52	32.52
39	23.65	39.25	21.87	32.39	30.52	46.12	46.12
40	25.90	43.34	26.52	39.56	33.57	51.01	51.01
41	23.69	39.29	26.30	39.09	30.56	46.16	46.16
42	18.05	28.00	22.44	32.16	22.65	32.60	32.60
43	6.62	8.13	12.42	17.03	7.51	9.02	17.03
44	14.27	22.70	8.75	10.36	18.54	26.97	26.97
45	51.45	69.03	45.41	52.76	62.38	79.96	79.96
46	51.45	69.03	45.41	52.76	62.38	79.96	79.96
47	70.69	91.01	63.85	72.94	84.45	104.77	104.77
48	89.47	111.32	81.69	91.75	105.65	127.50	127.50
49	75.39	98.49	67.22	78.49	89.96	113.06	113.06
50	63.38	86.64	54.98	66.77	76.34	99.61	99.61
51	48.90	71.12	40.85	52.44	59.75	81.98	81.98
52	27.20	45.36	20.72	30.47	34.44	52.60	52.60
53	10.74	21.57	6.89	12.83	14.35	25.19	25.19
54	0.00	0.00	0.00	0.00	0.00	0.00	0.00
101	8.84	8.84	8.21	8.14	9.79	9.79	9.79
102	6.96	28.79	19.18	1.03	0.27	35.47	35.47
301	8.84	8.84	8.33	8.26	9.79	9.79	9.79
302	21.97	46.57	45.80	7.05	10.41	58.12	58.12
401	0.00	0.00	0.00	0.00	0.00	0.00	0.00
402	36.43	38.49	85.29	56.26	31.23	44.05	85.29
403	16.36	20.07	67.26	39.35	10.67	25.76	67.26
404	6.46	24.17	26.18	1.11	10.69	28.41	28.41
405	10.60	16.66	8.63	30.83	12.89	18.95	30.83
406	8.00	8.64	37.00	56.36	8.92	9.56	56.36
407	4.46	3.33	59.00	75.50	4.66	3.53	75.50
408	1.86	0.68	74.55	88.21	1.78	0.60	88.21
409	0.44	0.35	83.69	94.48	0.30	0.50	94.48
410	0.16	0.54	86.30	94.26	0.29	0.67	94.26
411	0.14	0.28	82.45	87.54	0.21	0.36	87.54
412	0.61	0.60	72.01	74.27	0.64	0.63	74.27
413	2.60	2.60	55.06	54.46	2.84	2.84	55.06
414	6.36	6.37	31.50	28.05	6.99	7.00	31.50
415	11.75	11.84	1.21	5.03	12.95	13.05	13.05
416	16.25	16.26	35.51	44.65	17.90	17.92	44.65
417	11.50	11.54	78.96	90.97	12.67	12.70	90.97
418	20.11	20.01	129.20	144.05	22.19	22.09	144.05
419	51.85	51.97	159.48	175.49	57.19	57.37	175.49
420	20.01	20.17	126.84	144.75	22.13	22.30	144.75
421	11.50	11.49	76.25	90.23	12.66	12.65	90.23
422	16.23	16.27	32.46	42.53	17.88	17.92	42.53
423	11.84	11.80	4.64	1.59	13.03	12.99	13.03
424	6.32	6.40	34.65	32.41	6.96	7.04	34.65
425	2.55	2.63	57.87	59.56	2.80	2.87	59.56
426	0.62	0.59	74.25	79.84	0.65	0.60	79.84
427	0.10	0.31	83.67	93.19	0.18	0.45	93.19
428	0.00	0.63	86.18	99.60	0.15	0.91	99.60
429	0.76	0.51	81.66	99.01	0.56	0.87	99.01
430	2.42	0.43	70.18	91.43	2.24	0.16	91.43
431	5.05	3.14	51.63	76.81	5.15	3.50	76.81
432	8.05	8.84	26.07	55.16	8.99	10.38	55.16
433	8.54	18.07	6.61	26.40	11.25	20.82	26.40
434	0.39	28.04	46.40	9.49	5.16	33.47	46.40
435	31.57	27.75	93.34	52.49	23.07	36.16	93.34
436	55.49	42.09	113.92	71.52	46.83	48.81	113.92
437	0.00	0.00	0.00	0.00	0.00	0.00	0.00

사용 하중 상태							
절점	COMB. 7	COMB. 8	COMB. 9	COMB. 10	COMB. 11	COMB. 12	MAX
1	0.00	0.00	0.00	0.00	0.00	0.00	0.00
2	8.92	8.92	14.13	14.13	9.92	9.92	14.13
3	21.21	21.21	29.97	29.97	21.87	21.87	29.97
4	36.57	36.57	47.32	47.32	35.70	35.70	47.32
5	46.58	46.58	57.86	57.86	44.45	44.45	57.86
6	54.73	54.73	65.96	65.96	51.57	51.57	65.96
7	64.11	64.11	74.79	74.79	59.46	59.46	74.79
8	51.13	51.13	61.09	61.09	49.15	49.15	61.09
9	37.64	37.64	46.33	46.33	38.13	38.13	46.33
10	10.97	10.97	15.36	15.36	14.98	14.98	15.36
11	4.79	4.79	5.09	5.09	0.21	0.21	5.09
12	13.89	13.89	18.18	18.18	10.06	10.06	18.18
13	18.63	18.63	25.59	25.59	15.95	15.95	25.59
14	20.43	20.43	28.27	28.27	18.83	18.83	28.27
15	18.62	18.62	25.58	25.58	18.12	18.12	25.58
16	13.88	13.88	18.17	18.17	14.39	14.39	18.17
17	4.77	4.77	5.07	5.07	6.71	6.71	6.71
18	10.99	10.99	15.39	15.39	6.32	6.32	15.39
19	37.70	37.70	46.40	46.40	27.34	27.34	46.40
20	51.62	51.62	61.60	61.60	37.89	37.89	61.60
21	64.20	64.20	74.88	74.88	47.23	47.23	74.88
22	55.84	55.84	67.08	67.08	40.20	40.20	67.08
23	46.73	46.73	58.01	58.01	32.79	32.79	58.01
24	36.57	36.57	47.32	47.32	24.84	24.84	47.32
25	21.21	21.21	29.96	29.96	13.39	13.39	29.96
26	8.92	8.92	14.13	14.13	5.01	5.01	14.13
27	0.00	0.00	0.00	0.00	0.00	0.00	0.00
28	0.00	0.00	0.00	0.00	0.00	0.00	0.00
29	8.93	8.93	14.09	14.09	4.97	4.97	14.09
30	21.24	21.24	29.89	29.89	13.32	13.32	29.89
31	36.61	36.61	47.20	47.20	24.74	24.74	47.20
32	46.79	46.79	57.87	57.87	32.69	32.69	57.87
33	55.90	55.90	66.91	66.91	40.24	40.24	66.91
34	64.26	64.26	74.67	74.67	47.36	47.36	74.67
35	51.71	51.71	61.39	61.39	38.00	38.00	61.39
36	11.13	11.13	15.15	15.15	6.38	6.38	15.15
37	4.63	4.63	5.34	5.34	6.71	6.71	6.71
38	13.74	13.74	18.48	18.48	14.45	14.45	18.48
39	18.49	18.49	25.91	25.91	18.22	18.22	25.91
40	20.31	20.31	28.61	28.61	18.98	18.98	28.61
41	18.52	18.52	25.94	25.94	16.13	16.13	25.94
42	13.79	13.79	18.53	18.53	10.27	10.27	18.53
43	4.71	4.71	5.43	5.43	0.44	0.44	5.43
44	11.03	11.03	15.05	15.05	14.75	14.75	15.05
45	37.71	37.71	46.08	46.08	37.93	37.93	46.08
46	37.71	37.71	46.08	46.08	37.93	37.93	46.08
47	51.20	51.20	60.87	60.87	48.97	48.97	60.87
48	64.19	64.19	74.60	74.60	59.30	59.30	74.60
49	54.79	54.79	65.79	65.79	51.43	51.43	65.79
50	46.63	46.63	57.71	57.71	44.33	44.33	57.71
51	36.62	36.62	47.20	47.20	35.59	35.59	47.20
52	21.24	21.24	29.89	29.89	21.80	21.80	29.89

53	8.93	8.93	14.09	14.09	9.88	9.88	14.09
54	0.00	0.00	0.00	0.00	0.00	0.00	0.00
101	6.04	6.04	6.04	6.04	4.79	4.79	6.04
102	0.60	0.60	17.62	17.62	8.94	8.94	17.62
301	6.04	6.04	6.04	6.04	4.78	4.78	6.04
302	4.71	4.71	27.93	27.93	12.11	12.11	27.93
401	0.00	0.00	0.00	0.00	0.00	0.00	0.00
402	18.34	18.25	25.49	25.41	18.10	18.02	25.49
403	5.71	5.55	11.63	11.79	3.93	4.09	11.79
404	7.13	7.58	15.57	16.02	9.90	10.34	16.02
405	8.22	9.04	11.10	11.93	8.06	8.88	11.93
406	5.62	6.69	5.92	6.99	4.71	5.78	6.99
407	2.92	3.45	2.38	2.91	2.13	2.66	3.45
408	1.13	0.33	0.56	0.89	0.67	0.78	1.13
409	0.21	0.73	0.17	0.35	0.03	0.55	0.73
410	0.15	1.46	0.33	1.64	0.16	1.47	1.64
411	0.09	0.40	0.16	0.47	0.06	0.37	0.47
412	0.44	1.58	0.44	1.57	0.39	1.52	1.58
413	1.81	2.30	1.81	2.30	1.46	1.96	2.30
414	4.39	4.14	4.40	4.15	3.49	3.23	4.40
415	8.11	7.69	8.15	7.74	6.41	5.99	8.15
416	11.18	11.73	11.19	11.74	8.80	9.34	11.74
417	7.92	7.58	7.94	7.60	6.26	5.91	7.94
418	13.77	11.99	13.73	11.94	10.67	8.89	13.77
419	35.59	33.59	35.67	33.68	27.89	25.89	35.67
420	13.74	11.97	13.82	12.04	10.77	8.99	13.82
421	7.92	7.56	7.91	7.56	6.22	5.86	7.92
422	11.17	11.71	11.19	11.73	8.79	9.33	11.73
423	8.15	7.77	8.13	7.75	6.41	6.04	8.15
424	4.38	4.26	4.41	4.30	3.49	3.38	4.41
425	1.79	2.12	1.82	2.15	1.46	1.79	2.15
426	0.45	1.52	0.43	1.51	0.39	1.47	1.52
427	0.08	0.39	0.17	0.49	0.06	0.38	0.49
428	0.07	1.37	0.37	1.67	0.15	1.45	1.67
429	0.35	0.88	0.25	0.28	0.04	0.57	0.88
430	1.39	0.05	0.44	1.00	0.71	0.73	1.39
431	3.21	3.74	2.30	2.83	2.20	2.73	3.74
432	5.69	6.76	6.07	7.13	4.82	5.89	7.13
433	7.36	8.18	11.90	12.72	8.18	9.01	12.72
434	4.10	4.54	17.64	18.08	9.91	10.35	18.08
435	12.65	12.49	15.60	15.76	3.51	3.67	15.76
436	27.13	27.04	27.49	27.42	18.36	18.29	27.49
437	0.00	0.00	0.00	0.00	0.00	0.00	0.00

2) 전단력 하중조합 결과

극한 하중 상태							
절점	COMB.1	COMB. 2	COMB. 3	COMB. 4	COMB. 5	COMB. 6	MAX
1	11.78	31.38	4.70	15.60	17.35	36.95	36.95
2	20.85	34.85	15.72	23.28	26.42	40.42	40.42
3	29.25	38.06	25.86	30.28	34.81	43.63	43.63
4	36.94	41.00	35.11	36.59	42.51	46.57	46.57
5	36.20	37.39	35.68	35.40	41.17	42.35	42.35
6	30.84	29.28	31.60	29.66	34.66	33.10	34.66
7	45.90	48.38	42.38	43.91	51.50	53.98	53.98
8	39.50	43.38	36.53	38.95	44.84	48.73	48.73
9	38.75	43.54	36.34	39.23	44.45	49.24	49.24
10	25.78	32.18	24.61	28.49	30.63	37.03	37.03
11	17.42	23.45	16.90	20.45	21.30	27.33	27.33
12	11.88	16.13	11.53	13.75	14.66	18.92	18.92
13	8.41	9.84	7.83	7.96	10.00	11.43	11.43
14	4.68	3.06	5.26	4.98	4.94	3.33	5.26
15	8.42	9.85	9.44	11.45	10.01	11.44	11.45
16	11.89	16.14	13.11	17.20	14.67	18.93	18.93
17	17.43	23.46	18.44	23.80	21.31	27.34	27.34
18	25.79	32.19	26.08	31.70	30.63	37.04	37.04
19	38.75	43.55	37.72	42.25	44.45	49.25	49.25
20	40.31	44.14	38.62	42.53	45.74	49.57	49.57
21	44.95	47.47	42.70	45.75	50.44	52.95	52.95
22	33.42	31.87	34.60	33.27	37.54	35.99	37.54
23	36.74	37.93	37.68	39.17	41.77	42.96	42.96
24	36.94	41.00	37.56	41.96	42.50	46.57	46.57
25	29.24	38.06	29.87	39.02	34.81	43.63	43.63
26	20.85	34.85	21.47	35.81	26.42	40.42	40.42
27	11.78	31.38	12.40	32.34	17.34	36.95	36.95
28	11.85	31.28	13.64	33.46	17.39	36.82	36.82
29	20.92	34.75	22.72	36.93	26.46	40.29	40.29
30	29.31	37.96	31.11	40.14	34.85	43.50	43.50
31	37.01	40.90	38.80	43.08	42.55	46.44	46.44
32	36.81	37.83	39.09	40.45	41.81	42.83	42.83
33	33.49	31.77	36.26	34.81	37.58	35.86	37.58
34	44.92	47.54	42.74	45.87	50.42	53.04	53.04
35	35.95	40.12	34.37	38.52	40.92	45.09	45.09
36	15.30	23.49	15.91	22.81	19.16	27.35	27.35
37	6.46	15.09	8.07	15.31	9.46	18.09	18.09
38	1.10	8.47	3.22	9.60	3.13	10.50	10.50
39	2.45	2.51	0.22	4.42	1.52	3.44	4.42
40	4.66	3.04	2.68	0.51	4.92	3.30	4.92
41	8.39	9.83	6.74	6.87	9.99	11.42	11.42
42	11.86	16.14	10.30	12.55	14.65	18.93	18.93
43	17.39	23.46	16.95	20.53	21.28	27.36	27.36
44	25.74	32.21	25.99	29.93	30.60	37.07	37.07
45	38.70	43.58	37.61	40.57	44.41	49.29	49.29
46	38.70	43.58	37.61	40.57	44.41	49.29	49.29
47	39.45	43.43	37.69	40.18	44.81	48.80	48.80
48	45.85	48.44	43.50	45.11	51.46	54.05	54.05
49	30.91	29.18	31.64	29.57	34.70	32.97	34.70
50	36.28	37.29	35.88	35.47	41.21	42.23	42.23

51	37.01	40.90	35.39	36.74	42.55	46.44	46.44
52	29.32	37.96	26.14	30.43	34.86	43.50	43.50
53	20.92	34.75	15.99	23.42	26.46	40.29	40.29
54	11.85	31.28	4.98	15.75	17.39	36.82	36.82
101	11.78	31.38	4.70	15.60	17.35	36.95	36.95
102	9.54	23.23	21.32	2.74	3.98	28.80	28.80
301	11.85	31.28	4.98	15.75	17.39	36.82	36.82
302	24.85	17.25	39.91	16.03	19.31	22.79	39.91
401	26.53	43.72	49.93	56.08	32.53	49.72	56.08
402	56.52	39.51	57.40	63.55	57.91	45.51	63.55
403	58.11	35.97	50.08	46.87	59.50	37.36	59.50
404	27.83	10.51	42.96	39.72	26.19	12.71	42.96
405	6.70	11.08	35.76	32.52	6.50	12.63	35.76
406	6.02	8.02	28.53	25.29	6.84	8.83	28.53
407	4.94	5.02	21.28	18.04	5.26	5.33	21.28
408	3.62	3.18	13.99	10.76	3.69	3.25	13.99
409	2.70	2.22	6.67	3.43	2.67	2.20	6.67
410	1.98	1.79	0.72	3.93	1.92	1.82	3.93
411	2.04	2.30	8.09	11.31	2.10	2.36	11.31
412	2.86	3.01	15.51	18.72	2.98	3.13	18.72
413	4.26	4.27	22.95	26.16	4.49	4.51	26.16
414	6.27	6.28	30.49	33.65	6.71	6.72	33.65
415	8.10	8.20	38.00	41.16	8.75	8.85	41.16
416	7.38	7.36	45.41	48.65	7.93	7.91	48.65
417	37.75	37.68	53.01	56.22	41.43	41.36	56.22
418	91.41	91.42	84.95	88.24	100.71	100.72	100.72
419	89.82	89.98	87.97	91.26	99.11	99.32	99.32
420	91.29	91.57	84.24	83.33	100.63	100.91	100.91
421	37.64	37.81	53.42	57.84	41.35	41.53	57.84
422	7.36	7.41	45.85	50.21	7.92	7.98	50.21
423	8.25	8.12	38.13	42.48	8.87	8.74	42.48
424	6.28	6.28	30.17	34.62	6.72	6.73	34.62
425	4.20	4.31	22.45	26.87	4.44	4.58	26.87
426	2.83	3.03	14.63	19.05	2.95	3.19	19.05
427	1.89	2.38	6.78	11.19	1.97	2.53	11.19
428	2.13	1.87	1.16	3.31	2.04	1.97	3.31
429	2.87	2.15	9.07	4.63	2.81	2.05	9.07
430	3.89	3.07	17.02	12.57	3.92	3.17	17.02
431	4.98	5.08	24.99	20.54	5.30	5.79	24.99
432	5.41	8.46	32.99	28.54	6.35	9.81	32.99
433	12.10	12.46	41.02	36.57	8.90	13.83	41.02
434	37.30	13.28	49.09	44.64	33.96	16.31	49.09
435	69.12	31.76	57.18	52.73	68.64	31.20	69.12
436	67.53	43.40	60.40	62.48	67.05	50.66	67.53
437	20.65	47.61	38.89	53.97	27.85	54.87	54.87

사용 하중 상태							
절점	COMB. 7	COMB. 8	COMB. 9	COMB. 10	COMB. 11	COMB. 12	MAX
1	10.96	10.96	20.29	20.29	13.58	13.58	20.29
2	16.29	16.29	22.96	22.96	16.76	16.76	22.96
3	21.23	21.23	25.43	25.43	19.76	19.76	25.43
4	25.76	25.76	27.69	27.69	22.55	22.55	27.69
5	24.83	24.83	25.39	25.39	21.40	21.40	25.39
6	20.77	20.77	20.03	20.03	17.74	17.74	20.77
7	31.58	31.58	32.76	32.76	24.82	24.82	32.76
8	27.43	27.43	29.28	29.28	22.05	22.05	29.28
9	27.07	27.07	29.35	29.35	22.40	22.40	29.35
10	18.52	18.52	21.57	21.57	16.58	16.58	21.57
11	12.80	12.80	15.67	15.67	12.30	12.30	15.67
12	8.76	8.76	10.79	10.79	8.89	8.89	10.79
13	5.96	5.96	6.64	6.64	6.18	6.18	6.64
14	2.94	2.94	2.17	2.17	3.19	3.19	3.19
15	5.96	5.96	6.64	6.64	4.38	4.38	6.64
16	8.76	8.76	10.79	10.79	7.12	7.12	10.79
17	12.80	12.80	15.67	15.67	10.57	10.57	15.67
18	18.53	18.53	21.58	21.58	14.93	14.93	21.58
19	27.07	27.07	29.35	29.35	20.85	20.85	29.35
20	27.97	27.97	29.79	29.79	21.02	21.02	29.79
21	30.94	30.94	32.14	32.14	22.89	22.89	32.14
22	22.53	22.53	21.79	21.79	18.53	18.53	22.53
23	25.20	25.20	25.76	25.76	20.00	20.00	25.76
24	25.76	25.76	27.69	27.69	19.77	19.77	27.69
25	21.23	21.23	25.43	25.43	15.24	15.24	25.43
26	16.29	16.29	22.96	22.96	10.31	10.31	22.96
27	10.95	10.95	20.29	20.29	4.97	4.97	20.29
28	10.98	10.98	20.23	20.23	4.92	4.92	20.23
29	16.31	16.31	22.90	22.90	10.25	10.25	22.90
30	21.25	21.25	25.37	25.37	15.19	15.19	25.37
31	25.78	25.78	27.63	27.63	19.72	19.72	27.63
32	25.22	25.22	25.70	25.70	20.08	20.08	25.70
33	22.55	22.55	21.73	21.73	18.84	18.84	22.55
34	30.93	30.93	32.18	32.18	22.94	22.94	32.18
35	25.06	25.06	27.05	27.05	18.78	18.78	27.05
36	11.65	11.65	15.55	15.55	9.56	9.56	15.55
37	5.72	5.72	9.83	9.83	5.08	5.08	9.83
38	1.89	1.89	5.39	5.39	1.79	1.79	5.39
39	0.90	0.90	1.46	1.46	0.93	0.93	1.46
40	2.93	2.93	2.16	2.16	3.16	3.16	3.16
41	5.95	5.95	6.63	6.63	6.15	6.15	6.63
42	8.75	8.75	10.79	10.79	8.87	8.87	10.79
43	12.78	12.78	15.67	15.67	12.29	12.29	15.67
44	18.51	18.51	21.59	21.59	16.57	16.57	21.59
45	27.05	27.05	29.37	29.37	22.40	22.40	29.37
46	27.05	27.05	29.37	29.37	22.40	22.40	29.37
47	27.41	27.41	29.31	29.31	22.06	22.06	29.31
48	31.56	31.56	32.79	32.79	24.83	24.83	32.79
49	20.79	20.79	19.97	19.97	17.69	17.69	20.79
50	24.85	24.85	25.33	25.33	21.35	21.35	25.33
51	25.78	25.78	27.63	27.63	22.50	22.50	27.63
52	21.25	21.25	25.37	25.37	19.70	19.70	25.37

53	16.31	16.31	22.90	22.90	16.71	16.71	22.90
54	10.98	10.98	20.23	20.23	13.53	13.53	20.23
101	10.96	10.96	20.29	20.29	13.58	13.58	20.29
102	1.59	1.59	14.02	14.02	6.27	6.27	14.02
301	10.98	10.98	20.23	20.23	13.53	13.53	20.23
302	10.61	10.61	9.44	9.44	1.05	1.05	10.61
401	20.99	20.91	29.18	29.09	21.19	21.10	29.18
402	35.44	35.64	25.94	25.86	23.23	23.43	35.64
403	36.66	36.86	26.12	26.32	24.45	24.66	36.86
404	16.09	16.41	6.60	6.32	8.30	8.62	16.41
405	4.49	4.22	7.41	7.14	5.34	5.06	7.41
406	4.60	5.21	5.55	6.16	4.47	5.07	6.16
407	3.57	6.54	3.61	6.57	3.19	6.16	6.57
408	2.58	6.15	2.37	6.11	2.28	6.53	6.53
409	1.95	4.38	1.72	4.15	1.76	4.19	4.38
410	1.48	8.31	1.37	8.53	1.44	8.50	8.53
411	1.61	5.82	1.73	5.75	1.65	5.92	5.92
412	2.15	6.87	2.22	6.94	2.06	6.77	6.94
413	3.09	5.08	3.10	5.07	2.76	5.71	5.71
414	4.47	7.61	4.48	7.61	3.84	6.97	7.61
415	5.74	12.44	5.79	12.49	4.85	11.55	12.49
416	5.23	8.59	5.22	8.58	4.42	7.78	8.59
417	26.08	23.67	26.05	23.64	20.69	18.29	26.08
418	62.89	62.29	62.90	62.30	49.40	48.79	62.90
419	61.67	61.06	61.76	61.15	48.25	47.64	61.76
420	62.85	62.24	62.99	62.37	49.48	48.87	62.99
421	26.04	23.63	26.12	23.71	20.76	18.34	26.12
422	5.23	8.60	5.25	8.62	4.45	7.82	8.62
423	5.81	12.40	5.75	12.33	4.85	11.43	12.40
424	4.48	7.41	4.48	7.41	3.84	6.77	7.41
425	3.06	5.28	3.12	5.27	2.76	5.91	5.91
426	2.14	6.80	2.23	6.89	2.06	6.72	6.89
427	1.54	5.89	1.77	5.80	1.65	5.97	5.97
428	1.55	8.23	1.41	8.57	1.44	8.49	8.57
429	2.03	4.46	1.68	4.12	1.77	4.20	4.46
430	2.72	6.11	2.33	6.07	2.30	6.49	6.49
431	3.61	6.57	3.66	6.62	3.23	6.20	6.62
432	4.35	4.96	5.81	6.41	4.52	5.12	6.41
433	5.23	5.66	8.15	7.87	5.35	5.08	8.15
434	20.50	20.82	8.03	7.60	8.79	9.11	20.82
435	41.96	42.16	24.17	24.37	25.41	25.61	42.16
436	40.74	40.94	28.10	28.02	24.19	24.39	40.94
437	18.50	18.42	31.34	31.26	21.47	21.39	31.34

3) 설계 단면력 산정

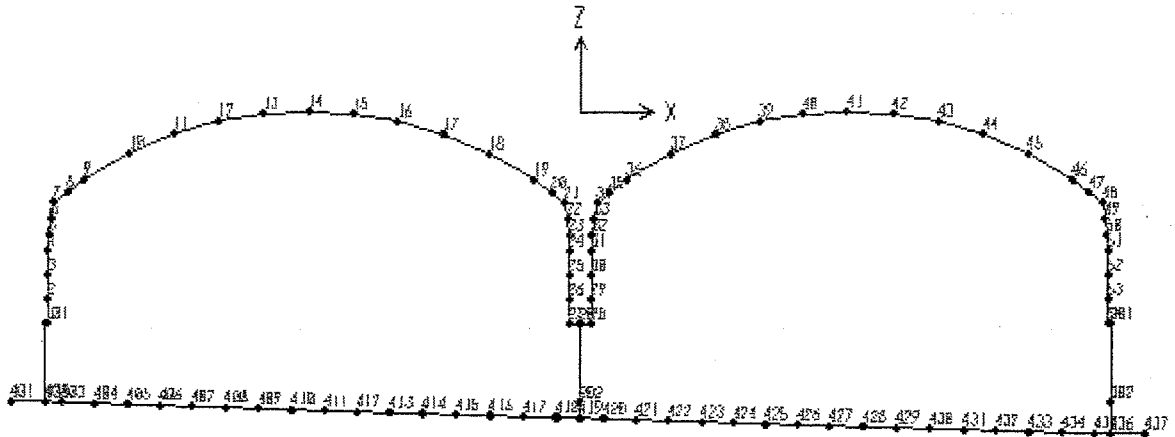
절점	모멘트		전단력	
	극한 하중 상태	사용하중 상태	극한 하중 상태	사용하중 상태
1	0.00	0.00	36.95	20.29
2	25.27	14.13	40.42	22.96
3	52.77	29.97	43.63	25.43
4	82.24	47.32	46.57	27.69
5	99.92	57.86	42.35	25.39
6	113.42	65.96	34.66	20.77
7	127.91	74.79	53.98	32.76
8	105.23	61.09	48.73	29.28
9	80.49	46.33	49.24	29.35
10	27.61	15.36	37.03	21.57
11	12.85	5.09	27.33	15.67
12	31.87	18.18	18.92	10.79
13	45.41	25.59	11.43	6.64
14	50.27	28.27	5.26	3.19
15	45.40	25.58	11.45	6.64
16	31.84	18.17	18.93	10.79
17	8.28	6.71	27.34	15.67
18	30.13	15.39	37.04	21.58
19	80.60	46.40	49.25	29.35
20	106.06	61.60	49.57	29.79
21	128.05	74.88	52.95	32.14
22	115.26	67.08	37.54	22.53
23	100.17	58.01	42.96	25.76
24	82.23	47.32	46.57	27.69
25	52.77	29.96	43.63	25.43
26	25.27	14.13	40.42	22.96
27	0.00	0.00	36.95	20.29
28	0.00	0.00	36.82	20.23
29	25.19	14.09	40.29	22.90
30	52.60	29.89	43.50	25.37
31	81.98	47.20	46.44	27.63
32	99.86	57.87	42.83	25.70
33	114.89	66.91	37.58	22.55
34	127.63	74.67	53.04	32.18
35	105.61	61.39	45.09	27.05
36	33.51	15.15	27.35	15.55
37	8.89	6.71	18.09	9.83
38	32.52	18.48	10.50	5.39
39	46.12	25.91	4.42	1.46
40	51.01	28.61	4.92	3.16
41	46.16	25.94	11.42	6.63
42	32.60	18.53	18.93	10.79
43	17.03	5.43	27.36	15.67
44	26.97	15.05	37.07	21.59
45	79.96	46.08	49.29	29.37
46	79.96	46.08	49.29	29.37
47	104.77	60.87	48.80	29.31
48	127.50	74.60	54.05	32.79
49	113.06	65.79	34.70	20.79

50	99.61	57.71	42.23	25.33
51	81.98	47.20	46.44	27.63
52	52.60	29.89	43.50	25.37
53	25.19	14.09	40.29	22.90
54	0.00	0.00	36.82	20.23
101	9.79	6.04	36.95	20.29
102	35.47	17.62	28.80	14.02
301	9.79	6.04	36.82	20.23
302	58.12	27.93	39.91	10.61
401	0.00	0.00	56.08	29.18
402	85.29	25.49	63.55	35.64
403	67.26	11.79	59.50	36.86
404	28.41	16.02	42.96	16.41
405	30.83	11.93	35.76	7.41
406	56.36	6.99	28.53	6.16
407	75.50	3.45	21.28	6.57
408	88.21	1.13	13.99	6.53
409	94.48	0.73	6.67	4.38
410	94.26	1.64	3.93	8.53
411	87.54	0.47	11.31	5.92
412	74.27	1.58	18.72	6.94
413	55.06	2.30	26.16	5.71
414	31.50	4.40	33.65	7.61
415	13.05	8.15	41.16	12.49
416	44.65	11.74	48.65	8.59
417	90.97	7.94	56.22	26.08
418	144.05	13.77	100.72	62.90
419	175.49	35.67	99.32	61.76
420	144.75	13.82	100.91	62.99
421	90.23	7.92	57.84	26.12
422	42.53	11.73	50.21	8.62
423	13.03	8.15	42.48	12.40
424	34.65	4.41	34.62	7.41
425	59.56	2.15	26.87	5.91
426	79.84	1.52	19.05	6.89
427	93.19	0.49	11.19	5.97
428	99.60	1.67	3.31	8.57
429	99.01	0.88	9.07	4.46
430	91.43	1.39	17.02	6.49
431	76.81	3.74	24.99	6.62
432	55.16	7.13	32.99	6.41
433	26.40	12.72	41.02	8.15
434	46.40	18.08	49.09	20.82
435	93.34	15.76	69.12	42.16
436	113.92	27.49	67.53	40.94
437	0.00	0.00	54.87	31.34

4. 단 면 검 토

4.1 Precast Arch Box 본체 검토

1) 단면력 집계



구분		극한 하중		사용 하중		비 고
	절점 위치	모멘트 t-m/m	전단력 t/m	모멘트 t-m/m	전단력 t/m	
PAB	5 번	100.17	42.96	58.01	25.76	벽체변화부
	7 번	128.05	54.05	74.88	32.79	헌치부
	14 번	50.27	11.42	28.27	6.63	슬래브중앙
기초	403 번	93.34	69.12	15.76	42.16	기초
	428 번	99.60	3.31	1.67	8.57	기초
	418 번	144.75	100.91	13.82	62.99	기초
	102 번	58.12	39.91	27.93	14.02	기초벽체

* 위의 각절점과 공통으로 검토해야하는 절점

5 번 : 23 32 50 번

7 번 : 21 34 48 번

14 번 : 41 번

403 번 : 435 번

428 번 : 기초슬래브구간 중 최대 정모멘트가 발생하는 절점

418 번 : 420 번

102 번 : 302 번

* 설계에 필요한 값들은 위의 공통된 절점에서 최대값을 설계에 반영함.

2) 극한강 검토 극한 강도 설계법 검토

(1) P.A.B 검토

① 상부 슬래브 (정모멘트) (14 번 절점)

$$M_u = 50.270 \text{ t-m / m}, \quad V_u = 11.420 \text{ t/m}$$

$$\begin{aligned} d &= 40.82 \text{ cm}, & d_c &= 9.18 \text{ cm}, & b &= 100 \text{ cm} \\ f_{ck} &= 400 \text{ kgf/cm}^2, & f_y &= 4000 \text{ kgf/cm}^2, & \beta_1 &= 0.766 \end{aligned}$$

$$\Phi M_n = 0.9 * f_y * A_s * (d - a/2) \text{ 에서} \quad \Phi = 0.9 \text{ (Precast)}$$

$$A_{s, \text{req}} = \frac{M_u}{0.90 * f_y * (d - a/2)} \text{ 로 부터}$$

$$a = \frac{A_s * f_y}{0.85 * f_{ck} * b} = 4.245 \quad A_{s, \text{req}} = 36.08 \text{ cm}^2$$

$$\begin{aligned} \therefore H \ 19 \ @ \ 100 &= 2.865 * 10.00 \\ H \ 19 \ @ \ 100 &= 2.865 * 10.00 \text{ (2단배근)} \\ &= 57.30 \text{ cm}^2 \text{를 배근함.} \end{aligned}$$

OK!

$$\text{단면 철근비} \quad \rho = \frac{A_s}{b * d} = 0.0140$$

$$\text{최대 철근비} \quad \rho_{\max} = 0.64 * \beta_1 * \frac{f_{ck}}{f_y} * \frac{6000}{(6000 + f_y)} = 0.0294$$

$$\text{최소 철근비} \quad \rho_{\min} = \frac{0.8 * \sqrt{f_{ck}}}{f_y} = 0.0040 > \frac{14}{f_y} = 0.0035$$

$\therefore$ 최대 철근비 규정 만족!

$\therefore$ 최소 철근비 규정 만족!

$$\begin{aligned} \Phi V_c &= 0.8 * 0.53 * \sqrt{f_{ck}} * b_w * d \\ &= 34.62 \text{ t/m} > V_u = 11.42 \text{ t/m} \end{aligned}$$

$$\Phi V_c / 2 = 17.31 \text{ t/m} > V_u = 11.42 \text{ t/m}$$

$\therefore$ 전단 철근을 배근하지 않아도 된다.

② 현치부 (부모멘트) (7 번 절점)

$$M_u = 128.050 \text{ t-m / m}, \quad V_u = 54.050 \text{ t/m}$$

$$\begin{aligned} d &= 82.11 \text{ cm}, & d_c &= 9.49 \text{ cm}, & b &= 100 \text{ cm} \\ f_{ck} &= 400 \text{ kgf/cm}^2 & f_y &= 4000 \text{ kgf/cm}^2 & \beta_1 &= 0.766 \end{aligned}$$

$$\Phi M_n = 0.9 * f_y * A_s * (d - a/2) \text{ 에서} \quad \Phi = 0.9 \text{ (Precast)}$$

$$A_{s,req} = \frac{M_u}{0.90 * f_y * (d - a/2)} \text{ 로 부터}$$

$$a = \frac{A_s * f_y}{0.85 * f_{ck} * b} = 5.265 \quad A_{s,req} = 44.75 \text{ cm}^2$$

$$\begin{aligned} \therefore H \ 22 \ @ \ 100 &= 3.871 * 10.00 \\ H \ 22 \ @ \ 100 &= 3.871 * 10.00 \text{ (2단배근)} \\ &= 77.42 \text{ cm}^2 \text{를 배근함.} \end{aligned}$$

OK!

$$\text{단면 철근비} \quad \rho = \frac{A_s}{b * d} = 0.0094$$

$$\text{최대 철근비} \quad \rho_{max} = 0.64 * \beta_1 * \frac{f_{ck}}{f_y} * \frac{6000}{(6000 + f_y)} = 0.0294$$

$$\text{최소 철근비} \quad \rho_{min} = \frac{0.8 * \sqrt{f_{ck}}}{f_y} = 0.0040 > \frac{14}{f_y} = 0.0035$$

$\therefore$ 최대 철근비 규정 만족!

$\therefore$ 최소 철근비 규정 만족!

$$\begin{aligned} \Phi V_c &= 0.8 * 0.53 * \sqrt{f_{ck}} * b_w * d \\ &= 69.63 \text{ t/m} > V_u = 54.05 \text{ t/m} \end{aligned}$$

$$\Phi V_c / 2 = 34.81 \text{ t/m} < V_u = 54.05 \text{ t/m}$$

$\therefore$ 전단철근을 배근해야 한다.

③ 벽체 변화부

(5 번 절점)

$$M_u = 100.170 \text{ t-m / m}, \quad V_u = 42.960 \text{ t/m}$$

$$\begin{aligned} d &= 44.71 \text{ cm}, & d_c &= 9.49 \text{ cm}, & b &= 100 \text{ cm} \\ f_{ck} &= 400 \text{ kgf/cm}^2 & f_y &= 4000 \text{ kgf/cm}^2 & \beta_1 &= 0.766 \end{aligned}$$

$$\Phi M_n = 0.9 * f_y * A_s * (d - a/2) \text{ 에서} \quad \Phi = 0.9 \text{ (Precast)}$$

$$A_{s,req} = \frac{M_u}{0.90 * f_y * (d - a/2)} \text{ 로 부터}$$

$$a = \frac{A_s * f_y}{0.85 * f_{ck} * b} = 8.046 \quad A_{s,req} = 68.39 \text{ cm}^2$$

$$\begin{aligned} \therefore H \ 22 \ @ \ 100 &= 3.871 * 10.00 \\ H \ 22 \ @ \ 100 &= 3.871 * 10.00 \text{ (2단배근)} \\ &= 77.42 \text{ cm}^2 \text{를 배근함.} \end{aligned}$$

OK!

$$\text{단면 철근비} \quad \rho = \frac{A_s}{b * d} = 0.0173$$

$$\text{최대 철근비} \quad \rho_{max} = 0.64 * \beta_1 * \frac{f_{ck}}{f_y} * \frac{6000}{(6000 + f_y)} = 0.0294$$

$$\text{최소 철근비} \quad \rho_{min} = \frac{0.8 * \sqrt{f_{ck}}}{f_y} = 0.0040 > \frac{14}{f_y} = 0.0035$$

∴ 최대 철근비 규정 만족!

∴ 최소 철근비 규정 만족!

$$\begin{aligned} \Phi V_c &= 0.8 * 0.53 * \sqrt{f_{ck}} * b_w * d \\ &= 37.91 \text{ t/m} < V_u = 42.96 \text{ t/m} \end{aligned}$$

$$\Phi V_c / 2 = 18.96 \text{ t/m} < V_u = 42.96 \text{ t/m}$$

∴ 전단철근을 배근해야 한다.

☐ 본체 전단면에 대한 단면력 검토

$f_{ck} = 400$ kgf/cm², $f_y = 4000$ kgf/cm², $K_1 = 0.766$ $b = 100$ cm

Node	사용 주철근				극한모멘트 t - m / m	두께 cm	d cm	d _c cm	a	A _{s,req} cm ²	공칭모멘트 t - m / m	철근비		결과
	①	②	간격	단								최대	최소	
1	22	22	100	2	0.000	50.0	40.5	9.49	0.000	0.00	100.183	만족	만족	OK
2	22	22	100	2	25.270	50.0	40.5	9.49	2.406	20.45	100.183	만족	만족	OK
3	22	22	100	2	52.770	50.0	40.5	9.49	5.160	43.86	100.183	만족	만족	OK
4	22	22	100	2	82.240	50.0	40.5	9.49	8.325	70.76	100.183	만족	만족	OK
5	22	22	100	2	99.920	54.2	44.7	9.49	8.853	75.25	111.893	만족	만족	OK
6	22	22	100	2	113.420	67.5	58.0	9.49	7.629	64.85	148.994	만족	만족	OK
7	22	22	100	2	127.910	91.6	82.1	9.49	5.875	49.94	216.158	만족	만족	OK
8	22	22	100	2	105.230	68.0	58.5	9.49	6.911	58.74	150.374	만족	만족	OK
9	22	22	100	2	80.490	55.3	45.8	9.49	6.825	58.01	114.947	만족	만족	OK
10	22	22	100	2	27.610	51.1	41.6	9.49	2.309	19.63	103.245	만족	만족	OK
11	19	19	100	2	12.850	50.0	40.8	9.18	1.387	11.79	77.248	만족	만족	OK
12	19	19	100	2	31.870	50.0	40.8	9.18	3.539	30.08	77.248	만족	만족	OK
13	19	19	100	2	45.410	50.0	40.8	9.18	4.991	42.42	77.248	만족	만족	OK
14	19	19	100	2	50.270	50.0	40.8	9.18	5.524	46.95	77.248	만족	만족	OK
15	19	19	100	2	45.400	50.0	40.8	9.18	4.995	42.46	77.248	만족	만족	OK
16	19	19	100	2	31.840	50.0	40.8	9.18	3.538	30.07	77.248	만족	만족	OK
17	19	19	100	2	8.280	50.0	40.8	9.18	1.160	9.86	77.248	만족	만족	OK
18	22	22	100	2	30.130	51.1	41.6	9.49	2.578	21.91	103.245	만족	만족	OK
19	22	22	100	2	80.600	55.3	45.8	9.49	6.826	58.02	114.947	만족	만족	OK
20	22	22	100	2	106.060	68.0	58.5	9.49	6.913	58.76	150.374	만족	만족	OK
21	22	22	100	2	128.050	91.6	82.1	9.49	5.876	49.95	216.158	만족	만족	OK
22	22	22	100	2	115.260	67.5	58.0	9.49	7.632	64.87	148.994	만족	만족	OK
23	22	22	100	2	100.170	54.2	44.7	9.49	8.941	76.00	111.893	만족	만족	OK
24	22	22	100	2	82.230	50.0	40.5	9.49	8.324	70.75	100.183	만족	만족	OK
25	22	22	100	2	52.770	50.0	40.5	9.49	5.160	43.86	100.183	만족	만족	OK
26	22	22	100	2	25.270	50.0	40.5	9.49	2.406	20.45	100.183	만족	만족	OK
27	22	22	100	2	0.000	50.0	40.5	9.49	0.000	0.00	100.183	만족	만족	OK
28	22	22	100	2	0.000	50.0	40.5	9.5	0.000	0.00	100.183	만족	만족	OK
29	22	22	100	2	25.190	50.0	40.5	9.49	0.000	0.00	100.183	만족	만족	OK
30	22	22	100	2	52.600	50.0	40.5	9.49	0.000	0.00	100.183	만족	만족	OK
31	22	22	100	2	81.980	50.0	40.5	9.49	0.000	0.00	100.183	만족	만족	OK
32	22	22	100	2	99.860	54.2	44.7	9.49	0.000	0.00	111.893	만족	만족	OK
33	22	22	100	2	114.890	67.5	58.0	9.49	0.000	0.00	148.994	만족	만족	OK

34	22	22	100	2	127.630	91.6	82.1	9.49	0.000	0.00	216.158	만족	만족	OK
35	22	22	100	2	105.610	68.0	58.5	9.49	0.000	0.00	150.374	만족	만족	OK
36	22	22	100	2	33.510	55.3	45.8	9.49	0.000	0.00	114.947	만족	만족	OK
37	22	22	100	2	8.890	51.1	41.6	9.49	0.000	0.00	103.245	만족	만족	OK
38	19	19	100	2	32.520	50.0	40.8	9.18	0.000	0.00	77.248	만족	만족	OK
39	19	19	100	2	46.120	50.0	40.8	9.18	0.000	0.00	77.248	만족	만족	OK
40	19	19	100	2	51.010	50.0	40.8	9.18	0.000	0.00	77.248	만족	만족	OK
41	19	19	100	2	46.160	50.0	40.8	9.18	0.000	0.00	77.248	만족	만족	OK
42	19	19	100	2	32.600	50.0	40.8	9.18	0.000	0.00	77.248	만족	만족	OK
43	19	19	100	2	17.030	50.0	40.8	9.18	0.000	0.00	77.248	만족	만족	OK
44	19	19	100	2	26.970	50.0	40.8	9.18	0.000	0.00	77.248	만족	만족	OK
45	22	22	100	2	79.960	51.1	41.6	9.49	0.000	0.00	103.245	만족	만족	OK
46	22	22	100	2	79.960	55.3	45.8	9.49	0.000	0.00	114.947	만족	만족	OK
47	22	22	100	2	104.770	68.0	58.5	9.49	0.000	0.00	150.374	만족	만족	OK
48	22	22	100	2	127.500	91.6	82.1	9.49	0.000	0.00	216.158	만족	만족	OK
49	22	22	100	2	113.060	67.5	58.0	9.49	0.000	0.00	148.994	만족	만족	OK
50	22	22	100	2	99.610	54.2	44.7	9.49	0.000	0.00	111.893	만족	만족	OK
51	22	22	100	2	81.980	50.0	40.5	9.49	0.000	0.00	100.183	만족	만족	OK
52	22	22	100	2	52.600	50.0	40.5	9.49	0.000	0.00	100.183	만족	만족	OK
53	22	22	100	2	25.190	50.0	40.5	9.49	0.000	0.00	100.183	만족	만족	OK
54	22	22	100	2	0.000	50.0	40.5	9.49	0.000	0.00	100.183	만족	만족	OK

④ 전단에 대한 검토 (5 번 절점)

$$V_u = 64.440 \text{ t/m} \quad \leftarrow -42.96 \times 1.5 = 64.44 \text{ PAB전체폭으로 계산함.}$$

$$d = 44.71 \text{ cm}, \quad d_c = 9.49 \text{ cm}, \quad b = 150 \text{ cm}$$

$$f_{ck} = 400 \text{ kgf/cm}^2, \quad f_y = 4000 \text{ kgf/cm}^2, \quad \beta_1 = 0.766$$

$$\Phi V_c = 0.8 * 0.53 * \sqrt{f_{ck}} * b_w * d$$

$$= 56.87 \text{ t/m} < V_u = 64.44 \text{ t/m}$$

$$\Phi V_c / 2 = 28.44 \text{ t/m} < V_u = 64.44 \text{ t/m}$$

∴ 전단 보강 철근을 배근해야 한다.

$$\frac{A_v}{s} > \frac{V_u - \Phi V_c}{\Phi f_y d} \text{ 에서, } \quad \text{철근의 간격 } s = 20 \text{ cm}$$

$$\text{전단철근량 } A_v = 1.06 \text{ cm}^2$$

$$\therefore H \quad 16 \quad - \quad 2 \quad \text{leg} \quad @ \quad 200$$

$$= 1.986 * 2 = 3.972 \text{ cm}^2 \text{를 배근.}$$

* Precast Arch Box 본체 전단면 전단 철근 검토

	V_u	$d_c(\text{cm})$	$d(\text{cm})$	ΦV_c	$\frac{1}{2} \Phi V_c$	결과	간격	필요철근량	사용철근량	ΦV_s	결과
1	55.43	9.49	40.5	51.53	25.76	전단보강	20	0.601	3.972	25.74	O.K
2	60.63	9.49	40.5	51.53	25.76	전단보강	20	1.404	3.972	25.74	O.K
3	65.45	9.49	40.5	51.53	25.76	전단보강	20	2.147	3.972	25.74	O.K
4	69.86	9.49	40.5	51.53	25.76	전단보강	20	2.827	3.972	25.74	O.K
5	63.53	9.49	44.7	56.87	28.44	전단보강	20	0.930	3.972	28.41	O.K
6	51.99	9.49	58.0	73.79	36.89	최소전단	20	1.750	3.972	36.87	O.K
7	80.97	9.49	82.1	104.44	52.22	최소전단	20	1.750	3.972	52.18	O.K
8	73.10	9.49	58.5	74.42	37.21	최소전단	20	1.750	3.972	37.18	O.K
9	73.86	9.49	45.8	58.27	29.14	전단보강	20	2.127	3.972	29.11	O.K
10	55.55	9.49	41.6	52.93	26.46	전단보강	20	0.393	3.972	26.44	O.K
11	41.00	9.18	40.8	51.92	25.96	최소전단	20	1.750	3.972	25.94	O.K
12	28.38	9.18	40.8	51.92	25.96	최소전단	20	1.750	3.972	25.94	O.K
13	17.15	9.18	40.8	51.92	25.96	필요없음	20	0.000	3.972	25.94	O.K
14	7.89	9.18	40.8	51.92	25.96	필요없음	20	0.000	3.972	25.94	O.K
15	17.18	9.18	40.8	51.92	25.96	필요없음	20	0.000	3.972	25.94	O.K
16	28.40	9.18	40.8	51.92	25.96	최소전단	20	1.750	3.972	25.94	O.K
17	41.01	9.18	40.8	51.92	25.96	최소전단	20	1.750	3.972	25.94	O.K
18	55.56	9.49	41.6	52.93	26.46	전단보강	20	0.395	3.972	26.44	O.K
19	73.88	9.49	45.8	58.27	29.14	전단보강	20	2.129	3.972	29.11	O.K
20	74.36	9.49	58.5	74.42	37.21	최소전단	20	1.750	3.972	37.18	O.K
21	79.43	9.49	82.1	104.44	52.22	최소전단	20	1.750	3.972	52.18	O.K
22	56.31	9.49	58.0	73.79	36.89	최소전단	20	1.750	3.972	36.87	O.K
23	64.44	9.49	44.7	56.87	28.44	전단보강	20	1.058	3.972	28.41	O.K
24	69.86	9.49	40.5	51.53	25.76	전단보강	20	2.827	3.972	25.74	O.K
25	65.45	9.49	40.5	51.53	25.76	전단보강	20	2.147	3.972	25.74	O.K
26	60.63	9.49	40.5	51.53	25.76	전단보강	20	1.404	3.972	25.74	O.K
27	55.43	9.49	40.5	51.53	25.76	전단보강	20	0.601	3.972	25.74	O.K
28	55.23	9.49	40.5	51.53	25.76	전단보강	20	0.571	3.972	25.74	O.K
29	60.44	9.49	40.5	51.53	25.76	전단보강	20	1.374	3.972	25.74	O.K
30	65.25	9.49	40.5	51.53	25.76	전단보강	20	2.117	3.972	25.74	O.K
31	69.66	9.49	40.5	51.53	25.76	전단보강	20	2.797	3.972	25.74	O.K
32	64.25	9.49	44.7	56.87	28.44	전단보강	20	1.031	3.972	28.41	O.K

33	56.37	9.49	58.0	73.79	36.89	최소전단	20	1.750	3.972	36.87	O.K
34	79.56	9.49	82.1	104.44	52.22	최소전단	20	1.750	3.972	52.18	O.K
35	67.64	9.49	58.5	74.42	37.21	최소전단	20	1.750	3.972	37.18	O.K
36	41.03	9.49	45.8	58.27	29.14	최소전단	20	1.750	3.972	29.11	O.K
37	27.14	9.49	41.6	52.93	26.46	최소전단	20	1.750	3.972	26.44	O.K
38	15.75	9.18	40.8	51.92	25.96	필요없음	20	0.000	3.972	25.94	O.K
39	6.63	9.18	40.8	51.92	25.96	필요없음	20	0.000	3.972	25.94	O.K
40	7.38	9.18	40.8	51.92	25.96	필요없음	20	0.000	3.972	25.94	O.K
41	17.13	9.18	40.8	51.92	25.96	필요없음	20	0.000	3.972	25.94	O.K
42	28.40	9.18	40.8	51.92	25.96	최소전단	20	1.750	3.972	25.94	O.K
43	41.04	9.18	40.8	51.92	25.96	최소전단	20	1.750	3.972	25.94	O.K
44	55.61	9.18	40.8	51.92	25.96	전단보강	20	0.564	3.972	25.94	O.K
45	73.94	9.49	41.6	52.93	26.46	전단보강	20	3.155	3.972	26.44	O.K
46	73.94	9.49	45.8	58.27	29.14	전단보강	20	2.137	3.972	29.11	O.K
47	73.20	9.49	58.5	74.42	37.21	최소전단	20	1.750	3.972	37.18	O.K
48	81.08	9.49	82.1	104.44	52.22	최소전단	20	1.750	3.972	52.18	O.K
49	52.05	9.49	58.0	73.79	36.89	최소전단	20	1.750	3.972	36.87	O.K
50	63.35	9.49	44.7	56.87	28.44	전단보강	20	0.905	3.972	28.41	O.K
51	69.66	9.49	40.5	51.53	25.76	전단보강	20	2.797	3.972	25.74	O.K
52	65.25	9.49	40.5	51.53	25.76	전단보강	20	2.117	3.972	25.74	O.K
53	60.44	9.49	40.5	51.53	25.76	전단보강	20	1.374	3.972	25.74	O.K
54	55.23	9.49	40.5	51.53	25.76	전단보강	20	0.571	3.972	25.74	O.K

3.5절에서 계산된 극한전단력에 1.5를 곱해서 검토함. B=150cm

배근 전단 철근	16	-	2	LEG	@	20
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Used $A_v = H16 \times 2 \text{ ea/m} = 3.972 \text{ cm}^2$ (간격 $s = 20.0 \text{ cm}$)

$\phi_s \cdot V_s = \phi_s \cdot A_v \cdot f_y \cdot D / (s \times 1000) = 25.739 \text{ tf}$ (D = 40.5 cm 기준)

$\phi_s \cdot V_n = \phi_s \cdot V_c + \phi_s \cdot V_s = 77.255 \text{ tf}$

⑤ 배력 철근량 검토 (1.1 일반사항 참조)

P.A.B 본체의 수축 및 온도 철근

$A_s = \rho \cdot b \cdot d = 0.002 \cdot 100 \cdot 50 = 10.00 \text{ cm}^2$

$A_{s(\text{현치부})} = 0.002 \cdot 100 \cdot 91.6 = 18.32 \text{ cm}^2$

배근된 배력 철근 : H19 @ 200(2단) = 28.66 cm^2

⑥ 우각부 검토

허용응력 설계

(7 번 절점)

(도로교 설계 기준 (2000) - p380)

$$M_0 = 74.880 \text{ t-m / m}$$

$$\begin{aligned} f_{t,max} &= \frac{5 \cdot M_0}{R^2 \cdot \omega} & R &= 91.60 \text{ cm} \\ & & \omega &= 100 \text{ cm} \\ &= \frac{5 * 7488000.00}{91.60^2 * 100} \\ &= 44.62 \text{ kgf/cm}^2 > 21.20 \text{ kgf/cm}^2 (1.06 * \sqrt{f_{ck}}) \\ &\text{(콘크리트 구조설계 기준 (1999) - 15.3 p243)} \end{aligned}$$

∴ 보강 철근을 배근 하여야 한다.

$$\begin{aligned} A_{s,req} &= \frac{2 \cdot M_0}{R \cdot 1800} \\ &= \frac{2 * 7488000.00}{91.60 * 1800} \\ &= 90.83 \text{ cm}^2/\text{m} \end{aligned}$$

보강 철근량

$$\begin{aligned} H \ 25 \ @ \ 100 &= 5.067 * 10.00 \\ H \ 25 \ @ \ 100 &= 5.067 * 10.00 \\ &= 101.34 \text{ cm}^2 \text{를 배근.} \end{aligned}$$

* P.A.B는 우각부에 정모멘트가 발생하지 않으므로 내측 인장 검토는 불필요함.

3) 사용성 검토 허용 응력 설계법 검토

(1) 균열 검토

① 슬래브 중앙 (14 번 절점)

$$M_{\text{Slab}} = 28.270 \text{ ton-m/m}$$

- 인장 철근의 제원

$$\begin{aligned} A_s &= 57.30 \text{ cm}^2, \quad d = 40.82 \text{ cm} \quad b = 100 \text{ cm} \\ \rho &= A_s / (b \cdot d) = 0.0140 \quad n = E_s / E_c = 7 \end{aligned}$$

$$\begin{aligned} k &= -n \cdot \rho + \sqrt{(n \cdot \rho)^2 + 2 \cdot n \cdot \rho} \\ &= 0.356 \end{aligned}$$

$$\begin{aligned} j &= 1 - k / 3 \\ &= 0.881 \end{aligned}$$

$$f_{s, \text{Slab}} = \frac{M_{\text{Slab}}}{A_s \cdot d \cdot j} = 1371 \text{ kg/cm}^2$$

$$\beta_c = 1.35 \quad d_c = 6.96 \quad A = 91.80$$

$$w = 1.08 \cdot \beta_c \cdot f_s \cdot \sqrt[3]{(d_c \cdot A)} \cdot 10^{-5} \text{ mm}$$

콘크리트 구조 설계 기준 (1999) 4.2.4

$$\therefore w = 0.172 \text{ mm}$$

$$\begin{aligned} \text{허용 균열 폭} &= 0.005 \quad * \quad \text{덮개} \quad (\text{해당 절점에서 최외곽주철근 기준 피복}) \\ &= 0.005 \quad * \quad 60 \quad = \quad 0.3 \text{ mm} \quad \therefore \text{O.K} \\ &(\text{콘크리트 구조 설계 기준 표 4.2.2}) \end{aligned}$$

② 현 치 부 (7 번 절점)

$$M_{\text{Slab}} = 74.880 \text{ ton-m/m}$$

- 인장 철근의 제원

$$\begin{aligned} A_s &= 77.42 \text{ cm}^2, \quad d = 82.11 \text{ cm} \quad b = 100 \text{ cm} \\ \rho &= A_s / (b \cdot d) = 0.0094 \quad n = E_s / E_c = 7 \end{aligned}$$

$$\begin{aligned} k &= -n \cdot \rho + \sqrt{(n \cdot \rho)^2 + 2 \cdot n \cdot \rho} \\ &= 0.303 \end{aligned}$$

$$\begin{aligned} j &= 1 - k / 3 \\ &= 0.899 \end{aligned}$$

$$f_{s, \text{Slab}} = \frac{M_{\text{Slab}}}{A_s \cdot d \cdot j} = 1310 \text{ kg/cm}^2$$

$$\beta_c = 1.35 \quad d_c = 7.11 \quad A = 94.90$$

$$w = 1.08 \cdot \beta_c \cdot f_s \cdot \sqrt[3]{(d_c \cdot A)} \cdot 10^{-5} \text{ mm}$$

콘크리트 구조 설계 기준 (1999) 4.2.4

$$\therefore w = 0.168 \text{ mm}$$

$$\begin{aligned} \text{허용 균열 폭} &= 0.005 \quad * \quad \text{덮개} \quad (\text{해당 절점에서 최외곽철근 기준 피복}) \\ &= 0.005 \quad * \quad 60 \quad = \quad 0.3 \text{ mm} \quad \therefore \underline{\underline{O.K}} \\ &(\text{콘크리트 구조 설계 기준 표 4.2.2}) \end{aligned}$$

③ 벽체 변화부 (5 번 절점)

$$M_{\text{Slab}} = 58.010 \text{ ton-m/m}$$

- 인장 철근의 제원

$$\begin{aligned} A_s &= 77.42 \text{ cm}^2, \quad d = 44.71 \text{ cm} \quad b = 100 \text{ cm} \\ \rho &= A_s / (b \cdot d) = 0.0173 \quad n = E_s / E_c = 7 \end{aligned}$$

$$\begin{aligned} k &= -n \cdot \rho + \sqrt{(n \cdot \rho)^2 + 2 \cdot n \cdot \rho} \\ &= 0.386 \end{aligned}$$

$$\begin{aligned} j &= 1 - k / 3 \\ &= 0.871 \end{aligned}$$

$$f_{s, \text{Slab}} = \frac{M_{\text{Slab}}}{A_s \cdot d \cdot j} = 1923 \text{ kg/cm}^2$$

$$\beta_c = 1.35 \quad d_c = 7.11 \quad A = 94.90$$

$$w = 1.08 \cdot \beta_c \cdot f_s \cdot \sqrt[3]{(d_c \cdot A)} \cdot 10^{-5} \text{ mm}$$

콘크리트 구조 설계 기준 (1999) 4.2.4

$$\therefore w = 0.246 \text{ mm}$$

$$\begin{aligned} \text{허용 균열 폭} &= 0.005 \quad * \quad \text{뒹개} \quad (\text{해당 절점에서 최외곽철근 기준 피복}) \\ &= 0.005 \quad * \quad 60 \quad = \quad 0.3 \text{ mm} \quad \underline{\underline{\therefore \text{O.K}}} \\ &(\text{콘크리트 구조 설계 기준 표 4.2.2}) \end{aligned}$$

본체 전체 균열 검토					균열제한폭 = 0.005 * 60 mm (뒹개) = 0.3 mm												
	모멘트 트 합	A _s 철근량	d _c cm	d cm	ρ	k	j	f _s kgf/cm ²	인장철근					d _c cm	A	균열 mm	결과
									H	H	간격	뒹개	개수				
1	0.00	77.42	9.49	40.51	0.019	0.401	0.866	0.00	22	22	100	60	20	7.11	94.9	0.00	Ok!
2	14.13	77.42	9.49	40.51	0.019	0.401	0.866	519.95	22	22	100	60	20	7.11	94.9	0.07	Ok!
3	29.97	77.42	9.49	40.51	0.019	0.401	0.866	1102.82	22	22	100	60	20	7.11	94.9	0.14	Ok!
4	47.32	77.42	9.49	40.51	0.019	0.401	0.866	1741.25	22	22	100	60	20	7.11	94.9	0.22	Ok!
5	57.86	77.42	9.49	44.71	0.017	0.386	0.871	1918.28	22	22	100	60	20	7.11	94.9	0.25	Ok!
6	65.96	77.42	9.49	58.01	0.013	0.349	0.884	1661.90	22	22	100	60	20	7.11	94.9	0.21	Ok!
7	74.79	77.42	9.49	82.11	0.009	0.303	0.899	1308.81	22	22	100	60	20	7.11	94.9	0.17	Ok!
8	61.09	77.42	9.49	58.51	0.013	0.348	0.884	1525.37	22	22	100	60	20	7.11	94.9	0.20	Ok!
9	46.33	77.42	9.49	45.81	0.017	0.382	0.873	1497.10	22	22	100	60	20	7.11	94.9	0.19	Ok!
10	15.36	77.42	9.49	41.61	0.019	0.396	0.868	549.42	22	22	100	60	20	7.11	94.9	0.07	Ok!
11	5.09	57.30	9.18	40.82	0.014	0.356	0.881	246.90	19	19	100	60	20	6.96	91.8	0.03	Ok!
12	18.18	57.30	9.18	40.82	0.014	0.356	0.881	881.85	19	19	100	60	20	6.96	91.8	0.11	Ok!
13	25.59	57.30	9.18	40.82	0.014	0.356	0.881	1241.28	19	19	100	60	20	6.96	91.8	0.16	Ok!
14	28.27	57.30	9.18	40.82	0.014	0.356	0.881	1371.28	19	19	100	60	20	6.96	91.8	0.17	Ok!
15	25.58	57.30	9.18	40.82	0.014	0.356	0.881	1240.80	19	19	100	60	20	6.96	91.8	0.16	Ok!
16	18.17	57.30	9.18	40.82	0.014	0.356	0.881	881.36	19	19	100	60	20	6.96	91.8	0.11	Ok!
17	6.71	57.30	9.18	40.82	0.014	0.356	0.881	325.48	19	19	100	60	20	6.96	91.8	0.04	Ok!
18	15.39	77.42	9.49	41.61	0.019	0.396	0.868	550.49	22	22	100	60	20	7.11	94.9	0.07	Ok!
19	46.40	77.42	9.49	45.81	0.017	0.382	0.873	1499.36	22	22	100	60	20	7.11	94.9	0.19	Ok!
20	61.60	77.42	9.49	58.51	0.013	0.348	0.884	1538.10	22	22	100	60	20	7.11	94.9	0.20	Ok!
21	74.88	77.42	9.49	82.11	0.009	0.303	0.899	1310.39	22	22	100	60	20	7.11	94.9	0.17	Ok!
22	67.08	77.42	9.49	58.01	0.013	0.349	0.884	1690.12	22	22	100	60	20	7.11	94.9	0.22	Ok!
23	58.01	77.42	9.49	44.71	0.017	0.386	0.871	1923.25	22	22	100	60	20	7.11	94.9	0.25	Ok!
24	47.32	77.42	9.49	40.51	0.019	0.401	0.866	1741.25	22	22	100	60	20	7.11	94.9	0.22	Ok!
25	29.96	77.42	9.49	40.51	0.019	0.401	0.866	1102.45	22	22	100	60	20	7.11	94.9	0.14	Ok!
26	14.13	77.42	9.49	40.51	0.019	0.401	0.866	519.95	22	22	100	60	20	7.11	94.9	0.07	Ok!
27	0.00	77.42	9.49	40.51	0.019	0.401	0.866	0.00	22	22	100	60	20	7.11	94.9	0.00	Ok!
28	0.00	77.42	9.49	40.51	0.019	0.401	0.866	0.00	22	22	100	60	20	7.11	94.9	0.00	Ok!
29	14.09	77.42	9.49	40.51	0.019	0.401	0.866	518.47	22	22	100	60	20	7.11	94.9	0.07	Ok!
30	29.89	77.42	9.49	40.51	0.019	0.401	0.866	1099.87	22	22	100	60	20	7.11	94.9	0.14	Ok!

31	47.20	77.42	9.49	40.51	0.019	0.401	0.866	1736.83	22	22	100	60	20	7.11	94.9	0.22	Ok!
32	57.87	77.42	9.49	44.71	0.017	0.386	0.871	1918.61	22	22	100	60	20	7.11	94.9	0.25	Ok!
33	66.91	77.42	9.49	58.01	0.013	0.349	0.884	1685.84	22	22	100	60	20	7.11	94.9	0.22	Ok!
34	74.67	77.42	9.49	82.11	0.009	0.303	0.899	1306.71	22	22	100	60	20	7.11	94.9	0.17	Ok!
35	61.39	77.42	9.49	58.51	0.013	0.348	0.884	1532.86	22	22	100	60	20	7.11	94.9	0.20	Ok!
36	15.15	77.42	9.49	45.81	0.017	0.382	0.873	489.55	22	22	100	60	20	7.11	94.9	0.06	Ok!
37	6.71	77.42	9.49	41.61	0.019	0.396	0.868	240.01	22	22	100	60	20	7.11	94.9	0.03	Ok!
38	18.48	57.30	9.18	40.82	0.014	0.356	0.881	896.40	19	19	100	60	20	6.96	91.8	0.11	Ok!
39	25.91	57.30	9.18	40.82	0.014	0.356	0.881	1256.80	19	19	100	60	20	6.96	91.8	0.16	Ok!
40	28.61	57.30	9.18	40.82	0.014	0.356	0.881	1387.77	19	19	100	60	20	6.96	91.8	0.17	Ok!
41	25.94	57.30	9.18	40.82	0.014	0.356	0.881	1258.26	19	19	100	60	20	6.96	91.8	0.16	Ok!
42	18.53	57.30	9.18	40.82	0.014	0.356	0.881	898.83	19	19	100	60	20	6.96	91.8	0.11	Ok!
43	5.43	57.30	9.18	40.82	0.014	0.356	0.881	263.39	19	19	100	60	20	6.96	91.8	0.03	Ok!
44	15.05	57.30	9.18	40.82	0.014	0.356	0.881	730.02	19	19	100	60	20	6.96	91.8	0.09	Ok!
45	46.08	77.42	9.49	41.61	0.019	0.396	0.868	1648.25	22	22	100	60	20	7.11	94.9	0.21	Ok!
46	46.08	77.42	9.49	45.81	0.017	0.382	0.873	1489.02	22	22	100	60	20	7.11	94.9	0.19	Ok!
47	60.87	77.42	9.49	58.51	0.013	0.348	0.884	1519.87	22	22	100	60	20	7.11	94.9	0.19	Ok!
48	74.60	77.42	9.49	82.11	0.009	0.303	0.899	1305.49	22	22	100	60	20	7.11	94.9	0.17	Ok!
49	65.79	77.42	9.49	58.01	0.013	0.349	0.884	1657.62	22	22	100	60	20	7.11	94.9	0.21	Ok!
50	57.71	77.42	9.49	44.71	0.017	0.386	0.871	1913.31	22	22	100	60	20	7.11	94.9	0.24	Ok!
51	47.20	77.42	9.49	40.51	0.019	0.401	0.866	1736.83	22	22	100	60	20	7.11	94.9	0.22	Ok!
52	29.89	77.42	9.49	40.51	0.019	0.401	0.866	1099.87	22	22	100	60	20	7.11	94.9	0.14	Ok!
53	14.09	77.42	9.49	40.51	0.019	0.401	0.866	518.47	22	22	100	60	20	7.11	94.9	0.07	Ok!
54	0.00	77.42	9.49	40.51	0.019	0.401	0.866	0.00	22	22	100	60	20	7.11	94.9	0.00	Ok!

(2) 상부 처짐 검토 (도로교 설계 기준 (2000) 4.4.9.5)

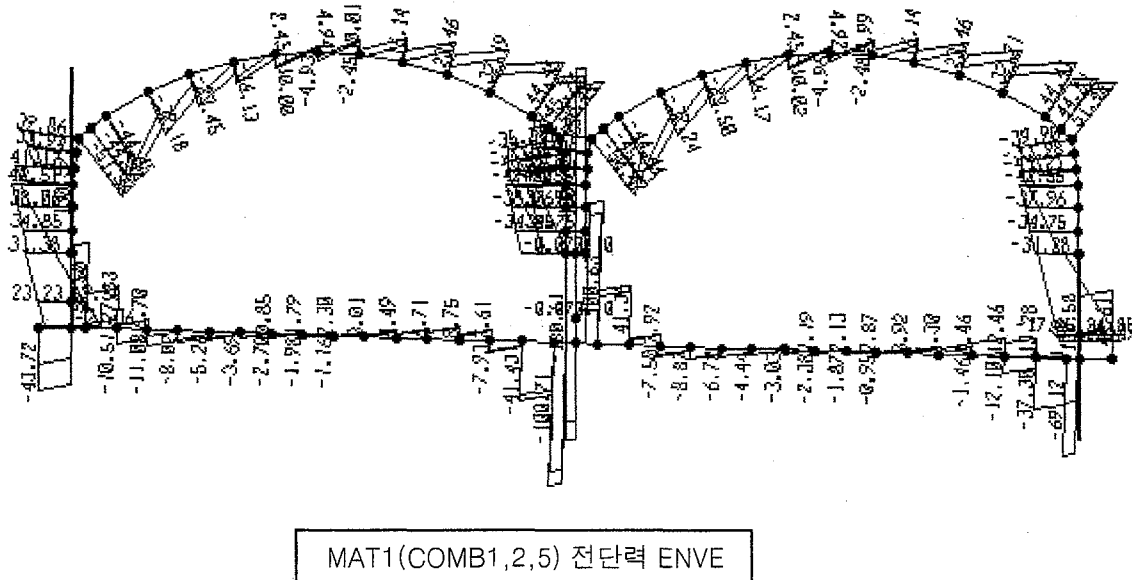
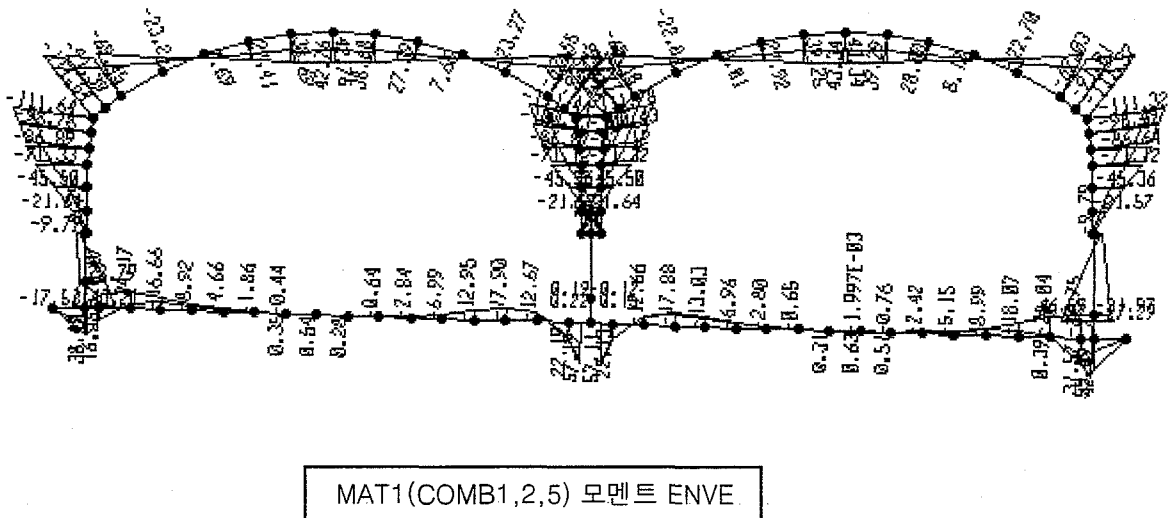
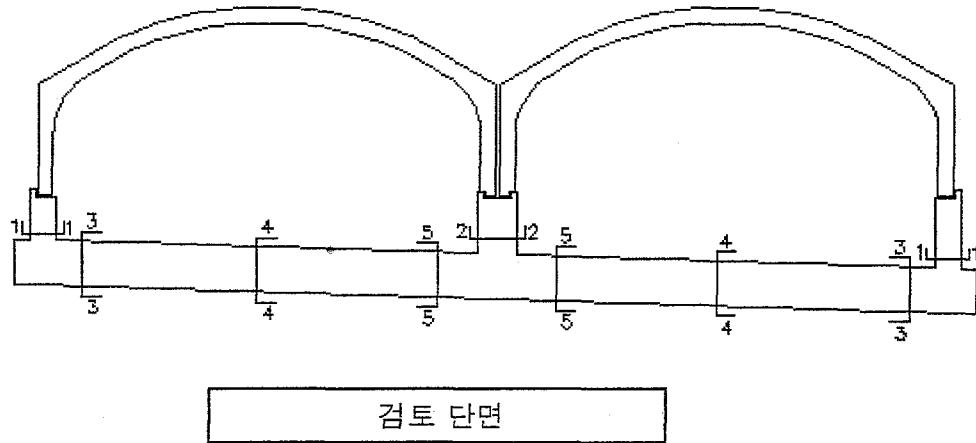
: 사용시 활하중이 작용하지 않으므로 고려하지 않음.

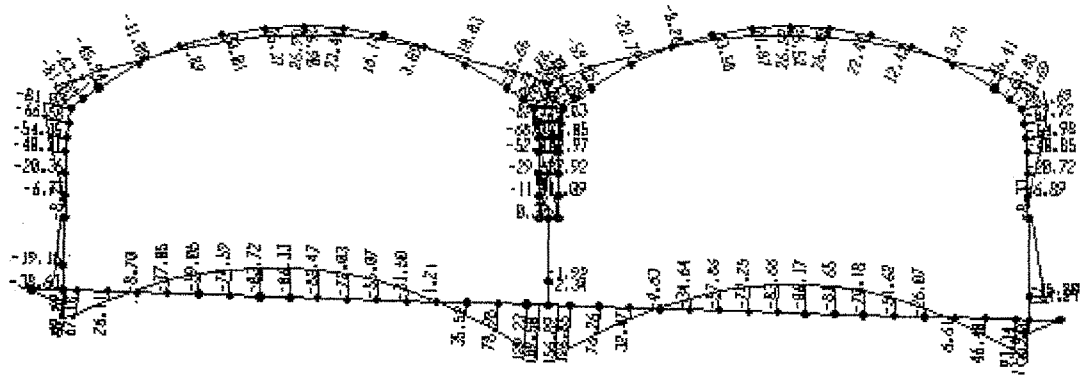
(3) 피로 검토

: P.A.B는 사용시 활하중이 작용하지 않으므로 고려하지 않고,
기초 슬래브에 작용하는 활하중(PL)에 의한 피로만 검토함.

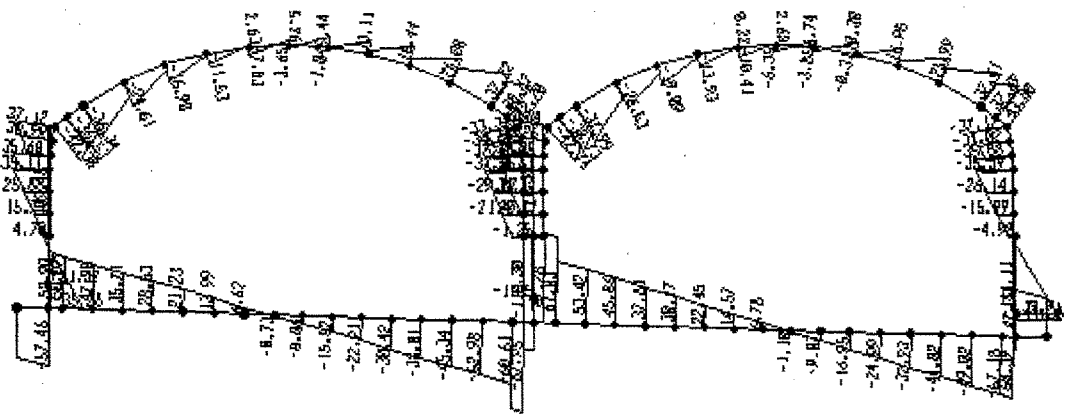
4.2 (8) 기초 슬래브 피로 검토 참조

4.2 현장타설 벽체 및 기초 검토

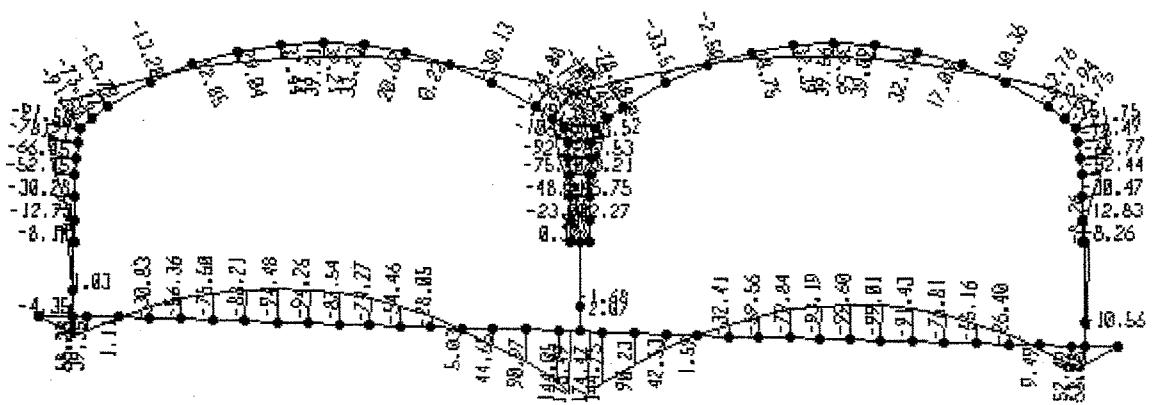




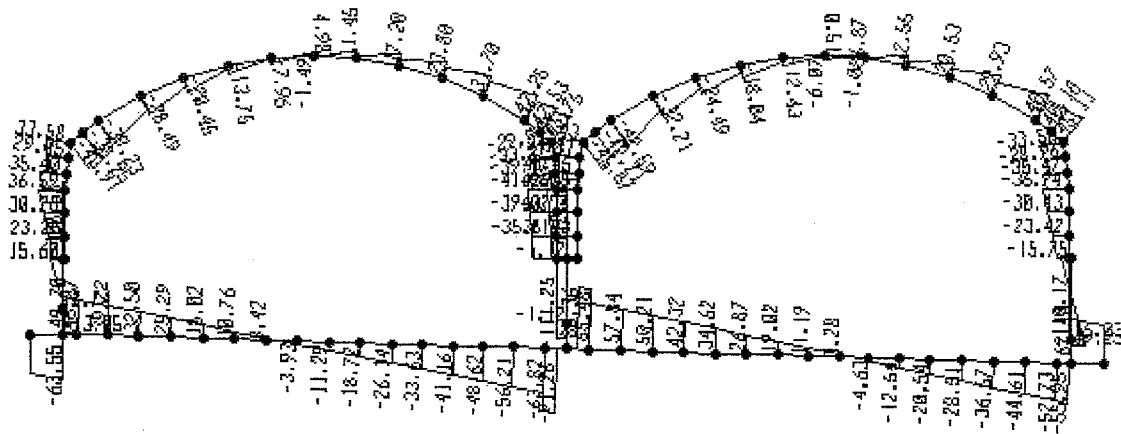
MAT3(COMB3) 모멘트 ENVE



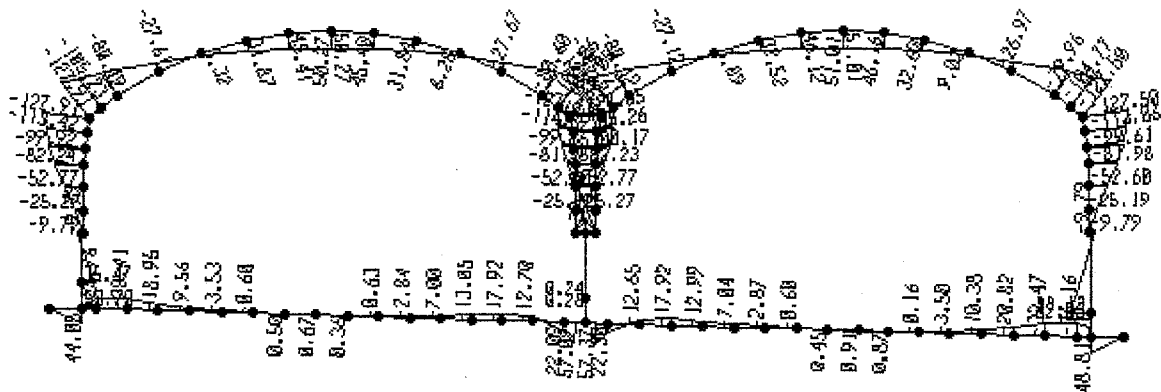
MAT3(COMB3) 전단력 ENVE



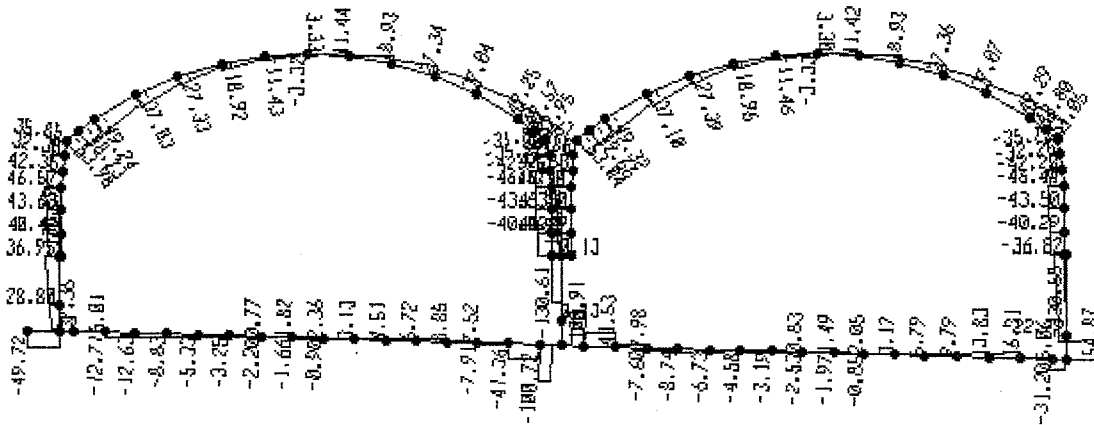
MAT4(COMB4) 모멘트 ENVE



MAT4(COMB4) 전단력 ENVE



MAT6(COMB6) 모멘트 ENVE



MAT6(COMB6) 전단력 ENVE

(1) 외측 벽체 검토 (절점102, 302번, 단면 1 - 1)

① 휨강도 검토

↳ 검토조건

$$f_{ck} = 270.0 \text{ kgf/cm}^2 \quad f_y = 4000.0 \text{ kgf/cm}^2$$

$$\beta_1 = 0.850 \quad \phi_b = 0.85 \quad \phi_s = 0.80$$

$$p_b = (0.85 \times \beta_1 \times f_{ck} / f_y) \times [6000 / (6000 + f_y)] = 0.02926$$

$$p_{max} = 0.75 \times p_b = 0.02195$$

$$p_{min} = \max(0.80 \sqrt{f_{ck}} / f_y, 14 / f_y) = 0.00350$$

$$\text{계수 모멘트 } M_u = 58.120 \text{ tf}\cdot\text{m}$$

$$\text{계수 전단력 } V_u = 39.910 \text{ tonf}$$

$$\text{단면의 두께 } H = 85.000 \text{ cm}$$

$$\text{단 면 폭 } B = 100.000 \text{ cm}$$

$$\text{유효 깊이 } D = 75.000 \text{ cm}$$

$$\text{피복 두께 } D_c = 10.000 \text{ cm}$$

소요등가응력깊이 $a = 4.084 \text{ cm}$ 로 가정

$$A_s = M_u / \{\phi_b \cdot f_y \cdot (D - a/2)\} = 23.430 \text{ cm}^2$$

$$a = (A_s \cdot f_y) / (0.85 \cdot f_{ck} \cdot B) = 4.084 \text{ cm} \quad \therefore \text{가정과 비슷함 O.K}$$

$$P_{req} = [M_u / \{\phi_b \cdot f_y \cdot (D - a/2)\}] / (B \cdot D) = 0.00312 \Rightarrow 4/3 P_{req} = 0.00417$$

$$\therefore \text{필요철근량 } req.A_s = P_{req} \times (B \cdot D) = 23.430 \text{ cm}^2$$

$$\text{Used } A_s = H22 @ 12.50 \text{ cm} \quad (D_c = 10.00 \text{ cm})$$

$$= 30.968 \text{ cm}^2 \quad \therefore P = A_s / (B \cdot D) = 0.00413$$

$$P_{min} \leq P \leq P_{max} \quad \therefore \text{O.K}$$

$$a = (A_s \cdot f_y) / (0.85 \cdot f_{ck} \cdot B) = 5.397 \text{ cm}$$

$$\phi M_n = \phi_b \cdot f_y \cdot A_s \cdot (D - a/2) = 7612687.000 \text{ kgf}\cdot\text{cm}$$

$$= 76.127 \text{ tf}\cdot\text{m} \geq M_u = 58.120 \text{ tf}\cdot\text{m} \quad \therefore \text{O.K}$$

↳ 전단력 검토

$$\phi_s \cdot V_c = \phi_s \cdot 0.53 \cdot \sqrt{f_{ck}} \cdot B \cdot d / 1000 = 52.253 \text{ tf}$$

$$\phi_s \cdot V_c = 52.253 \text{ tf} > V_u \quad \therefore \text{전단철근 필요없음.}$$

② 벽체 검토

↳ 벽체 검토 조건

$$f_{ck} = 270.0 \text{ kgf/cm}^2 \quad f_y = 4000.0 \text{ kgf/cm}^2$$

$$\phi_c = 0.70 \quad \phi_v = 0.80 \quad \alpha = 0.80$$

$$\text{극한 모멘트 } M_u = 58.120 \text{ tf}\cdot\text{m} \quad \text{극한 축력 } P_u = 136.820 \text{ tonf}$$

$$\text{단면의 두께 } H = 85.000 \text{ cm} \quad \text{단 위 폭 } B = 100.000 \text{ cm}$$

$$\text{유효 깊이 } D = 75.000 \text{ cm} \quad \text{피복 두께 } D_c = 10.000 \text{ cm}$$

$$\text{작용 편심 } e = 42.479 \text{ cm}$$

$$\text{인장축 철근 } A_{st} = 30.968 \text{ cm}^2$$

$$\text{1단 } (d_c = 10 \text{ cm}) : H 22 @ 12.5 \text{ cm}$$

$$\text{압축축 철근 } A_{sc} = 0.000 \text{ cm}^2$$

↳ 평형상태 검토

$$c = 6000 / (6000 + f_y) \cdot d = 45.000 \text{ cm}$$

$$k_1 = 0.850 \quad a = k_1 \cdot c = 38.25 \text{ cm}$$

$$C_{ck} = 0.85 \cdot f_{ck} \cdot B \cdot H = 1950750.0 \text{ kgf}$$

$$\begin{aligned} \text{소성중심 } x &= (C_{ck} \cdot H/2 + f_y \cdot A_{sc} \cdot d_c + f_y \cdot A_{st} \cdot d) / (C_{ck} + f_y \cdot A_{sc} + f_y \cdot A_{st}) \\ &= 44.44 \text{ cm} \end{aligned}$$

$$\text{콘크리트 } C_c = 0.85 \cdot f_{ck} \cdot a \cdot b = 877837.5 \text{ kgf}$$

$$\text{압축철근 } C_s = (f_s - 0.85 \cdot f_{ck}) \cdot A_{sc} = 0.0 \text{ kgf}$$

$$(\epsilon_{sc} > \epsilon_y \rightarrow f_s = f_y = 4000.00 \text{ kgf/cm}^2)$$

$$\text{인장철근 } T_s = f_y \cdot A_{st} = 123872.0 \text{ kgf}$$

$$\text{평형축력 } P_b = C_c + C_s - T_s = 753965.5 \text{ kgf}$$

$$\text{평형모멘트 } M_b = C_c(x - a/2) + C_s(x - d_c) + T_s(d - x) = 26008370.0 \text{ kgf}\cdot\text{m}$$

$$\text{평형편심 } e_b = M_b / P_b = 34.50 \text{ cm}$$

$$e \geq e_b \rightarrow \text{인장파괴영역}$$

↳ 기동 강도 검토

철근의 응력을 Trial & Error Method로 계산한다.

$$c = 35.42 \text{ cm로 가정하면.. } a = k_1 \cdot c = 30.11 \text{ cm}$$

$$\epsilon_{sc} = 0.0020 \quad f_s = 4000.00 \text{ kgf/cm}^2$$

$$\begin{aligned} P_n &= 0.85 \cdot f_{ck} \cdot a \cdot b + A_{sc} \cdot (f_{sc} - 0.85 \cdot f_{ck}) - A_{st} \cdot f_y \\ &= 567125.0 \text{ kgf} \end{aligned}$$

$$M_n = 0.85 \cdot f_{ck} \cdot a \cdot b \cdot (x - a/2) + A_{sc} \cdot f_{sc} \cdot (x - d_c) + A_{st} \cdot f_{st} \cdot (d - x)$$

$$= 24091180.0 \text{ kgf} \cdot \text{cm}$$

$$e' = M_n / P_n = 42.480 \text{ cm} \approx e = 42.479 \text{ cm} \rightarrow \text{say O.K.}$$

$$\phi P_n > 0.1 \cdot f_{ck} \cdot B \cdot H = 229500.0 \text{ kgf} \quad \dots \quad \phi = 0.70$$

$$\phi P_n = 396.988 \text{ tonf} \geq P_u = 136.820 \text{ tonf} \quad \therefore \text{O.K.}$$

$$\phi M_n = 168.638 \text{ tf} \cdot \text{m} \geq M_u = 58.120 \text{ tf} \cdot \text{m} \quad \therefore \text{O.K.}$$

③ 배력철근 검토 (1.1 일반사항 참조)

A. 수축 및 온도 철근

$$A_s = \rho \cdot b \cdot d = 0.002 \cdot 100 \cdot 75 = 15.00 \text{ cm}^2$$

$$\text{배력 철근 : H19 @ 150 (2단)} = 38.2 \text{ cm}^2$$

(2) 중앙부벽체 (절점 202번, 단면 2 - 2) - 가설시 검토

: P.A.B 가설중(한쪽에만 P.A.B를 설치하였을경우) 발생하는 모멘트에 대한 검토.

INPUTDATA : 가설.\$2K 참조

① 휨강도 검토

$$f_{ck} = 270.0 \text{ kgf/cm}^2 \quad f_y = 4000.0 \text{ kgf/cm}^2$$

$$\beta_1 = 0.850 \quad \phi_b = 0.85 \quad \phi_s = 0.80$$

$$\rho_b = (0.85 \times \beta_1 \times f_{ck} / f_y) \cdot [6000 / (6000 + f_y)] = 0.02926$$

$$\rho_{max} = 0.75 \times \rho_b = 0.02195$$

$$\rho_{min} = \max(0.80 \sqrt{f_{ck}} / f_y, 14 / f_y) = 0.00350$$

$$\text{계수 모멘트 } M_u = 5.122 \text{ tf} \cdot \text{m} \quad \text{계수 전단력 } V_u = 5.980 \text{ tonf}$$

$$\text{단면의 두께 } H = 130.000 \text{ cm} \quad \text{단 면 폭 } B = 100.000 \text{ cm}$$

$$\text{유효 깊이 } D = 120.000 \text{ cm} \quad \text{피복 두께 } D_c = 10.000 \text{ cm}$$

↳ 휨모멘트 검토

소요등가응력깊이 $a = 0.219 \text{ cm}$ 로 가정

$$A_s = M_u / \{ \phi_b \cdot f_y \cdot (D - a/2) \} = 1.257 \text{ cm}^2$$

$$a = (A_s \cdot f_y) / (0.85 \cdot f_{ck} \cdot B) = 0.219 \text{ cm} \quad \therefore \text{가정과 비슷함 O.K.}$$

$$P_{req} = [M_u / \{ \phi_b \cdot f_y \cdot (D - a/2) \}] / (B \cdot D) = 0.00010 \Rightarrow 4/3 P_{req} = 0.00014$$

$$\therefore \text{필요철근량 } \text{req.As} = \text{Preq} \times (B \cdot D) = 1.257 \text{ cm}^2$$

$$\text{Used As} = \text{H16 @ 12.50 cm} \quad (D_c = 10.00 \text{ cm})$$

$$= 15.888 \text{ cm}^2 \quad \therefore P = \text{As} / (B \cdot D) = 0.00132$$

$$4/3 \text{ Preq} \leq P \leq P_{\min} \quad \therefore \text{O.K}$$

$$a = (\text{As} \cdot f_y) / (0.85 \cdot f_{ck} \cdot B) = 2.769 \text{ cm}$$

$$\phi M_n = \phi b \cdot f_y \cdot \text{As} \cdot (D - a/2) = 6407511.000 \text{ kgf} \cdot \text{cm}$$

$$= 64.075 \text{ tf} \cdot \text{m} \geq M_u = 5.122 \text{ tf} \cdot \text{m} \quad \therefore \text{O.K}$$

▷ 전단력 검토

$$\phi_s \cdot V_c = \phi_s \cdot 0.53 \cdot \sqrt{f_{ck}} \cdot B \cdot d / 1000 = 83.604 \text{ tf}$$

$$\phi_s \cdot V_c = 83.604 \text{ tf} > V_u \quad \therefore \text{전단철근 필요없음.}$$

② 벽체 검토

$$f_{ck} = 270.0 \text{ kgf/cm}^2 \quad f_y = 4000.0 \text{ kgf/cm}^2$$

$$\phi_c = 0.70 \quad \phi_v = 0.80 \quad \alpha = 0.80$$

$$\text{극한 모멘트 } M_u = 5.122 \text{ tf} \cdot \text{m} \quad \text{극한 축력 } P_u = 26.299 \text{ tonf}$$

$$\text{단면의 두께 } H = 130.000 \text{ cm} \quad \text{단 위 폭 } B = 100.000 \text{ cm}$$

$$\text{유효 깊이 } D = 120.000 \text{ cm} \quad \text{피복 두께 } D_c = 10.000 \text{ cm}$$

$$\text{작용 편심 } e = 19.476 \text{ cm}$$

$$\text{인장축 철근 } A_{st} = 15.888 \text{ cm}^2$$

$$1 \text{ 단 } (d_c = 10 \text{ cm}) : \text{H 16 @ 12.5 cm}$$

$$\text{압축축 철근 } A_{sc} = 0.000 \text{ cm}^2$$

▷ 평형상태 검토

$$c = 6000 / (6000 + f_y) \cdot d = 72.000 \text{ cm}$$

$$k_1 = 0.850 \quad a = k_1 \cdot c = 61.20 \text{ cm}$$

$$C_{ck} = 0.85 \cdot f_{ck} \cdot B \cdot H = 2983500.0 \text{ kgf}$$

$$\text{소성중심 } x = (C_{ck} \cdot H/2 + f_y \cdot A_{sc} \cdot d_c + f_y \cdot A_{st} \cdot d) / (C_{ck} + f_y \cdot A_{sc} + f_y \cdot A_{st})$$

$$= 66.15 \text{ cm}$$

$$\text{콘크리트 } C_c = 0.85 \cdot f_{ck} \cdot a \cdot b = 1404540.0 \text{ kgf}$$

$$\text{압축철근 } C_s = (f_s - 0.85 \cdot f_{ck}) \cdot A_{sc} = 0.0 \text{ kgf}$$

$$(\epsilon_{sc} > \epsilon_y \rightarrow f_s = f_y = 4000.00 \text{ kgf/cm}^2)$$

$$\text{인장철근 } T_s = f_y \cdot A_{st} = 63552.0 \text{ kgf}$$

$$\text{평형축력 } P_b = C_c + C_s - T_s = 1340988.0 \text{ kgf}$$

$$\text{평형모멘트 } M_b = C_c(x - a/2) + C_s(x - d_c) + T_s(d - x) = 53349830.0 \text{ kgf} \cdot \text{cm}$$

$$\text{평형편심 } e_b = M_b / P_b = 39.78 \text{ cm}$$

$$e < e_b \text{ -----} > \text{ 압축 파괴영역}$$

↳ 기둥 강도 검토

$$e_{\min} = 13.10 \text{ cm} < e = 19.48 \text{ cm}$$

----> 철근의 응력을 Trial & Error Method로 계산한다.

$$c = 110.47 \text{ cm로 가정하면.. } a = k_1 \cdot c = 93.90 \text{ cm}$$

$$f_{sc} = 4000.00 \text{ kgf/cm}^2, \quad f_{st} = 517.4 \text{ kgf/cm}^2$$

$$P_n = 0.85 f_{ck} \cdot a \cdot B + A_{sc} \cdot f_{sc} - A_{st} \cdot f_{st} = 2146834.0 \text{ kgf}$$

$$M_n = 0.85 f_{ck} \cdot a \cdot B \cdot (x - a/2) + A_{sc} \cdot f_{sc} \cdot (x - d_{cc}) - A_{st} \cdot f_{st} \cdot (d - x) \\ = 41811240.0 \text{ kgf} \cdot \text{cm}$$

$$e' = M_n / P_n = 19.476 \text{ cm} \approx e = 19.476 \text{ cm} \text{ ----} > \text{ say O.K.}$$

$$\phi = 0.700$$

$$\phi P_n = 1502.784 \text{ tonf} \geq P_u = 26.299 \text{ tonf} \quad \therefore \text{O.K}$$

$$\phi M_n = 292.679 \text{ tf} \cdot \text{m} \geq M_u = 5.122 \text{ tf} \cdot \text{m} \quad \therefore \text{O.K}$$

↳ 전단력 검토

$$V_u = 5.980 \text{ tonf}$$

$$\phi V_c = \phi_s \cdot 0.53 \cdot (1 + 0.0071 \cdot P_u / A_g) \cdot \sqrt{f_{ck}} \cdot B \cdot D / 1000 = 84.805 \text{ tf}$$

$$\phi_s \cdot V_c = 84.805 \text{ tf} > V_u \quad \therefore \text{전단철근 필요없음.}$$

(3) 중앙부벽체 (절점 202번, 단면 2 - 2) - 완공후 검토

: 완공 후엔 좌우가 대칭인 구조물이므로 모멘트와 전단력은 발생하지 않고 축력만 발생한다.

그러므로 휨검토는 생략함.

해석 결과 COMB6.에서 $P_u = 268.82 \text{ tonf}$ 가 최대값임.

① 벽체 검토

$$f_{ck} = 270.0 \text{ kgf/cm}^2 \quad f_y = 4000.0 \text{ kgf/cm}^2$$

$$\phi_c = 0.70 \quad \phi_v = 0.80 \quad \alpha = 0.80$$

$$\text{극한 모멘트 } M_u = 0.000 \text{ tf} \cdot \text{m} \quad \text{극한 축력 } P_u = 268.820 \text{ tonf}$$

$$\text{단면의 두께 } H = 130.000 \text{ cm} \quad \text{단 위 폭 } B = 100.000 \text{ cm}$$

$$\text{유효 깊이 } D = 120.000 \text{ cm} \quad \text{피복 두께 } D_c = 10.000 \text{ cm}$$

$$\text{작용 편심 } e = 0.000 \text{ cm}$$

인장축 철근 $A_{st} = 15.888 \text{ cm}^2$

1단 ($d_c = 10 \text{ cm}$) : H 16 @ 12.5 cm

압축축 철근 $A_{sc} = 0.000 \text{ cm}^2$

▷ 평형상태 검토

$$c = 6000 / (6000 + f_y) \cdot d = 72.000 \text{ cm}$$

$$k_1 = 0.850 \quad a = k_1 \cdot c = 61.20 \text{ cm}$$

$$C_{ck} = 0.85 \cdot f_{ck} \cdot B \cdot H = 2983500.0 \text{ kgf}$$

$$\begin{aligned} \text{소성중심 } x &= (C_{ck} \cdot H/2 + f_y \cdot A_{sc} \cdot d_c + f_y \cdot A_{st} \cdot d) / (C_{ck} + f_y \cdot A_{sc} + f_y \cdot A_{st}) \\ &= 66.15 \text{ cm} \end{aligned}$$

$$\text{콘크리트 } C_c = 0.85 \cdot f_{ck} \cdot a \cdot b = 1404540.0 \text{ kgf}$$

$$\text{압축철근 } C_s = (f_s - 0.85 \cdot f_{ck}) \cdot A_{sc} = 0.0 \text{ kgf}$$

$$(\epsilon_{sc} > \epsilon_y \rightarrow f_s = f_y = 4000.00 \text{ kgf/cm}^2)$$

$$\text{인장철근 } T_s = f_y \cdot A_{st} = 63552.0 \text{ kgf}$$

$$\text{평형축력 } P_b = C_c + C_s - T_s = 1340988.0 \text{ kgf}$$

$$\text{평형모멘트 } M_b = C_c(x - a/2) + C_s(x - d_c) + T_s(d - x) = 53349830.0 \text{ kgf} \cdot \text{m}$$

$$\text{평형편심 } e_b = M_b / P_b = 39.78 \text{ cm}$$

$$e < e_b \rightarrow \text{압축파괴영역}$$

▷ 기동 강도 검토

$$e_{\min} = 13.10 \text{ cm} \geq e = 0.00 \text{ cm}$$

편심이 최소편심보다 작으므로..

$$P_n = 0.85 \cdot f_{ck} \cdot (A_g - A_s) + f_y \cdot A_s = 3043406.0 \text{ kgf}$$

$$M_n = P_n \cdot e_{\min} = 39877350.0 \text{ kgf} \cdot \text{cm}$$

$$\phi = 0.700 \quad \alpha = 0.800$$

$$\alpha \phi P_n = 1704.307 \text{ tonf} \geq P_u = 268.820 \text{ tonf} \quad \therefore \text{O.K}$$

$$\phi M_n = 223.313 \text{ tf} \cdot \text{m} \geq M_u = 0.000 \text{ tf} \cdot \text{m} \quad \therefore \text{O.K}$$

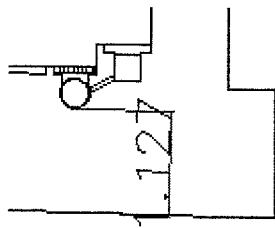
② 배력 철근 검토

A. 수축 및 온도 철근

$$\begin{aligned} A_s &= \rho \cdot b \cdot d \quad 0.002 \quad * \quad 100 \quad * \quad 130 \\ &= 26.00 \text{ cm}^2 \end{aligned}$$

$$\text{배력 철근 : H19 @ 150 (2단)} = 38.2 \text{ cm}^2$$

(4) 바닥 슬래브 (절점 403, 435번, 단면 3 - 3)



단면 3 - 3 형상

$$M_u = 93.340 \text{ t-m / m}, \quad V_u = 69.120 \text{ t/m}$$

$$d = 102.70 \text{ cm}, \quad d_c = 10.00 \text{ cm},$$

$$b = 100 \text{ cm}$$

$$f_{ck} = 270 \text{ kgf/cm}^2, \quad f_y = 4000 \text{ kgf/cm}^2$$

$$\beta_1 = 0.857$$

$$\Phi M_n = 0.85 * f_y * A_s * (d - a/2) \text{ 에서}$$

$$A_{s,req} = \frac{M_u}{0.85 * f_y * (d - a/2)} \text{ 로 부터}$$

$$a = \frac{A_s * f_y}{0.85 * f_{ck} * b} = 4.770$$

$$A_{s,req} = 27.37 \text{ cm}^2$$

$$\therefore H 25 @ 125 = 5.067 * 8.00$$

$$= 40.54 \text{ cm}^2 \text{를 배근함.}$$

OK!

$$\text{단면 철근비} \quad \rho = \frac{A_s}{b \cdot d} = 0.0039$$

$$\text{최대 철근비} \quad \rho_{max} = 0.64 * \beta_1 * \frac{f_{ck}}{f_y} * \frac{6000}{(6000 + f_y)} = 0.0222$$

$$\text{최소 철근비} \quad \rho_{min} = \frac{0.8 \cdot \sqrt{f_{ck}}}{f_y} = 0.0033 < \frac{14}{f_y} = 0.0035$$

$\therefore$ 최대 철근비 규정 만족!

$\therefore$ 최소 철근비 규정 만족!

$$\begin{aligned} \Phi V_c &= 0.8 * 0.53 * \sqrt{f_{ck}} * b_w * d \\ &= 71.55 \text{ t/m} > V_u = 69.12 \text{ t/m} \end{aligned}$$

$$\Phi V_c / 2 = 35.78 \text{ t/m} < V_u = 69.12 \text{ t/m}$$

$\therefore$ 전단철근을 배근해야 한다.

(5) 바닥 슬래브 (절점 428번, 단면 4 - 4)

$$M_u = 99.600 \text{ t-m / m}, \quad V_u = 3.310 \text{ t/m}$$

$$\begin{aligned} d &= 130.00 \text{ cm}, & d_c &= 10.00 \text{ cm}, & b &= 100 \text{ cm} \\ f_{ck} &= 270 \text{ kgf/cm}^2 & f_y &= 4000 \text{ kgf/cm}^2 & \beta_1 &= 0.857 \end{aligned}$$

$\Phi M_n = 0.85 * f_y * A_s * (d - a/2)$ 에서

$$A_{s,req} = \frac{M_u}{0.85 * f_y * (d - a/2)} \text{ 로 부터}$$

$$a = \frac{A_s * f_y}{0.85 * f_{ck} * b} = 3.988 \quad A_{s,req} = 22.88 \text{ cm}^2$$

$$\therefore H \ 25 \ @ \ 125 = 5.067 * 8.00$$

$$= 40.54 \text{ cm}^2 \text{를 배근함.}$$

OK!

$$\text{단면 철근비} \quad \rho = \frac{A_s}{b * d} = 0.0031$$

$$\text{최대 철근비} \quad \rho_{max} = 0.64 * \beta_1 * \frac{f_{ck}}{f_y} * \frac{6000}{(6000 + f_y)} = 0.0222$$

$$\text{최소 철근비} \quad \rho_{min} = \frac{0.8 * \sqrt{f_{ck}}}{f_y} = 0.0033 < \frac{14}{f_y} = 0.0035$$

$\therefore$ 최대 철근비 규정 만족!

$\therefore$ 최소 철근비 규정 불만족!

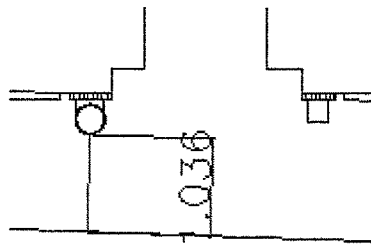
* 배근된 철근량(40.54cm²)이 필요한 철근량(22.88cm²)의 4/3이상이므로 최소철근비를 따르지 않아도 됨.

$$\begin{aligned} \Phi V_c &= 0.8 * 0.53 * \sqrt{f_{ck}} * b_w * d \\ &= 90.57 \text{ t/m} > V_u = 3.31 \text{ t/m} \end{aligned}$$

$$\Phi V_c / 2 = 45.29 \text{ t/m} > V_u = 3.31 \text{ t/m}$$

$\therefore$ 전단 철근을 배근하지 않아도 된다.

(6) 바닥 슬래브 (절점 418, 420번, 단면 5 - 5)



단면 5 - 5 형상

$$M_u = 144.750 \text{ t-m / m}, \quad V_u = 100.910 \text{ t/m}$$

$$\begin{aligned} d &= 93.60 \text{ cm}, & d_c &= 10.00 \text{ cm}, & b &= 100 \text{ cm} \\ f_{ck} &= 270 \text{ kgf/cm}^2 & f_y &= 4000 \text{ kgf/cm}^2 & \beta_1 &= 0.857 \end{aligned}$$

$$\Phi M_n = 0.85 * f_y * A_s * (d - a/2) \text{ 에서}$$

$$A_{s,req} = \frac{M_u}{0.85 * f_y * (d - a/2)} \text{ 로 부터}$$

$$a = \frac{A_s * f_y}{0.85 * f_{ck} * b} = 8.295$$

$$A_{s,req} = 47.59 \text{ cm}^2$$

$$\therefore H \ 29 \ @ \ 125 = 6.424 * 8.00$$

$$= 51.39 \text{ cm}^2 \text{를 배근함.}$$

OK!

$$\text{단면 철근비} \quad \rho = \frac{A_s}{b * d} = 0.0055$$

$$\text{최대 철근비} \quad \rho_{max} = 0.64 * \beta_1 * \frac{f_{ck}}{f_y} * \frac{6000}{(6000 + f_y)} = 0.0222$$

$$\text{최소 철근비} \quad \rho_{min} = \frac{0.8 * \sqrt{f_{ck}}}{f_y} = 0.0033 < \frac{14}{f_y} = 0.0035$$

$\therefore$ 최대 철근비 규정 만족!

$\therefore$ 최소 철근비 규정 만족!

$$\Phi V_c = 0.8 * 0.53 * \sqrt{f_{ck}} * b_w * d$$

$$= 65.21 \text{ t/m} < V_u = 100.91 \text{ t/m}$$

$$\Phi V_c / 2 = 32.61 \text{ t/m} < V_u = 100.91 \text{ t/m}$$

$\therefore$ 전단철근을 배근해야 한다.

* 현장타설 기초 바닥 전단면 전단 철근 검토

	V_u	$d_c(\text{cm})$	$d(\text{cm})$	ΦV_c	$\frac{1}{2} \Phi V_c$	결과	간격	필요철근량	사용철근량	ΦV_s	결과
403	42.83	10.0	130.0	90.57	45.29	필요없음	40	0.000	3.972	41.31	O.K
404	37.58	10.0	130.0	90.57	45.29	필요없음	40	0.000	3.972	41.31	O.K
405	53.04	10.0	130.0	90.57	45.29	최소전단	40	3.500	3.972	41.31	O.K
406	45.09	10.0	130.0	90.57	45.29	필요없음	40	0.000	3.972	41.31	O.K
407	27.35	10.0	130.0	90.57	45.29	필요없음	40	0.000	3.972	41.31	O.K
408	18.09	10.0	130.0	90.57	45.29	필요없음	40	0.000	3.972	41.31	O.K
409	10.50	10.0	130.0	90.57	45.29	필요없음	40	0.000	3.972	41.31	O.K
410	4.42	10.0	130.0	90.57	45.29	필요없음	40	0.000	3.972	41.31	O.K
411	4.92	10.0	130.0	90.57	45.29	필요없음	40	0.000	3.972	41.31	O.K
412	11.42	10.0	130.0	90.57	45.29	필요없음	40	0.000	3.972	41.31	O.K
413	18.93	10.0	130.0	90.57	45.29	필요없음	40	0.000	3.972	41.31	O.K
414	27.36	10.0	130.0	90.57	45.29	필요없음	40	0.000	3.972	41.31	O.K
415	37.07	10.0	130.0	90.57	45.29	필요없음	40	0.000	3.972	41.31	O.K
416	49.29	10.0	130.0	90.57	45.29	최소전단	40	3.500	3.972	41.31	O.K
417	49.29	10.0	130.0	90.57	45.29	최소전단	40	3.500	3.972	41.31	O.K
418	48.80	10.0	130.0	90.57	45.29	최소전단	40	3.500	3.972	41.31	O.K
420	34.70	10.0	130.0	90.57	45.29	필요없음	40	0.000	3.972	41.31	O.K
421	42.23	10.0	130.0	90.57	45.29	필요없음	40	0.000	3.972	41.31	O.K
422	46.44	10.0	130.0	90.57	45.29	최소전단	40	3.500	3.972	41.31	O.K
423	43.50	10.0	130.0	90.57	45.29	필요없음	40	0.000	3.972	41.31	O.K
424	40.29	10.0	130.0	90.57	45.29	필요없음	40	0.000	3.972	41.31	O.K
425	36.82	10.0	130.0	90.57	45.29	필요없음	40	0.000	3.972	41.31	O.K
426	36.95	10.0	130.0	90.57	45.29	필요없음	40	0.000	3.972	41.31	O.K
427	28.80	10.0	130.0	90.57	45.29	필요없음	40	0.000	3.972	41.31	O.K
428	36.82	10.0	130.0	90.57	45.29	필요없음	40	0.000	3.972	41.31	O.K
429	39.91	10.0	130.0	90.57	45.29	필요없음	40	0.000	3.972	41.31	O.K
430	56.08	10.0	130.0	90.57	45.29	최소전단	40	3.500	3.972	41.31	O.K
431	63.55	10.0	130.0	90.57	45.29	최소전단	40	3.500	3.972	41.31	O.K
432	59.50	10.0	130.0	90.57	45.29	최소전단	40	3.500	3.972	41.31	O.K
433	42.96	10.0	130.0	90.57	45.29	필요없음	40	0.000	3.972	41.31	O.K
434	35.76	10.0	130.0	90.57	45.29	필요없음	40	0.000	3.972	41.31	O.K
435	28.53	10.0	130.0	90.57	45.29	필요없음	40	0.000	3.972	41.31	O.K

* 배근된 전단철근

16	-	2	LEG	@	40
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$$\text{Used } A_v = H16 \times 2 \text{ ea/m} = 3.972 \text{ cm}^2 \quad (\text{간격 } s = 40.0 \text{ cm}) \quad (\phi_s = 0.80)$$

$$\phi_s \cdot V_s = \phi_s \cdot A_v \cdot f_y \cdot D / (s \times 1000) = 41.309 \text{ tf}$$

$$\phi_s \cdot V_n = \phi_s \cdot V_c + \phi_s \cdot V_s = 90.57 + 41.309 = 131.880 \text{ tf}$$

* 현장 타설 기초 슬래브 배력 철근량 검토 (1.1 일반사항 참조)

A. 도로교설계기준 4.7 바닥판 적용시.

$$= 0.307 \times 47.59 = 14.62 \text{ cm}^2$$

($A_{s, \text{req}} = 36.42 \text{ cm}^2$ 가 최대, 절점 418번)

B. P.A.B 본체의 수축 및 온도 철근

$$A_s = \rho \times b \times d = 0.002 \times 100 \times 140 = 28.00 \text{ cm}^2$$

배근된 배력 철근 : H19 @ 150(2단) = 38.2 cm²

(7) 기초 우각부 검토 (402, 436 번 절점)

① 외측 인장 검토

콘크리트 기준강도 $f_{ck} = 270 \text{ kg/cm}^2$

콘크리트 허용인장응력 $f_{ta} = 1.06 \sqrt{f_{ck}} = 17.42 \text{ kg/cm}^2$

철근항복강도 $f_y = 4000 \text{ kg/cm}^2$

철근허용응력 $f_{sa} = 1800 \text{ kg/cm}^2$

설계단면력 : 사용하중 모멘트 $M_o = 27.49 \text{ t.m}$

구조물단면 : 슬라브 두께 $A = 140.0 \text{ cm}$ 벽 두께 $B = 85.0 \text{ cm}$

현치수직거리 $C = 0.0 \text{ cm}$ 수평거리 $D = 0.0 \text{ cm}$

사용철근 : 2 - D19@125 ($A_g = 45.84 \text{ cm}^2$)

$a = B = 85.0 \text{ cm}$ $b = A = 140.0 \text{ cm}$

$R = \sqrt{(a^2 + b^2)} = 163.8 \text{ cm}$

$$\text{최대인장응력 } \sigma_{\max} = 5 \cdot M_o / (R^2 \cdot B) = 5.12 \text{ kg/cm}^2 < \sigma_{ta} \dots \text{철근보강 필요없음}$$

② 내측 인장 검토 (절점 403, 435번) (참고도서 : 구조물 설계 기준 - 교량편, P.4-26)

* 435번 절점에서 내측인장을 발생시키는 모멘트가 15.76 t-m (COMB.10) 가 발생하며,
해석에 필요한 단면은 불리한 경우인 벽체를 기준으로 해석함.

$$A_{st} = T / F_{sa} \quad , \quad T = \sqrt{2} \times T_h$$

A_{st} = 스트럽 필요 단면적

T = 대각선 방향의 인장응력의 합력 (kgf)

T_h = 수평 부재 또는 연직부재에 작용하는 인장응력의 합력 (kgf)

$$T_h = f_s \times A_s$$

$$f_s = M / (A_s (d - x/3)) \quad M : \text{수평 또는 연직 부재에 발생한 모멘트 (tf - m)}$$

$$x = k d$$

$$k = -np + \sqrt{(np)^2 + 2np}$$

$$p = A_s / (bd)$$

$$A_s = H22 - 8EA = 30.97 \text{ cm}^2$$

$$d = 85 - 10 = 75 \text{ cm}$$

$$b = 100 \text{ cm}$$

$$p = 30.97 / (100 \times 75) = 0.00413$$

$$n = E_s / E_c = 2000000 / 246475 = 8.11 = 8 \text{ (가장 가까운 정수 적용)}$$

$$k = -np + \sqrt{(np)^2 + 2np} = 8 \times 0.00413 + \sqrt{(8 \times 0.00413)^2 + 2 \times 8 \times 0.00413} = 0.2922$$

$$x = k d = 0.2922 \times 75 = 21.915$$

$$f_s = M / (A_s (d - x/3)) = 15.76 \times 10^5 / (30.97 (75 - 21.915/3)) = 751.724 \text{ kg/cm}^2$$

$$T_h = f_s \times A_s = 751.724 \times 30.97 = 23280.89 \text{ kgf}$$

$$T = \sqrt{2} \times T_h = \sqrt{2} \times 19927.65 = 32924.15 \text{ kgf}$$

$$A_{st} = T / f_{sa} = 31963.05 / 1500 = 21.95 \text{ cm}^2$$

$$\therefore \text{사용 스트럽 H19 - 8EA} = 22.92 \text{ cm}^2$$

(8) 기초 슬래브 피로 검토

① 기초 슬래브에 작용하는 활하중에 의한 피로 검토

- * 피로에 대한 안전성을 검토 할 경우, 충격을 포함한 사용 활하중에 의한 철근의 응력 범위가 피로를 고려하지 않아도 되는 철근의 응력 범위 이내에 들면 피로에 대하여 검토 할 필요가 없다.

(콘크리트 구조 설계 기준 4.4.2 (1) 참조)

- * 피로를 고려하지 않아도 되는 철근의 인장 및 압축 범위

SD 40 (1500 kg/cm²)

	기초슬래브	단위
$f_{s,max}$	194	kg/cm ²
$f_{s,min}$	223	kg/cm ²
Δf	-29	kg/cm ²
검토 여부	필요없음	

(콘크리트 구조 설계 기준 4.4.2 '피로에 대한 검토' 참조)

기초 슬래브에 작용하는 활하중에 의한 모멘트의 변화량이 가장 많은 418번 절점을 기준으로 검토함.

Mcomb7. = 11.99 ton-m/m Mcomb8. = 13.77 ton-m/m

- 인장 철근의 제원

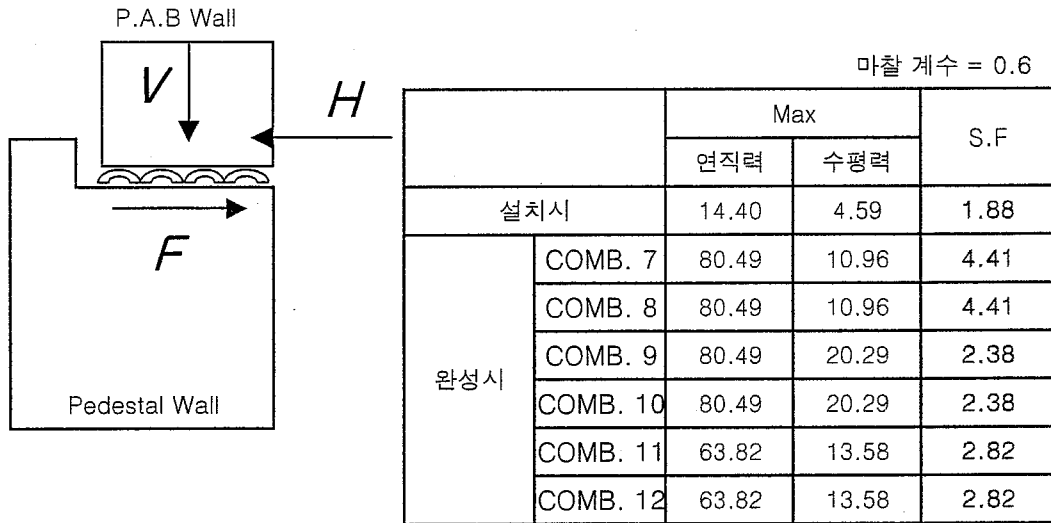
$$\begin{aligned}
 A_s &= 51.39 \text{ cm}^2, & d &= 130.00 \text{ cm} & b &= 100 \text{ cm} \\
 \rho &= A_s / (b * d) & &= 0.0040 & n &= E_s / E_c = 8 \\
 k &= -n \cdot \rho + \sqrt{((n \cdot \rho)^2 + 2 \cdot n \cdot \rho)} & & & j &= 1 - k / 3 \\
 &= 0.222 & & & &= 0.926
 \end{aligned}$$

$$f_{s,max} = \frac{M_{max}}{A_s * d * j} = 194 \text{ kg/cm}^2$$

$$f_{s,min} = \frac{M_{min}}{A_s * d * j} = 223 \text{ kg/cm}^2$$

4.3 P.A.B 벽체 연결부 검토

① P.A.B & 현장 타설 벽체 연결부 SLIDING검토



* 5. SAP2000 OUTPUT 참조

P.A.B 벽체로 부터 전달되는 수평력에 비해 마찰력이 커 SLIDING에 안전함!

② P.A.B & 현장 타설 벽체 연결부 전단마찰 검토

$$f_{ck} = 270 \text{ kg/cm}^2$$

$$f_y = 4000 \text{ kg/cm}^2$$

수평력	마찰저항력
$H_u' = H_u / 0.8$	$F = \mu \cdot V$
(t/m)	(t/m)
25.36	48.29

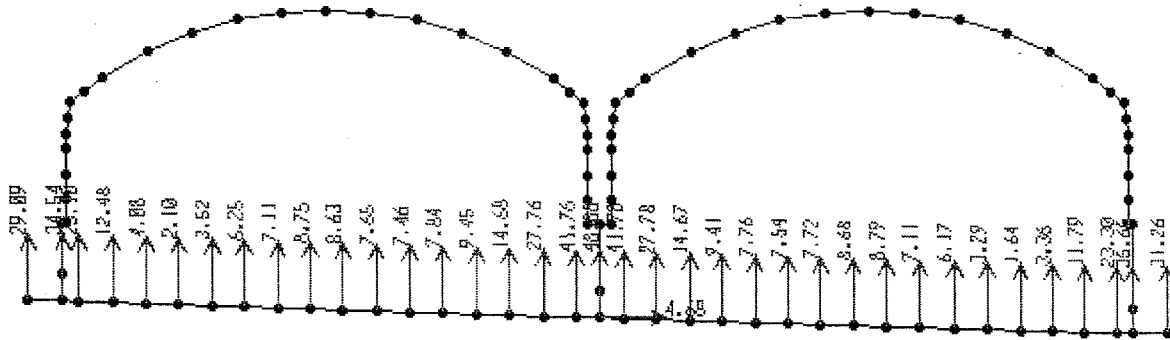
$$\Phi_v = 0.8$$

$$\text{마찰계수} = 0.6$$

$$\mu = 1.0 \cdot \lambda, \lambda = 1.0$$

∴ 마찰저항력 > 수평력 이므로 전단마찰 철근 필요 없음.

4.4 지지력 검토



COMB 10. Spring force

기초 저면에서의 최대반력은 COMB.10 (활하중 고려시)에서 중앙부 벽체 하면에서
약 48.88 ton/m²의 결과를 보이고 있음.

($q_{\max} = 48.88 \text{ tonf/m}^2 < q_a = 85 \text{ tonf/m}^2$) $\therefore$ O.K

* 허용지지력은 "암반에 지지되는 직접기초의 허용지지력" 참조

4.5 부력에 대한 안정성 검토

1) 조건

기초저면의 깊이(지표로 부터) : 12.145 m
 지하수위(지표하 m) : 2.000 m
 기초의 저판 폭 : 30.500 m (부력의 작용폭 - 부력방지용 Key 길이 포함)
 기초의 저판 두께 : 1.400 m
 흙과흙의마찰력 고려깊이 : 10.745 m
 포장두께 t = 0.08 m 포장 폭 : B = 11.280
 기초저판의 부력방지용 Key 길이 : 0.5 m

2) 단위중량

$\gamma_t = 1.9$ $\phi = 30$
 $\gamma_{sub} = 0.9$
 $\gamma_{con} = 2.5$
 $\gamma_{ascon} = 2.3$

3) 하중계산

PAB자중 :	2.5	x	11.400	x	2	ea	=	57.000		
연직토압 :	1.9	x	59.000	+	0.9	x	56.341	=	162.807	
	1.9	x	2.000	+	0.9	x	8.745	(기초저판 Key 상단)	=	11.671
기초중량:	2.5	x	47.850	+	1.750	(기초저판 Key)	=	121.375		
흙의마찰력:	$Ka = \tan^2(45 - \phi/2) = 0.333$ $Pf = 1/2 * Ka * \gamma_{sub} * H^2 * \tan \delta * 2ea$ $= 0.5 x 0.333 x 0.9 x 10.745^2 x \tan \phi x 2 ea$ $= 19.965$									
벽면 마찰력 :	=	0.5	x	0.333	x	0.9	x	1.400^2 x		
								$\tan(\phi * 2/3)$	x 2 ea = 0.214	
Ascon :	11.280	x	0.08	x	2.3	x	2	ea	= 4.151	
부가하중 :									= 0.000	
								ΣW	= 377.183	

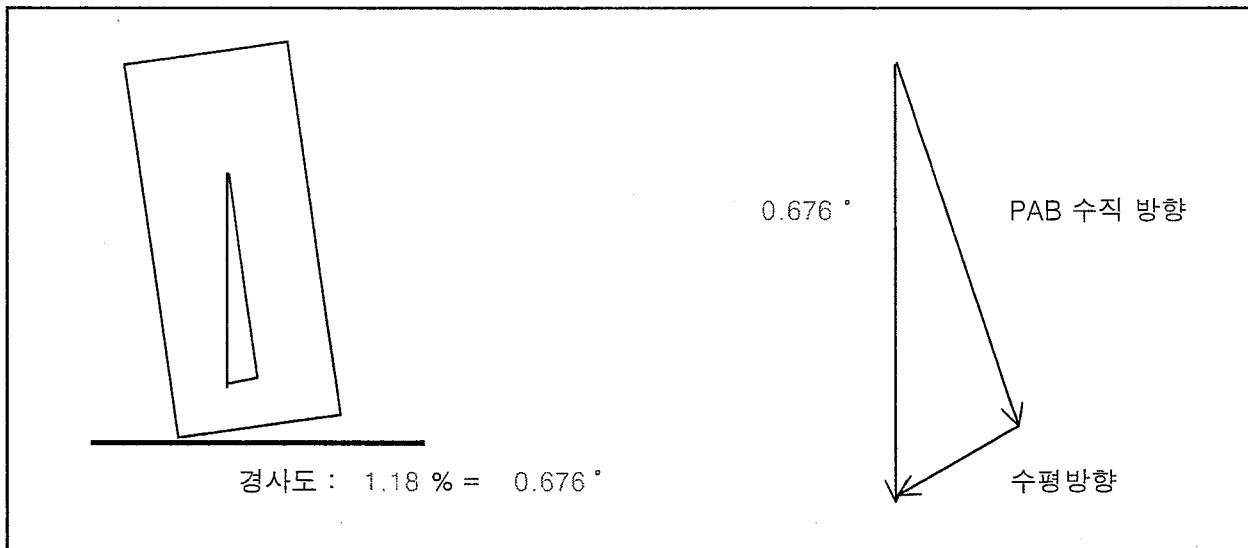
4) 부력

부력 : $U = 1 x 10.145 x 30.500 = 309.423$

5) 안정성 검토

안전율 : $FS = W / U = 377.183 / 309.423 = 1.219 > 1.2$ O.K!

4.6 가설시 전도에 대한 안정성 검토



$$\Theta = \tan^{-1} (1.1792) = 0.6756^{\circ}$$

$$\text{수직분력} = \text{Weight} * \cos(\Theta)$$

$$\text{수평분력} = \text{Weight} * \sin(\Theta)$$

$$M_o = 11.4 \times 1.5 \times 2.5 \times \cos(0.6756) = 42.75 \text{ ton}$$

$$M_r = 11.4 \times 1.5 \times 2.5 \times \sin(0.6756) = 0.50 \text{ ton}$$

$$S.F = 42.75 / 0.50 = 85.5 \quad \therefore \text{가설시 전도에 대해 안정함.}$$

* 시공완료 후에는 마감벽과 현장 타설 벽체 및 PAB가 일체로 연결되어 토압을 지지하므로 전도가 발생하지 않음.

5. SAP2000 OUTPUT

COMB1				COMB2		
	P	V	M	P	V	M
1	-117.86	11.78	0.00	-117.85	31.38	0.00
2	-116.79	20.85	10.69	-116.79	34.85	21.64
3	-115.73	29.25	27.11	-115.73	38.06	45.50
4	-114.67	36.94	48.76	-114.67	41.00	71.33
5	-115.77	36.20	63.21	-115.83	37.39	86.89
6	-110.79	30.84	75.19	-110.56	29.28	98.78
7	-103.11	45.90	89.23	-102.55	48.38	111.64
8	-97.19	39.50	70.46	-92.00	43.38	91.39
9	-94.36	38.75	51.20	-86.69	43.54	69.45
10	-89.45	25.78	13.99	-75.56	32.18	23.21
11	-88.16	17.42	6.94	-68.46	23.45	7.57
12	-89.67	11.88	18.40	-64.63	16.13	27.41
13	-93.32	8.41	24.07	-63.49	9.84	38.69
14	-98.74	4.68	26.30	-64.60	3.06	42.76
15	-93.32	8.42	24.07	-63.49	9.85	38.68
16	-89.67	11.89	18.38	-64.63	16.14	27.39
17	-88.16	17.43	6.91	-68.46	23.46	7.53
18	-89.45	25.79	14.03	-75.56	32.19	23.27
19	-94.16	38.75	51.29	-86.44	43.55	69.55
20	-97.56	40.31	71.18	-92.44	44.14	92.12
21	-104.32	44.95	89.35	-103.61	47.47	111.78
22	-109.89	33.42	76.83	-109.71	31.87	100.43
23	-115.62	36.74	63.43	-115.67	37.93	87.12
24	-114.68	36.94	48.75	-114.68	41.00	71.32
25	-115.74	29.24	27.11	-115.75	38.06	45.50
26	-116.81	20.85	10.69	-116.81	34.85	21.64
27	-117.88	11.78	0.00	-117.88	31.38	0.00
28	-117.88	11.85	0.00	-117.88	31.28	0.00
29	-116.82	20.92	10.74	-116.82	34.75	21.57
30	-115.76	29.31	27.20	-115.76	37.96	45.36
31	-114.69	37.01	48.89	-114.70	40.90	71.12
32	-115.63	36.81	63.60	-115.67	37.83	86.87
33	-109.91	33.49	77.03	-109.71	31.77	100.13
34	-104.34	44.92	89.58	-103.60	47.54	111.44
35	-97.62	35.95	71.44	-92.37	40.12	91.77
36	-94.22	15.30	14.40	-86.37	23.49	22.84
37	-89.52	6.46	6.51	-75.48	15.09	8.01
38	-88.23	1.10	17.97	-68.37	8.47	27.92
39	-89.74	2.45	23.65	-64.53	2.51	39.25
40	-93.39	4.66	25.90	-63.39	3.04	43.34
41	-98.81	8.39	23.69	-64.50	9.83	39.29
42	-93.39	11.86	18.05	-63.38	16.14	28.00
43	-89.73	17.39	6.62	-64.52	23.46	8.13
44	-88.22	25.74	14.27	-68.36	32.21	22.70
45	-89.51	38.70	51.45	-75.46	43.58	69.03
46	-94.42	38.70	51.45	-86.60	43.58	69.03
47	-97.24	39.45	70.69	-91.91	43.43	91.01
48	-103.11	45.85	89.47	-102.52	48.44	111.32

49	-110.79	30.91	75.39	-110.53	29.18	98.49
50	-115.77	36.28	63.38	-115.81	37.29	86.64
51	-114.66	37.01	48.90	-114.66	40.90	71.12
52	-115.72	29.32	27.20	-115.72	37.96	45.36
53	-116.78	20.92	10.74	-116.78	34.75	21.57
54	-117.84	11.85	0.00	-117.84	31.28	0.00
101	-117.86	11.78	8.84	-117.85	31.38	8.84
102	-121.65	9.54	6.96	-121.65	23.23	28.79
301	-117.84	11.85	8.84	-117.84	31.28	8.84
302	-124.08	24.85	21.97	-124.08	17.25	46.57
401	0.00	26.53	0.00	0.00	43.72	0.00
402	-23.54	56.52	36.43	17.50	39.51	38.49
403	-22.54	58.11	16.36	18.47	35.97	20.07
404	-21.89	27.83	6.46	18.86	10.51	24.17
405	-21.66	6.70	10.60	18.89	11.08	16.66
406	-21.63	6.02	8.00	18.79	8.02	8.64
407	-21.66	4.94	4.46	18.71	5.02	3.33
408	-21.70	3.62	1.86	18.65	3.18	0.68
409	-21.73	2.70	0.44	18.62	2.22	0.35
410	-21.75	1.98	0.16	18.60	1.79	0.54
411	-21.77	2.04	0.14	18.58	2.30	0.28
412	-21.81	2.86	0.61	18.54	3.01	0.60
413	-21.88	4.26	2.60	18.48	4.27	2.60
414	-21.94	6.27	6.36	18.42	6.28	6.37
415	-21.89	8.10	11.75	18.47	8.20	11.84
416	-21.59	7.38	16.25	18.77	7.36	16.26
417	-20.66	37.75	11.50	19.70	37.68	11.54
418	-19.14	91.41	20.11	21.22	91.42	20.01
419	-40.42	89.82	51.85	9.59	89.98	51.97
420	-38.69	91.29	20.01	11.33	91.57	20.17
421	-37.76	37.64	11.50	12.26	37.81	11.49
422	-37.47	7.36	16.23	12.55	7.41	16.27
423	-37.39	8.25	11.84	12.63	8.12	11.80
424	-37.47	6.28	6.32	12.55	6.28	6.40
425	-37.54	4.20	2.55	12.49	4.31	2.63
426	-37.57	2.83	0.62	12.45	3.03	0.59
427	-37.60	1.89	0.10	12.43	2.38	0.31
428	-37.63	2.13	0.00	12.42	1.87	0.63
429	-37.66	2.87	0.76	12.39	2.15	0.51
430	-37.69	3.89	2.42	12.33	3.07	0.43
431	-37.70	4.98	5.05	12.23	5.08	3.14
432	-37.62	5.41	8.05	12.10	8.46	8.84
433	-37.30	12.10	8.54	12.09	12.46	18.07
434	-36.52	37.30	0.39	12.43	13.28	28.04
435	-35.55	69.12	31.57	13.33	31.76	27.75
436	0.00	67.53	55.49	0.00	43.40	42.09
437	0.00	20.65	0.00	0.00	47.61	0.00

	COMB3			COMB4		
	P	V	M	P	V	M
1	-109.48	4.70	0.00	-108.53	15.60	0.00
2	-108.42	15.72	6.71	-107.47	23.28	12.73
3	-107.35	25.86	20.36	-106.41	30.28	30.28
4	-106.29	35.11	40.31	-105.35	36.59	52.15
5	-107.24	35.68	54.35	-106.28	35.40	66.45
6	-104.77	31.60	66.58	-103.53	29.66	78.21
7	-99.27	42.38	81.03	-97.81	43.91	91.50
8	-95.60	36.53	63.72	-90.77	38.95	73.26
9	-93.16	36.34	45.94	-86.66	39.23	53.79
10	-88.43	24.61	11.09	-77.64	28.49	13.28
11	-86.62	16.90	8.89	-71.69	20.45	12.85
12	-87.25	11.53	20.01	-68.39	13.75	29.04
13	-89.85	7.83	25.37	-67.37	7.96	37.44
14	-94.09	5.26	26.90	-68.33	4.98	39.21
15	-90.11	9.44	23.43	-67.94	11.45	33.23
16	-87.70	13.11	16.14	-69.37	17.20	20.62
17	-87.26	18.44	3.09	-73.08	23.80	0.22
18	-89.23	26.08	18.83	-79.40	31.70	30.13
19	-93.91	37.72	55.65	-88.49	42.25	74.88
20	-96.95	38.62	74.78	-93.34	42.53	96.57
21	-102.09	42.70	92.08	-102.37	45.75	115.46
22	-105.21	34.60	79.03	-106.01	33.27	103.52
23	-108.08	37.68	65.05	-109.09	39.17	89.53
24	-107.12	37.56	49.97	-108.06	41.96	73.21
25	-108.18	29.87	27.92	-109.12	39.02	46.75
26	-109.24	21.47	11.10	-110.19	35.81	22.27
27	-111.38	12.40	0.00	-112.32	32.34	0.00
28	-111.38	13.64	0.00	-112.32	33.46	0.00
29	-110.32	22.72	11.91	-111.26	36.93	23.00
30	-109.25	31.11	29.55	-110.20	40.14	48.21
31	-108.19	38.80	52.41	-109.14	43.08	75.40
32	-104.24	39.09	68.05	-105.24	40.45	92.22
33	-101.74	36.26	82.76	-102.52	34.81	106.88
34	-103.33	42.74	96.41	-103.58	45.87	119.38
35	-98.57	34.37	79.12	-94.86	38.52	100.45
36	-95.52	15.91	22.79	-90.00	22.81	33.51
37	-90.83	8.07	0.28	-80.88	15.31	2.50
38	-88.82	3.22	13.58	-74.52	9.60	18.75
39	-89.19	0.22	21.87	-70.73	4.42	32.39
40	-91.50	2.68	26.52	-69.22	0.51	39.56
41	-95.46	6.74	26.30	-69.66	6.87	39.09
42	-90.90	10.30	22.44	-68.31	12.55	32.16
43	-88.15	16.95	12.42	-69.17	20.53	17.03
44	-87.53	25.99	8.75	-72.47	29.93	10.36
45	-89.49	37.61	45.41	-78.59	40.57	52.76
46	-94.35	37.61	45.41	-87.75	40.57	52.76
47	-96.82	37.69	63.85	-91.89	40.18	72.94
48	-100.92	43.50	81.69	-99.45	45.11	91.75
49	-106.42	31.64	67.22	-105.16	29.57	78.49

50	-108.88	35.88	54.98	-107.92	35.47	66.77
51	-107.93	35.39	40.85	-106.98	36.74	52.44
52	-108.99	26.14	20.72	-108.04	30.43	30.47
53	-110.05	15.99	6.89	-109.10	23.42	12.83
54	-111.11	4.98	0.00	-110.17	15.75	0.00
101	-109.48	4.70	8.21	-108.53	15.60	8.14
102	-113.27	21.32	19.18	-112.33	2.74	1.03
301	-111.11	4.98	8.33	-110.17	15.75	8.26
302	-117.35	39.91	45.80	-116.41	16.03	7.05
401	0.00	49.93	0.00	0.00	56.08	0.00
402	-37.99	57.40	85.29	-14.97	63.55	56.26
403	-37.90	50.08	67.26	-14.88	46.87	39.35
404	-37.63	42.96	26.18	-14.61	39.72	1.11
405	-37.46	35.76	8.63	-14.44	32.52	30.83
406	-37.21	28.53	37.00	-14.19	25.29	56.36
407	-37.02	21.28	59.00	-14.00	18.04	75.50
408	-36.78	13.99	74.55	-13.76	10.76	88.21
409	-36.57	6.67	83.69	-13.55	3.43	94.48
410	-36.35	0.72	86.30	-13.33	3.93	94.26
411	-36.12	8.09	82.45	-13.10	11.31	87.54
412	-35.91	15.51	72.01	-12.90	18.72	74.27
413	-35.67	22.95	55.06	-12.65	26.16	54.46
414	-35.37	30.49	31.50	-12.34	33.65	28.05
415	-35.34	38.00	1.21	-12.33	41.16	5.03
416	-35.03	45.41	35.51	-12.01	48.65	44.65
417	-34.75	53.01	78.96	-11.73	56.22	90.97
418	-33.89	84.95	129.20	-10.87	88.24	144.05
419	-58.36	87.97	159.48	-29.98	91.26	175.49
420	-57.54	84.24	126.84	-29.32	83.33	144.75
421	-57.25	53.42	76.25	-29.02	57.84	90.23
422	-56.92	45.85	32.46	-28.68	50.21	42.53
423	-56.92	38.13	4.64	-28.71	42.48	1.59
424	-56.60	30.17	34.65	-28.38	34.62	32.41
425	-56.34	22.45	57.87	-28.11	26.87	59.56
426	-56.12	14.63	74.25	-27.90	19.05	79.84
427	-55.87	6.78	83.67	-27.65	11.19	93.19
428	-55.64	1.16	86.18	-27.42	3.31	99.60
429	-55.41	9.07	81.66	-27.18	4.63	99.01
430	-55.16	17.02	70.18	-26.93	12.57	91.43
431	-54.94	24.99	51.63	-26.71	20.54	76.81
432	-54.67	32.99	26.07	-26.45	28.54	55.16
433	-54.47	41.02	6.61	-26.24	36.57	26.40
434	-54.18	49.09	46.40	-25.95	44.64	9.49
435	-53.93	57.18	93.34	-25.71	52.73	52.49
436	0.00	60.40	113.92	0.00	62.48	71.52
437	0.00	38.89	0.00	0.00	53.97	0.00

	COMB5			COMB6		
	P	V	M	P	V	M
1	-130.59	17.35	0.00	-130.59	36.95	0.00
2	-129.53	26.42	14.33	-129.53	40.42	25.27
3	-128.47	34.81	34.39	-128.47	43.63	52.77
4	-127.41	42.51	59.67	-127.40	46.57	82.24
5	-128.76	41.17	76.24	-128.81	42.35	99.92
6	-123.53	34.66	89.83	-123.30	33.10	113.42
7	-115.20	51.50	105.50	-114.63	53.98	127.91
8	-108.16	44.84	84.30	-102.97	48.73	105.23
9	-104.68	44.45	62.24	-97.00	49.24	80.49
10	-98.14	30.63	18.39	-84.25	37.03	27.61
11	-95.53	21.30	7.69	-75.82	27.33	8.32
12	-96.06	14.66	22.86	-71.02	18.92	31.87
13	-99.11	10.00	30.79	-69.28	11.43	45.41
14	-104.30	4.94	33.82	-70.16	3.33	50.27
15	-99.11	10.01	30.78	-69.28	11.44	45.40
16	-96.06	14.67	22.84	-71.02	18.93	31.84
17	-95.53	21.31	7.66	-75.83	27.34	8.28
18	-98.14	30.63	18.44	-84.25	37.04	27.67
19	-104.43	44.45	62.34	-96.72	49.25	80.60
20	-108.58	45.74	85.12	-103.46	49.57	106.06
21	-116.53	50.44	105.63	-115.82	52.95	128.05
22	-122.53	37.54	91.66	-122.35	35.99	115.26
23	-128.58	41.77	76.49	-128.63	42.96	100.17
24	-127.42	42.50	59.66	-127.42	46.57	82.23
25	-128.48	34.81	34.38	-128.48	43.63	52.77
26	-129.55	26.42	14.32	-129.55	40.42	25.27
27	-130.62	17.34	0.00	-130.62	36.95	0.00
28	-130.62	17.39	0.00	-130.62	36.82	0.00
29	-129.56	26.46	14.35	-129.56	40.29	25.19
30	-128.49	34.85	34.44	-128.50	43.50	52.60
31	-127.43	42.55	59.75	-127.43	46.44	81.98
32	-128.59	41.81	76.59	-128.64	42.83	99.86
33	-122.55	37.58	91.78	-122.34	35.86	114.89
34	-116.55	50.42	105.77	-115.81	53.04	127.63
35	-108.63	40.92	85.28	-103.37	45.09	105.61
36	-104.47	19.16	18.68	-96.62	27.35	27.12
37	-98.19	9.46	7.39	-84.14	18.09	8.89
38	-95.57	3.13	22.57	-75.71	10.50	32.52
39	-96.11	1.52	30.52	-70.90	3.44	46.12
40	-99.16	4.92	33.57	-69.16	3.30	51.01
41	-104.35	9.99	30.56	-70.03	11.42	46.16
42	-99.15	14.65	22.65	-69.15	18.93	32.60
43	-96.10	21.28	7.51	-70.89	27.36	9.02
44	-95.56	30.60	18.54	-75.70	37.07	26.97
45	-98.17	44.41	62.38	-84.13	49.29	79.96
46	-104.70	44.41	62.38	-96.89	49.29	79.96
47	-108.18	44.81	84.45	-102.86	48.80	104.77
48	-115.19	51.46	105.65	-114.60	54.05	127.50
49	-123.53	34.70	89.96	-123.27	32.97	113.06

50	-128.75	41.21	76.34	-128.79	42.23	99.61
51	-127.39	42.55	59.75	-127.39	46.44	81.98
52	-128.46	34.86	34.44	-128.45	43.50	52.60
53	-129.52	26.46	14.35	-129.52	40.29	25.19
54	-130.58	17.39	0.00	-130.58	36.82	0.00
101	-130.59	17.35	9.79	-130.59	36.95	9.79
102	-134.38	3.98	0.27	-134.38	28.80	35.47
301	-130.58	17.39	9.79	-130.58	36.82	9.79
302	-136.82	19.31	10.41	-136.82	22.79	58.12
401	0.00	32.53	0.00	0.00	49.72	0.00
402	-18.01	57.91	31.23	23.03	45.51	44.05
403	-16.92	59.50	10.67	24.09	37.36	25.76
404	-16.25	26.19	10.69	24.49	12.71	28.41
405	-16.04	6.50	12.89	24.51	12.63	18.95
406	-16.04	6.84	8.92	24.38	8.83	9.56
407	-16.08	5.26	4.66	24.28	5.33	3.53
408	-16.13	3.69	1.78	24.22	3.25	0.60
409	-16.16	2.67	0.30	24.19	2.20	0.50
410	-16.18	1.92	0.29	24.17	1.82	0.67
411	-16.21	2.10	0.21	24.15	2.36	0.36
412	-16.25	2.98	0.64	24.11	3.13	0.63
413	-16.32	4.49	2.84	24.04	4.51	2.84
414	-16.40	6.71	6.99	23.97	6.72	7.00
415	-16.34	8.75	12.95	24.02	8.85	13.05
416	-16.01	7.93	17.90	24.35	7.91	17.92
417	-14.97	41.43	12.67	25.38	41.36	12.70
418	-13.30	100.71	22.19	27.06	100.72	22.09
419	-35.17	99.11	57.19	14.85	99.32	57.37
420	-33.26	100.63	22.13	16.76	100.91	22.30
421	-32.23	41.35	12.66	17.79	41.53	12.65
422	-31.91	7.92	17.88	18.11	7.98	17.92
423	-31.83	8.87	13.03	18.19	8.74	12.99
424	-31.91	6.72	6.96	18.11	6.73	7.04
425	-31.99	4.44	2.80	18.04	4.58	2.87
426	-32.03	2.95	0.65	18.00	3.19	0.60
427	-32.06	1.97	0.18	17.98	2.53	0.45
428	-32.08	2.04	0.15	17.96	1.97	0.91
429	-32.11	2.81	0.56	17.93	2.05	0.87
430	-32.16	3.92	2.24	17.85	3.17	0.16
431	-32.19	5.30	5.15	17.73	5.79	3.50
432	-32.14	6.35	8.99	17.60	9.81	10.38
433	-31.86	8.90	11.25	17.54	13.83	20.82
434	-31.08	33.96	5.16	17.87	16.31	33.47
435	-30.02	68.64	23.07	18.86	31.20	36.16
436	0.00	67.05	46.83	0.00	50.66	48.81
437	0.00	27.85	0.00	0.00	54.87	0.00

	COMB7			COMB8		
	P	V	M	P	V	M
1	-80.49	10.96	0.00	-80.49	10.96	0.00
2	-79.67	16.29	8.92	-79.67	16.29	8.92
3	-78.86	21.23	21.21	-78.86	21.23	21.21
4	-78.04	25.76	36.57	-78.04	25.76	36.57
5	-78.74	24.83	46.58	-78.74	24.83	46.58
6	-75.33	20.77	54.73	-75.33	20.77	54.73
7	-70.06	31.58	64.11	-70.06	31.58	64.11
8	-65.35	27.43	51.13	-65.35	27.43	51.13
9	-63.07	27.07	37.64	-63.07	27.07	37.64
10	-58.82	18.52	10.97	-58.82	18.52	10.97
11	-57.08	12.80	4.79	-57.08	12.80	4.79
12	-57.30	8.76	13.89	-57.30	8.76	13.89
13	-59.06	5.96	18.63	-59.06	5.96	18.63
14	-62.11	2.94	20.43	-62.11	2.94	20.43
15	-59.06	5.96	18.62	-59.06	5.96	18.62
16	-57.30	8.76	13.88	-57.30	8.76	13.88
17	-57.08	12.80	4.77	-57.08	12.80	4.77
18	-58.82	18.53	10.99	-58.82	18.53	10.99
19	-62.92	27.07	37.70	-62.92	27.07	37.70
20	-65.62	27.97	51.62	-65.62	27.97	51.62
21	-70.86	30.94	64.20	-70.86	30.94	64.20
22	-74.73	22.53	55.84	-74.73	22.53	55.84
23	-78.63	25.20	46.73	-78.63	25.20	46.73
24	-78.05	25.76	36.57	-78.05	25.76	36.57
25	-78.86	21.23	21.21	-78.86	21.23	21.21
26	-79.68	16.29	8.92	-79.68	16.29	8.92
27	-80.51	10.95	0.00	-80.51	10.95	0.00
28	-80.51	10.98	0.00	-80.51	10.98	0.00
29	-79.69	16.31	8.93	-79.69	16.31	8.93
30	-78.87	21.25	21.24	-78.87	21.25	21.24
31	-78.06	25.78	36.61	-78.06	25.78	36.61
32	-78.64	25.22	46.79	-78.64	25.22	46.79
33	-74.74	22.55	55.90	-74.74	22.55	55.90
34	-70.87	30.93	64.26	-70.87	30.93	64.26
35	-65.64	25.06	51.71	-65.64	25.06	51.71
36	-62.94	11.65	11.13	-62.94	11.65	11.13
37	-58.85	5.72	4.63	-58.85	5.72	4.63
38	-57.11	1.89	13.74	-57.11	1.89	13.74
39	-57.33	0.90	18.49	-57.33	0.90	18.49
40	-59.09	2.93	20.31	-59.09	2.93	20.31
41	-62.13	5.95	18.52	-62.13	5.95	18.52
42	-59.08	8.75	13.79	-59.08	8.75	13.79
43	-57.32	12.78	4.71	-57.32	12.78	4.71
44	-57.10	18.51	11.03	-57.10	18.51	11.03
45	-58.84	27.05	37.71	-58.84	27.05	37.71
46	-63.08	27.05	37.71	-63.08	27.05	37.71
47	-65.37	27.41	51.20	-65.37	27.41	51.20
48	-70.06	31.56	64.19	-70.06	31.56	64.19
49	-75.33	20.79	54.79	-75.33	20.79	54.79

50	-78.73	24.85	46.63	-78.73	24.85	46.63
51	-78.03	25.78	36.62	-78.03	25.78	36.62
52	-78.85	21.25	21.24	-78.85	21.25	21.24
53	-79.66	16.31	8.93	-79.66	16.31	8.93
54	-80.48	10.98	0.00	-80.48	10.98	0.00
101	-80.49	10.96	6.04	-80.49	10.96	6.04
102	-83.41	1.59	0.60	-83.41	1.59	0.60
301	-80.48	10.98	6.04	-80.48	10.98	6.04
302	-85.28	10.61	4.71	-85.28	10.61	4.71
401	0.00	20.99	0.00	0.00	20.91	0.00
402	-9.88	35.44	18.34	-9.89	35.64	18.25
403	-9.20	36.66	5.71	-9.21	36.86	5.55
404	-8.79	16.09	7.13	-8.80	16.41	7.58
405	-8.66	4.49	8.22	-8.67	4.22	9.04
406	-8.66	4.60	5.62	-8.65	5.21	6.69
407	-8.69	3.57	2.92	-8.60	6.54	3.45
408	-8.72	2.58	1.13	-8.79	6.15	0.33
409	-8.74	1.95	0.21	-8.67	4.38	0.73
410	-8.76	1.48	0.15	-8.79	8.31	1.46
411	-8.77	1.61	0.09	-8.62	5.82	0.40
412	-8.80	2.15	0.44	-8.78	6.87	1.58
413	-8.84	3.09	1.81	-8.64	5.08	2.30
414	-8.89	4.47	4.39	-8.79	7.61	4.14
415	-8.85	5.74	8.11	-8.88	12.44	7.69
416	-8.65	5.23	11.18	-8.55	8.59	11.73
417	-8.00	26.08	7.92	-8.08	23.67	7.58
418	-6.96	62.89	13.77	-6.98	62.29	11.99
419	-20.04	61.67	35.59	-20.02	61.06	33.59
420	-18.84	62.85	13.74	-18.77	62.24	11.97
421	-18.21	26.04	7.92	-18.02	23.63	7.56
422	-18.01	5.23	11.17	-17.98	8.60	11.71
423	-17.95	5.81	8.15	-17.74	12.40	7.77
424	-18.01	4.48	4.38	-17.92	7.41	4.26
425	-18.05	3.06	1.79	-18.08	5.28	2.12
426	-18.08	2.14	0.45	-17.94	6.80	1.52
427	-18.10	1.54	0.08	-18.06	5.89	0.39
428	-18.11	1.55	0.07	-17.89	8.23	1.37
429	-18.13	2.03	0.35	-18.07	4.46	0.88
430	-18.16	2.72	1.39	-17.96	6.11	0.05
431	-18.18	3.61	3.21	-18.20	6.57	3.74
432	-18.15	4.35	5.69	-18.15	4.96	6.76
433	-17.99	5.23	7.36	-17.98	5.66	8.18
434	-17.52	20.50	4.10	-17.51	20.82	4.54
435	-16.86	41.96	12.65	-16.85	42.16	12.49
436	0.00	40.74	27.13	0.00	40.94	27.04
437	0.00	18.50	0.00	0.00	18.42	0.00

	COMB9			COMB10		
	P	V	M	P	V	M
1	-80.49	20.29	0.00	-80.49	20.29	0.00
2	-79.67	22.96	14.13	-79.67	22.96	14.13
3	-78.86	25.43	29.97	-78.86	25.43	29.97
4	-78.04	27.69	47.32	-78.04	27.69	47.32
5	-78.76	25.39	57.86	-78.76	25.39	57.86
6	-75.22	20.03	65.96	-75.22	20.03	65.96
7	-69.79	32.76	74.79	-69.79	32.76	74.79
8	-62.88	29.28	61.09	-62.88	29.28	61.09
9	-59.42	29.35	46.33	-59.42	29.35	46.33
10	-52.21	21.57	15.36	-52.21	21.57	15.36
11	-47.70	15.67	5.09	-47.70	15.67	5.09
12	-45.38	10.79	18.18	-45.38	10.79	18.18
13	-44.86	6.64	25.59	-44.86	6.64	25.59
14	-45.85	2.17	28.27	-45.85	2.17	28.27
15	-44.86	6.64	25.58	-44.86	6.64	25.58
16	-45.38	10.79	18.17	-45.38	10.79	18.17
17	-47.70	15.67	5.07	-47.70	15.67	5.07
18	-52.21	21.58	15.39	-52.21	21.58	15.39
19	-59.25	29.35	46.40	-59.25	29.35	46.40
20	-63.18	29.79	61.60	-63.18	29.79	61.60
21	-70.52	32.14	74.88	-70.52	32.14	74.88
22	-74.65	21.79	67.08	-74.65	21.79	67.08
23	-78.65	25.76	58.01	-78.65	25.76	58.01
24	-78.05	27.69	47.32	-78.05	27.69	47.32
25	-78.86	25.43	29.96	-78.86	25.43	29.96
26	-79.68	22.96	14.13	-79.68	22.96	14.13
27	-80.51	20.29	0.00	-80.51	20.29	0.00
28	-80.51	20.23	0.00	-80.51	20.23	0.00
29	-79.69	22.90	14.09	-79.69	22.90	14.09
30	-78.87	25.37	29.89	-78.87	25.37	29.89
31	-78.06	27.63	47.20	-78.06	27.63	47.20
32	-78.66	25.70	57.87	-78.66	25.70	57.87
33	-74.65	21.73	66.91	-74.65	21.73	66.91
34	-70.52	32.18	74.67	-70.52	32.18	74.67
35	-63.13	27.05	61.39	-63.13	27.05	61.39
36	-59.21	15.55	15.15	-59.21	15.55	15.15
37	-52.16	9.83	5.34	-52.16	9.83	5.34
38	-47.65	5.39	18.48	-47.65	5.39	18.48
39	-45.32	1.46	25.91	-45.32	1.46	25.91
40	-44.80	2.16	28.61	-44.80	2.16	28.61
41	-45.79	6.63	25.94	-45.79	6.63	25.94
42	-44.80	10.79	18.53	-44.80	10.79	18.53
43	-45.32	15.67	5.43	-45.32	15.67	5.43
44	-47.64	21.59	15.05	-47.64	21.59	15.05
45	-52.15	29.37	46.08	-52.15	29.37	46.08
46	-59.36	29.37	46.08	-59.36	29.37	46.08
47	-62.83	29.31	60.87	-62.83	29.31	60.87
48	-69.77	32.79	74.60	-69.77	32.79	74.60
49	-75.21	19.97	65.79	-75.21	19.97	65.79

50	-78.75	25.33	57.71	-78.75	25.33	57.71
51	-78.03	27.63	47.20	-78.03	27.63	47.20
52	-78.85	25.37	29.89	-78.85	25.37	29.89
53	-79.66	22.90	14.09	-79.66	22.90	14.09
54	-80.48	20.23	0.00	-80.48	20.23	0.00
101	-80.49	20.29	6.04	-80.49	20.29	6.04
102	-83.41	14.02	17.62	-83.41	14.02	17.62
301	-80.48	20.23	6.04	-80.48	20.23	6.04
302	-85.28	9.44	27.93	-85.28	9.44	27.93
401	0.00	29.18	0.00	0.00	29.09	0.00
402	9.66	25.94	25.49	9.65	25.86	25.41
403	10.33	26.12	11.63	10.32	26.32	11.79
404	10.61	6.60	15.57	10.60	6.32	16.02
405	10.65	7.41	11.10	10.64	7.14	11.93
406	10.58	5.55	5.92	10.60	6.16	6.99
407	10.53	3.61	2.38	10.62	6.57	2.91
408	10.49	2.37	0.56	10.42	6.11	0.89
409	10.47	1.72	0.17	10.55	4.15	0.35
410	10.46	1.37	0.33	10.43	8.53	1.64
411	10.45	1.73	0.16	10.60	5.75	0.47
412	10.42	2.22	0.44	10.44	6.94	1.57
413	10.38	3.10	1.81	10.58	5.07	2.30
414	10.33	4.48	4.40	10.43	7.61	4.15
415	10.37	5.79	8.15	10.34	12.49	7.74
416	10.57	5.22	11.19	10.67	8.58	11.74
417	11.22	26.05	7.94	11.14	23.64	7.60
418	12.26	62.90	13.73	12.24	62.30	11.94
419	3.78	61.76	35.67	3.79	61.15	33.68
420	4.97	62.99	13.82	5.05	62.37	12.04
421	5.61	26.12	7.91	5.80	23.71	7.56
422	5.81	5.25	11.19	5.84	8.62	11.73
423	5.87	5.75	8.13	6.08	12.33	7.75
424	5.81	4.48	4.41	5.90	7.41	4.30
425	5.77	3.12	1.82	5.74	5.27	2.15
426	5.74	2.23	0.43	5.89	6.89	1.51
427	5.73	1.77	0.17	5.76	5.80	0.49
428	5.72	1.41	0.37	5.94	8.57	1.67
429	5.70	1.68	0.25	5.76	4.12	0.28
430	5.66	2.33	0.44	5.86	6.07	1.00
431	5.60	3.66	2.30	5.58	6.62	2.83
432	5.52	5.81	6.07	5.53	6.41	7.13
433	5.53	8.15	11.90	5.54	7.87	12.72
434	5.79	8.03	17.64	5.80	7.60	18.08
435	6.42	24.17	15.60	6.42	24.37	15.76
436	0.00	28.10	27.49	0.00	28.02	27.42
437	0.00	31.34	0.00	0.00	31.26	0.00

	COMB11			COMB12		
	P	V	M	P	V	M
1	-63.82	13.58	0.00	-63.82	13.58	0.00
2	-63.00	16.76	9.92	-63.00	16.76	9.92
3	-62.18	19.76	21.87	-62.18	19.76	21.87
4	-61.37	22.55	35.70	-61.37	22.55	35.70
5	-61.88	21.40	44.45	-61.88	21.40	44.45
6	-59.93	17.74	51.57	-59.93	17.74	51.57
7	-56.14	24.82	59.46	-56.14	24.82	59.46
8	-52.84	22.05	49.15	-52.84	22.05	49.15
9	-51.01	22.40	38.13	-51.01	22.40	38.13
10	-47.35	16.58	14.98	-47.35	16.58	14.98
11	-45.50	12.30	0.21	-45.50	12.30	0.21
12	-45.21	8.89	10.06	-45.21	8.89	10.06
13	-46.26	6.18	15.95	-46.26	6.18	15.95
14	-48.48	3.19	18.83	-48.48	3.19	18.83
15	-45.96	4.38	18.12	-45.97	4.38	18.12
16	-44.70	7.12	14.39	-44.70	7.12	14.39
17	-44.79	10.57	6.71	-44.79	10.57	6.71
18	-46.45	14.93	6.32	-46.45	14.93	6.32
19	-49.83	20.85	27.34	-49.83	20.85	27.34
20	-51.93	21.02	37.89	-51.93	21.02	37.89
21	-55.03	22.89	47.23	-55.03	22.89	47.23
22	-57.52	18.53	40.20	-57.52	18.53	40.20
23	-59.91	20.00	32.79	-59.91	20.00	32.79
24	-59.57	19.77	24.84	-59.57	19.77	24.84
25	-60.39	15.24	13.39	-60.39	15.24	13.39
26	-61.21	10.31	5.01	-61.21	10.31	5.01
27	-62.08	4.97	0.00	-62.08	4.97	0.00
28	-62.08	4.92	0.00	-62.08	4.92	0.00
29	-61.26	10.25	4.97	-61.26	10.25	4.97
30	-60.44	15.19	13.32	-60.44	15.19	13.32
31	-59.63	19.72	24.74	-59.63	19.72	24.74
32	-56.65	20.08	32.69	-56.65	20.08	32.69
33	-54.45	18.84	40.24	-54.45	18.84	40.24
34	-55.05	22.94	47.36	-55.05	22.94	47.36
35	-51.91	18.78	38.00	-51.91	18.78	38.00
36	-49.80	9.56	6.38	-49.80	9.56	6.38
37	-46.42	5.08	6.71	-46.42	5.08	6.71
38	-44.75	1.79	14.45	-44.75	1.79	14.45
39	-44.66	0.93	18.22	-44.66	0.93	18.22
40	-45.92	3.16	18.98	-45.92	3.16	18.98
41	-48.34	6.15	16.13	-48.34	6.15	16.13
42	-46.20	8.87	10.27	-46.20	8.87	10.27
43	-45.15	12.29	0.44	-45.15	12.29	0.44
44	-45.44	16.57	14.75	-45.44	16.57	14.75
45	-47.29	22.40	37.93	-47.29	22.40	37.93
46	-50.95	22.40	37.93	-50.95	22.40	37.93
47	-52.78	22.06	48.97	-52.78	22.06	48.97
48	-56.10	24.83	59.30	-56.10	24.83	59.30
49	-59.89	17.69	51.43	-59.89	17.69	51.43

50	-61.85	21.35	44.33	-61.85	21.35	44.33
51	-61.34	22.50	35.59	-61.34	22.50	35.59
52	-62.15	19.70	21.80	-62.15	19.70	21.80
53	-62.97	16.71	9.88	-62.97	16.71	9.88
54	-63.79	13.53	0.00	-63.79	13.53	0.00
101	-63.82	13.58	4.79	-63.82	13.58	4.79
102	-66.73	6.27	8.94	-66.73	6.27	8.94
301	-63.79	13.53	4.78	-63.79	13.53	4.78
302	-68.59	1.05	12.11	-68.59	1.05	12.11
401	0.00	21.19	0.00	0.00	21.10	0.00
402	1.43	23.23	18.10	1.43	23.43	18.02
403	1.98	24.45	3.93	1.97	24.66	4.09
404	2.25	8.30	9.90	2.24	8.62	10.34
405	2.31	5.34	8.06	2.30	5.06	8.88
406	2.27	4.47	4.71	2.29	5.07	5.78
407	2.24	3.19	2.13	2.33	6.16	2.66
408	2.21	2.28	0.67	2.14	6.53	0.78
409	2.20	1.76	0.03	2.27	4.19	0.55
410	2.19	1.44	0.16	2.15	8.50	1.47
411	2.18	1.65	0.06	2.32	5.92	0.37
412	2.15	2.06	0.39	2.17	6.77	1.52
413	2.12	2.76	1.46	2.32	5.71	1.96
414	2.09	3.84	3.49	2.18	6.97	3.23
415	2.11	4.85	6.41	2.08	11.55	5.99
416	2.27	4.42	8.80	2.37	7.78	9.34
417	2.78	20.69	6.26	2.70	18.29	5.91
418	3.59	49.40	10.67	3.57	48.79	8.89
419	-4.69	48.25	27.89	-4.67	47.64	25.89
420	-3.75	49.48	10.77	-3.67	48.87	8.99
421	-3.25	20.76	6.22	-3.06	18.34	5.86
422	-3.09	4.45	8.79	-3.06	7.82	9.33
423	-3.05	4.85	6.41	-2.83	11.43	6.04
424	-3.09	3.84	3.49	-3.00	6.77	3.38
425	-3.13	2.76	1.46	-3.15	5.91	1.79
426	-3.15	2.06	0.39	-3.00	6.72	1.47
427	-3.16	1.65	0.06	-3.13	5.97	0.38
428	-3.17	1.44	0.15	-2.95	8.49	1.45
429	-3.18	1.77	0.04	-3.12	4.20	0.57
430	-3.21	2.30	0.71	-3.01	6.49	0.73
431	-3.25	3.23	2.20	-3.27	6.20	2.73
432	-3.28	4.52	4.82	-3.27	5.12	5.89
433	-3.22	5.35	8.18	-3.21	5.08	9.01
434	-2.94	8.79	9.91	-2.93	9.11	10.35
435	-2.43	25.41	3.51	-2.42	25.61	3.67
436	0.00	24.19	18.36	0.00	24.39	18.29
437	0.00	21.47	0.00	0.00	21.39	0.00

2) 시공중 P.A.B 안정성 검토

1. 검토 내용

부산-울산 개착식 터널(4공구)의 시공과 관련하여 P.A.B 구조물 설치 후 P.A.B 벽체부까지 성토가 완료되었을 때의 구조적 안정성에 대해 검토하고자 함.

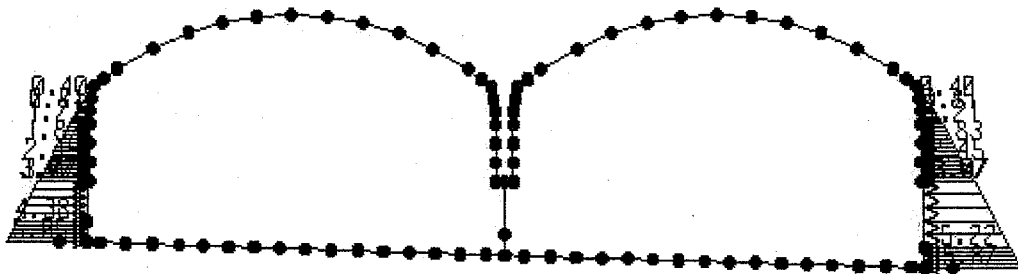
2. 검토 방법

2.1 모델링

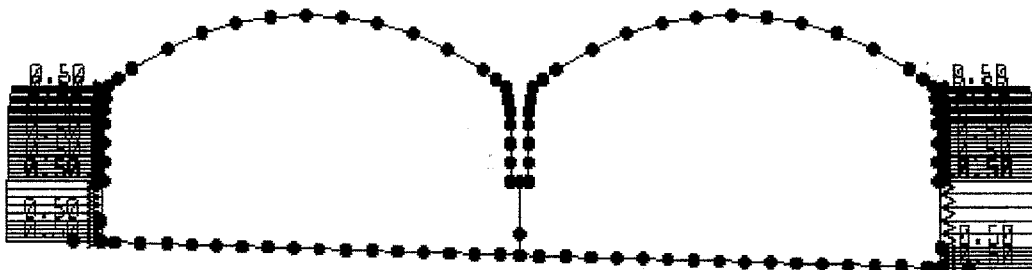
- 개착식 터널의 상시 검토와 동일

2.2 하중조건

- 1) 사하중 ; 구조물 사하중은 SAP2000에서 자동 고려.
- 2) 토압 ; P.A.B 벽체부까지 성토가 완료되었다고 가정하여 검토함.



- 3) 활하중 ; 벽체 성토부 차량 활하중으로 $P_v=1.0\text{t/m}^2$ 를 가정하고 활하중의 수평토압으로 0.5t/m^2 을 가정.



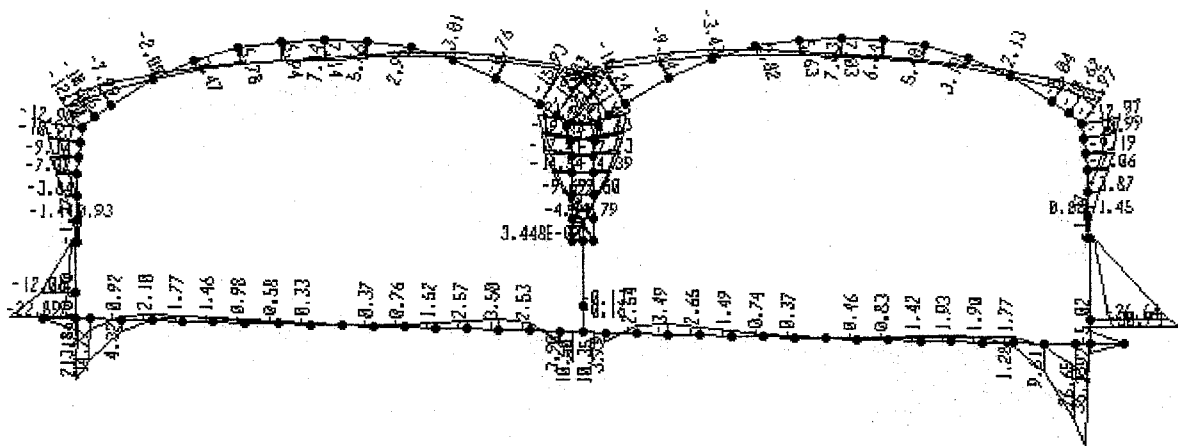
2.3 하중조합

- 도로교설계기준(p32) ; 가설시하중 참조

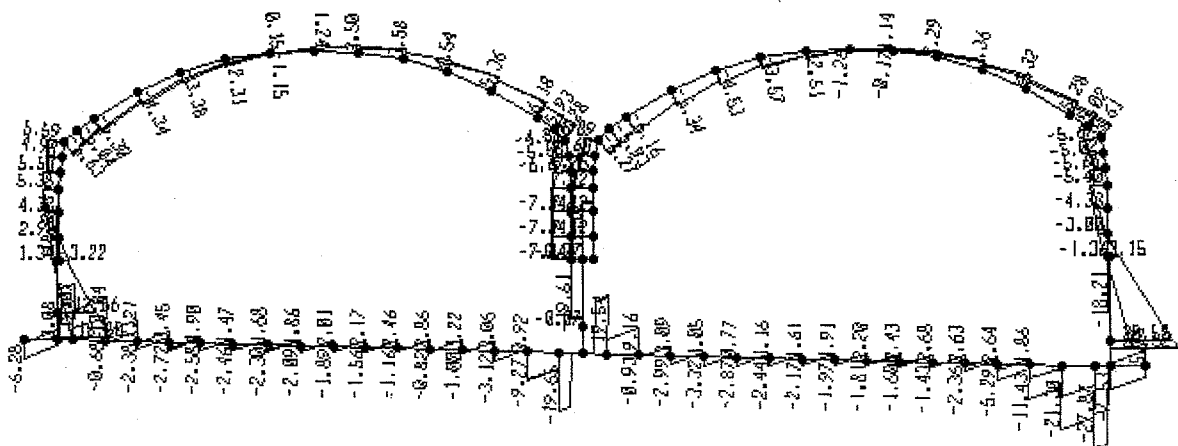
	사하중	토압	활하중의 토압	비고
Comb 1.	1.3	1.7	1.3	강도설계법
Comb 2.	1.3	0.65	1.3	
Comb 3.	1.0	1.0	1.0	허용응력설계법
Comb 4.	1.0	0.5	1.0	

3. 검토 결과

3.1 극한강 검토결과



< Moment Envelop >

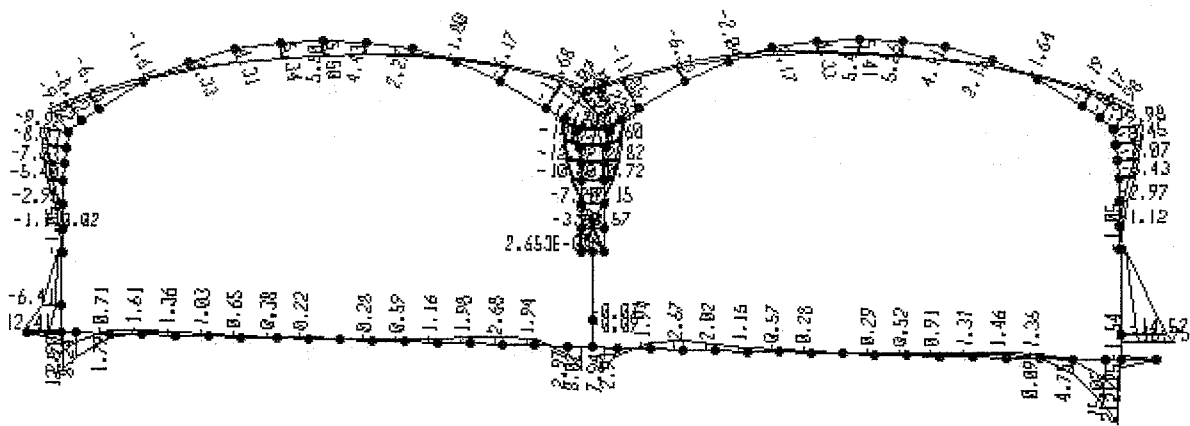


< Shear Envelop >

- 극한강 검토결과에 따르면,

- 1) 헌치부(절점 7) : $M_u = -21.86\text{t-m/m}$, $V_u = 6.28\text{t/m}$
- 2) 슬래브(절점 14) : $M_u = 7.14\text{t-m/m}$ 로서 완성시 P.A.B 단면력 검토시 적용된 하중에 비해 작아 시공중에 발생하는 하중은 구조적으로 문제없는 것으로 계산되었음.
- 3) 벽체부에 발생하는 하중은 벽체외측에 $M_u = -30.94\text{t-m/m}$, $V_u = 22.52\text{t/m}$ 로서 마찬가지로 완성시 현장타설 벽체부 단면력 검토시 적용된 하중에 비해 작아 구조적으로 문제없는 것으로 계산되었음.

3.2 허용응력 검토 결과



< Moment Envelop >

- 1) 현차부(절점 7) ; $M = -16.20\text{t-m/m}$
- 2) 슬래브(절점 14) ; $M = 5.50\text{t-m/m}$ 로서 완성시 성토 완료후 검토된 하중에 비해 작아 사용성 검토 결과는 문제없는 것으로 판단됨.

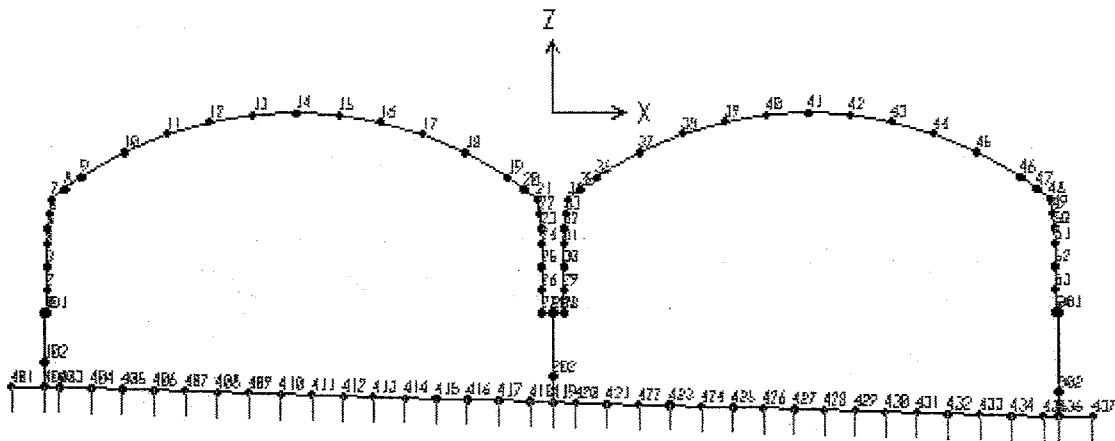
3) 온도하중 및 건조수축의 영향 검토

1. 검토 내용

부산-울산 개착식 터널(4공구)은 Precast Arch 크라운부에서의 토피고가 3m이고 Arch 면을 따라서 5.271m로 토피고가 증가하는 지중구조물이다. 따라서 대기에 노출된 구조물과 달라 온도하중의 영향이 작을 것으로 예상되나 본 검토에서는 온도하중의 영향을 고려하여 구조적 안정성을 확인하고자 함.

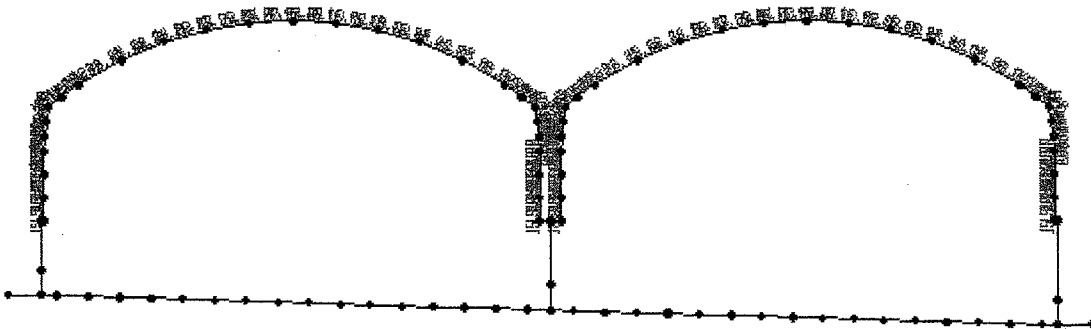
2. 검토 방법

2.1 모델링



2.2 하중조건

- 1) Comb 1. : 온도하중(+15°C) 작용시
- 2) Comb 2. : 온도하중(-15°C) 및 건조수축(-15°C의 온도하중으로 환산) 작용시



- 온도하중(+15°C)과 건조수축(-15°C의 온도하중으로 환산)을 모두 고려하면 결과적으로 온도가 “ 0” 이되므로 온도하중(-15°C)와 건조수축(-15°C)만 고려함.

2.3 하중조합

- ### 3 검토 결과

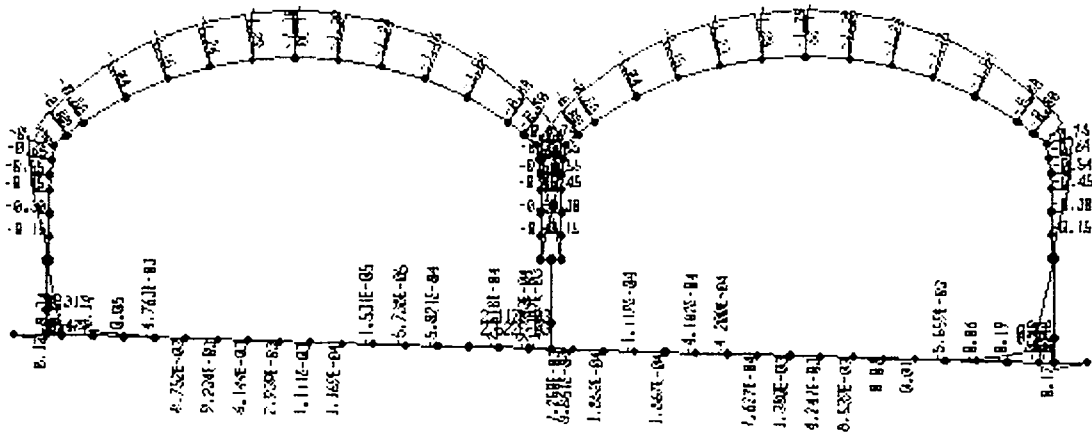


Figure 1: A schematic diagram of a two-span continuous beam bridge. The bridge has two equal spans, each 100m long, supported by three piers. The total length is 200m. The diagram shows the bridge structure with various dimensions and labels. The left span is labeled '100m' and the right span is labeled '100m'. The bridge is supported by three piers. The diagram also shows the bridge deck, the piers, and the approach spans. The bridge is labeled 'Figure 1' and 'Figure 2'.

- 고산터널 구조계산서에서 해석한 극한모멘트값에 온도 및 건조수축에 의해 발행한 모멘트값을 더해서 공칭모멘트와 비교 검토

절점번호	Mu	COMB1	COMB2	Mu+comb1	Mu+comb2	공칭모멘트	결과
1	0	0	0	0	0	100.183	0.K
2	-25.27	-0.15	0.30	-25.42	-24.97	100.183	0.K
3	-52.77	-0.30	0.6	-53.07	-52.17	100.183	0.K
4	-82.24	-0.45	0.90	-82.69	-81.34	100.183	0.K
5	-99.92	-0.55	1.09	-100.47	-98.83	111.893	0.K
6	-113.42	-0.65	1.29	-114.07	-112.13	148.994	0.K
7	-127.91	-0.74	1.48	-128.65	-126.43	216.158	0.K
8	-105.23	-0.80	1.61	-106.03	-103.62	150.374	0.K
9	-80.49	-0.88	1.76	-81.37	-78.73	114.947	0.K
10	-27.61	-1.04	2.08	-28.65	-25.53	103.245	0.K
11	12.85	-1.16	2.32	11.69	15.17	77.248	0.K
12	31.87	-1.24	2.48	30.63	34.35	77.248	0.K
13	45.41	-1.29	2.57	44.12	47.98	77.248	0.K
14	50.27	-1.3	2.60	48.97	52.87	77.248	0.K
15	45.4	-1.29	2.57	44.11	47.97	77.248	0.K
16	31.84	-1.24	2.48	30.60	34.32	77.248	0.K
17	8.28	-1.16	2.32	7.12	10.60	77.248	0.K
18	-30.13	-1.04	2.08	-31.17	-28.05	103.245	0.K
19	-80.60	-0.88	1.76	-81.48	-78.84	114.947	0.K
20	-106.06	-0.80	1.61	-106.86	-104.45	150.374	0.K
21	-128.05	-0.74	1.48	-128.79	-126.57	216.158	0.K
22	-115.26	-0.65	1.29	-115.91	-113.97	148.994	0.K
23	-100.17	-0.55	1.09	-100.72	-99.08	111.893	0.K
24	-82.23	-0.45	0.90	-82.68	-81.33	100.183	0.K
25	-52.77	-0.30	0.60	-53.07	-52.17	100.183	0.K
26	-25.27	-0.15	0.30	-25.42	-24.97	100.183	0.K
27	0	0	0	0	0	100.183	0.K

4) 기초슬래브에 작용하는 노면활하중의 영향 검토

1. 검토내용

기초슬래브 상면에 노면 활하중이 작용하는 경우에 대해 검토하여 P.A.R 및 바닥슬래브에 하중의 증감을 확인하여 구조적으로 미치는 영향에 대해 확인하도록 함.

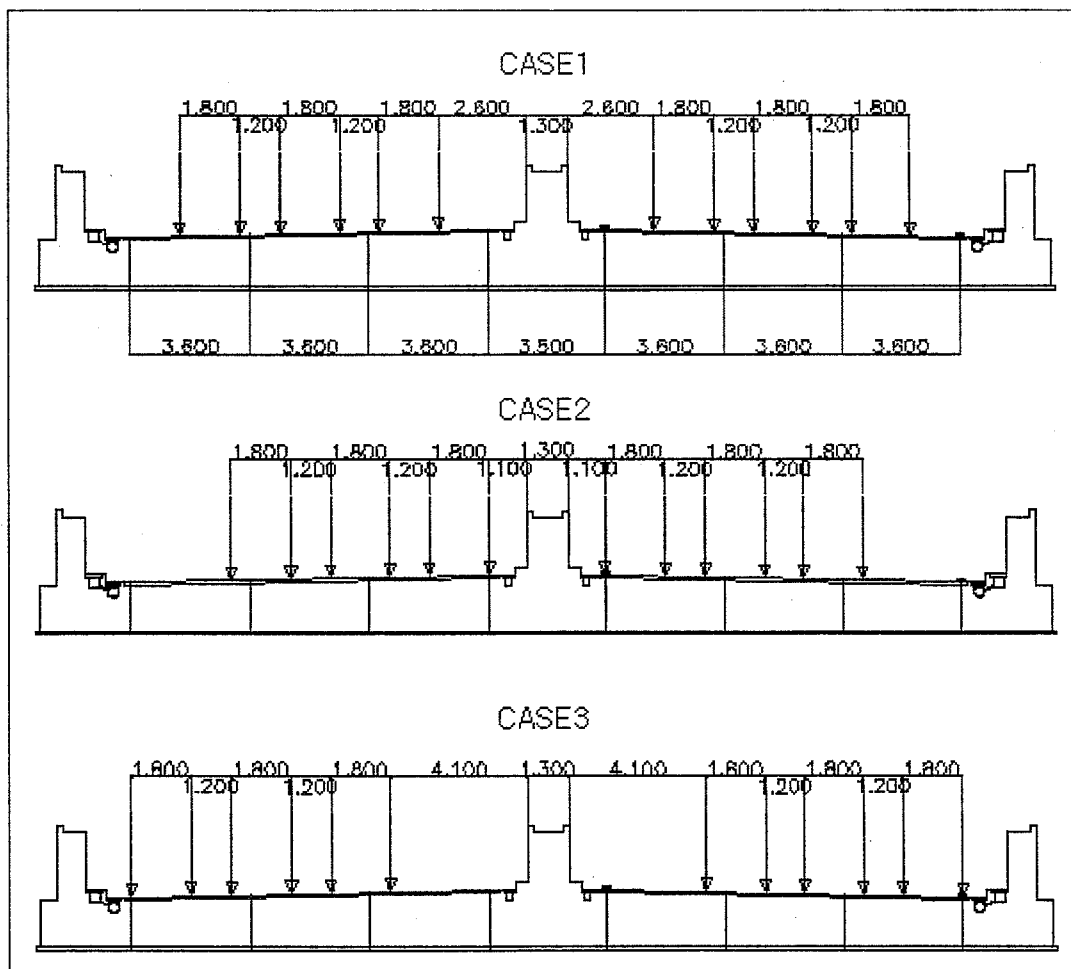
2. 검토 방법

바닥 슬래브에 작용하는 활하중의 종류는 하중의 재하위치를 고려하여 다음과 같이 구분하여 작용하도록 함.

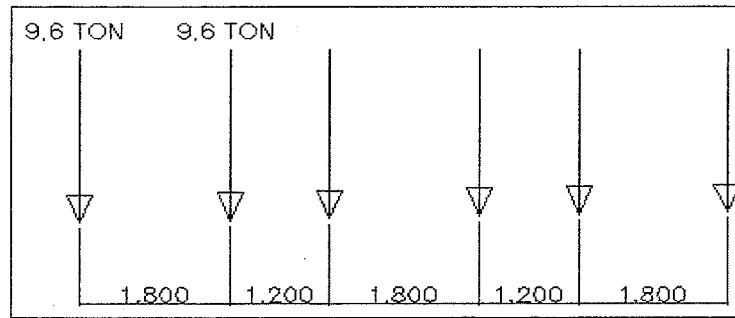
CASE1 : 차량이 슬래브 중앙에 배치된 경우

CASE2 : 차량이 슬래브 우측으로 배치된 경우

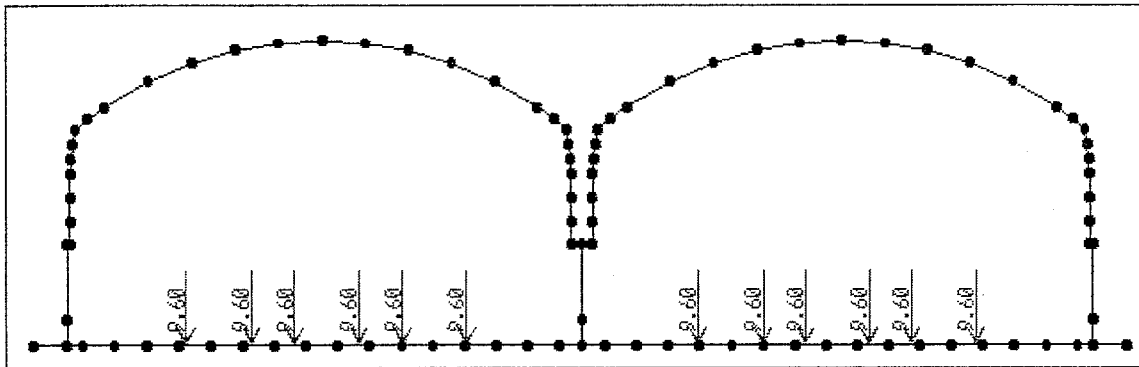
CASE3 : 차량이 슬래브 좌측으로 배치된 경우



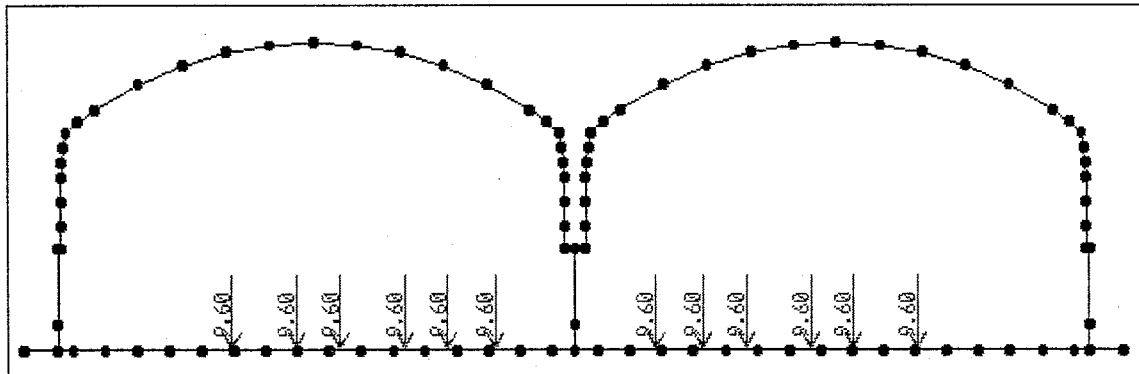
<CASE>



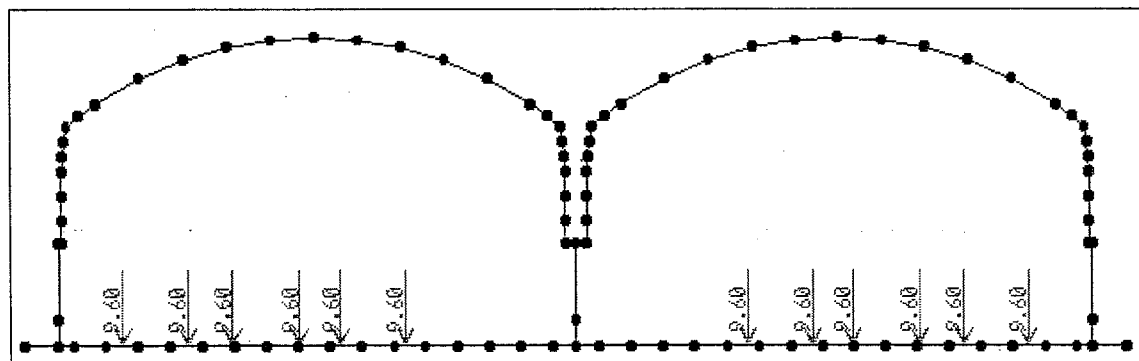
<차량 폭 및 간격>



<CASE1 SAP2000모델링>



<CASE2 SAP2000모델링>

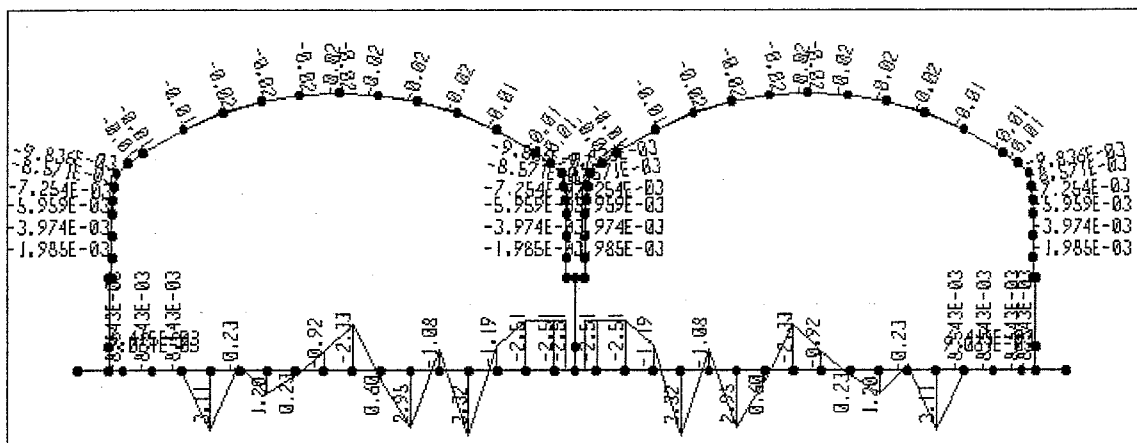


<CASE3 SAP2000모델링>

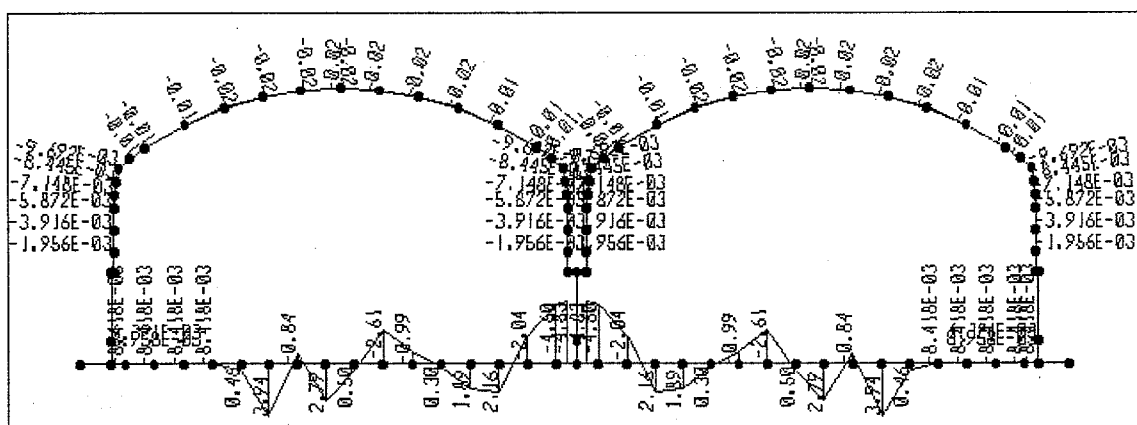
3. 해석결과

3.1 모멘트 검토결과(극한강도)

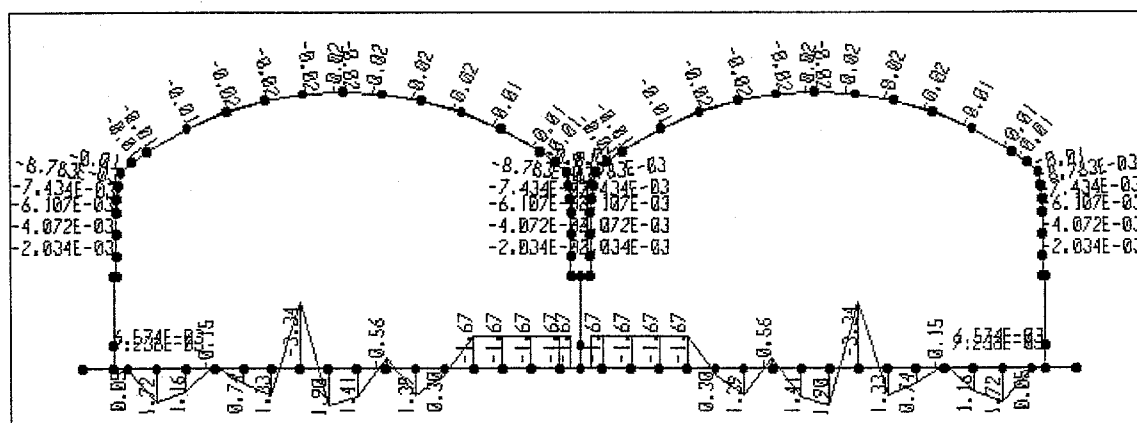
절점	상시MAX	CASE1	CASE2	CASE3	상시MAX +CASE1	상시MAX +CASE2	상시MAX +CASE3	비고
1	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
2	-25.21	0.00	0.00	0.00	-25.21	-25.21	-25.21	25.21
3	-52.63	0.00	0.00	0.00	-52.63	-52.63	-52.63	52.63
4	-82.03	-0.01	-0.01	-0.01	-82.04	-82.04	-82.04	82.04
5	-99.67	-0.01	-0.01	-0.01	-99.68	-99.68	-99.68	99.68
6	-113.13	-0.01	-0.01	-0.01	-113.14	-113.14	-113.14	113.14
7	-127.57	-0.01	-0.01	-0.01	-127.58	-127.58	-127.58	127.58
8	-104.86	-0.01	-0.01	-0.01	-104.87	-104.87	-104.87	104.87
9	-80.08	-0.01	-0.01	-0.01	-80.09	-80.09	-80.09	80.09
10	-27.13	-0.01	-0.01	-0.01	-27.14	-27.14	-27.14	27.14
11	12.91	-0.02	-0.02	-0.02	12.89	12.89	12.89	12.91
12	32.44	-0.02	-0.02	-0.02	32.42	32.42	32.42	32.44
13	46.00	-0.02	-0.02	-0.02	45.98	45.98	45.98	46.00
14	50.87	-0.02	-0.02	-0.02	50.85	50.85	50.85	50.87
15	45.99	-0.02	-0.02	-0.02	45.97	45.97	45.97	45.99
16	32.41	-0.02	-0.02	-0.02	32.39	32.39	32.39	32.41
17	8.81	-0.02	-0.02	-0.02	8.79	8.79	8.79	8.81
18	-30.07	-0.01	-0.01	-0.01	-30.08	-30.08	-30.08	30.08
19	-80.20	-0.01	-0.01	-0.01	-80.21	-80.21	-80.21	80.21
20	-105.69	-0.01	-0.01	-0.01	-105.70	-105.70	-105.70	105.70
21	-127.71	-0.01	-0.01	-0.01	-127.72	-127.72	-127.72	127.72
22	-114.96	-0.01	-0.01	-0.01	-114.97	-114.97	-114.97	114.97
23	-99.92	-0.01	-0.01	-0.01	-99.93	-99.93	-99.93	99.93
24	-82.03	-0.01	-0.01	-0.01	-82.04	-82.04	-82.04	82.04
25	-52.63	0.00	0.00	0.00	-52.63	-52.63	-52.63	52.63
26	-25.21	0.00	0.00	0.00	-25.21	-25.21	-25.21	25.21
27	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
101	9.79	0.00	0.00	0.00	9.79	9.79	9.79	9.79
102	54.71	0.01	0.01	0.01	54.72	54.72	54.72	54.72
401	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
402	52.13	-0.01	0.00	0.00	52.12	52.13	52.13	52.13
403	88.54	-0.01	0.00	0.05	88.53	88.54	88.59	88.59
404	42.20	-0.01	0.00	1.72	42.19	42.20	43.92	43.92
405	-29.79	-0.01	0.00	1.16	-29.80	-29.79	-28.63	29.80
406	-58.06	3.11	0.00	-0.15	-54.95	-58.06	-58.21	58.21
407	-79.29	-0.23	0.46	0.74	-79.52	-78.83	-78.55	79.52
408	-93.49	1.20	3.94	1.33	-92.29	-89.55	-92.16	93.49
409	-100.67	0.23	-0.84	-3.34	-100.44	-101.51	-104.01	104.01
410	-100.79	-0.92	2.79	1.90	-101.71	-98.00	-98.89	101.71
411	-93.89	-2.33	0.50	1.41	-96.22	-93.39	-92.48	96.22
412	-79.93	0.60	-2.61	-0.56	-79.33	-82.54	-80.49	82.54
413	-58.95	2.95	-0.99	1.39	-56.00	-59.94	-57.56	59.94
414	-34.29	-1.08	0.30	0.30	-35.37	-33.99	-33.99	35.37
415	-13.08	3.30	1.89	-1.67	-9.78	-11.19	-14.75	14.75
416	46.24	-1.19	2.16	-1.67	45.05	48.40	44.57	48.40
417	95.37	-2.51	-2.04	-1.67	92.86	93.33	93.70	95.37
418	151.59	-2.51	-4.60	-1.67	149.08	146.99	149.92	151.59



<CASE1>



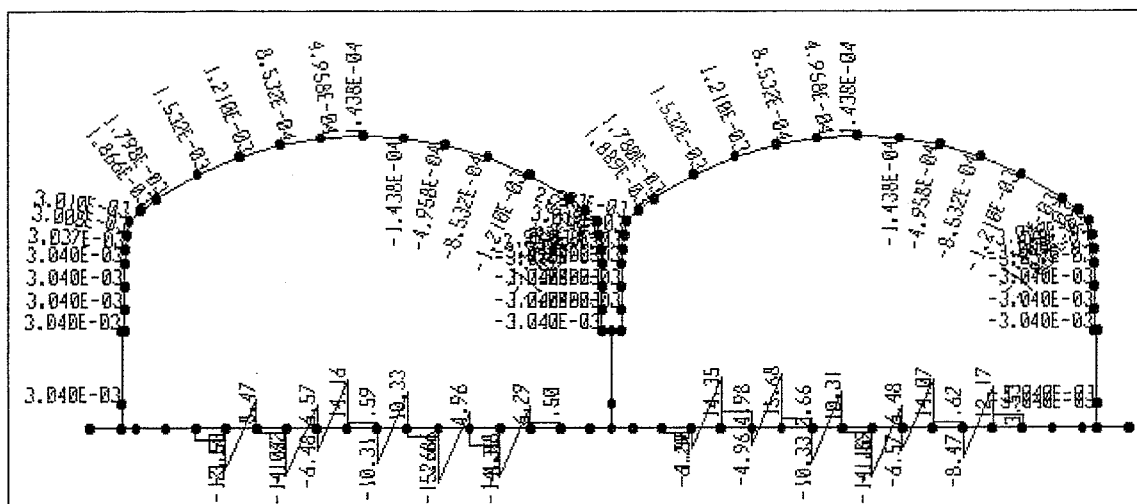
<CASE2>



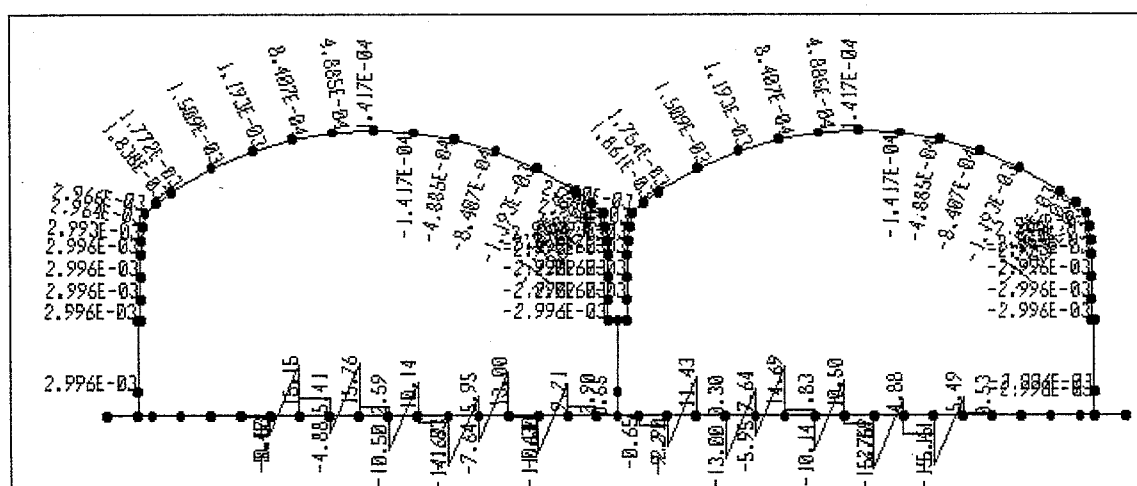
<CASE3>

3.2 전단력 검토결과(극한강도)

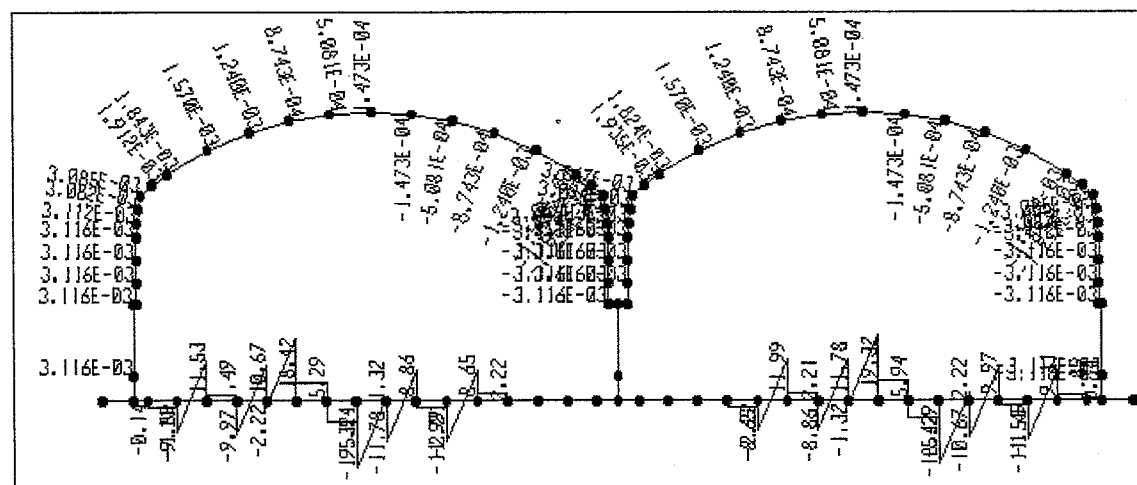
절점	상시MAX	CASE1	CASE2	CASE3	상시MAX +CASE1	상시MAX +CASE2	상시MAX +CASE3	비고
1	36.84	0.00	0.00	0.00	36.84	36.84	36.84	36.84
2	40.31	0.00	0.00	0.00	40.31	40.31	40.31	40.31
3	43.52	0.00	0.00	0.00	43.52	43.52	43.52	43.52
4	46.46	0.00	0.00	0.00	46.46	46.46	46.46	46.46
5	42.25	0.00	0.00	0.00	42.25	42.25	42.25	42.25
6	34.69	0.00	0.00	0.00	34.69	34.69	34.69	34.69
7	54.04	0.00	0.00	0.00	54.04	54.04	54.04	54.04
8	48.79	0.00	0.00	0.00	48.79	48.79	48.79	48.79
9	49.29	0.00	0.00	0.00	49.29	49.29	49.29	49.29
10	37.07	0.00	0.00	0.00	37.07	37.07	37.07	37.07
11	27.36	0.00	0.00	0.00	27.36	27.36	27.36	27.36
12	18.93	0.00	0.00	0.00	18.93	18.93	18.93	18.93
13	11.43	0.00	0.00	0.00	11.43	11.43	11.43	11.43
14	5.26	0.00	0.00	0.00	5.26	5.26	5.26	5.26
15	11.45	0.00	0.00	0.00	11.45	11.45	11.45	11.45
16	18.94	0.00	0.00	0.00	18.94	18.94	18.94	18.94
17	27.37	0.00	0.00	0.00	27.37	27.37	27.37	27.37
18	37.08	0.00	0.00	0.00	37.08	37.08	37.08	37.08
19	49.30	0.00	0.00	0.00	49.30	49.30	49.30	49.30
20	49.63	0.00	0.00	0.00	49.63	49.63	49.63	49.63
21	53.02	0.00	0.00	0.00	53.02	53.02	53.02	53.02
22	37.57	0.00	0.00	0.00	37.57	37.57	37.57	37.57
23	42.85	0.00	0.00	0.00	42.85	42.85	42.85	42.85
24	46.46	0.00	0.00	0.00	46.46	46.46	46.46	46.46
25	43.52	0.00	0.00	0.00	43.52	43.52	43.52	43.52
26	40.31	0.00	0.00	0.00	40.31	40.31	40.31	40.31
27	36.84	0.00	0.00	0.00	36.84	36.84	36.84	36.84
101	36.84	0.00	0.00	0.00	36.84	36.84	36.84	36.84
102	36.81	0.00	0.00	0.00	36.81	36.81	36.81	36.81
401	-54.25	0.00	0.00	0.00	-54.25	-54.25	-54.25	54.25
402	-60.53	0.00	0.00	0.00	-60.53	-60.53	-60.53	60.53
403	56.46	0.00	0.00	-1.89	56.46	56.46	54.57	56.46
404	48.50	0.00	0.00	-9.11	48.50	48.50	39.39	48.50
405	40.52	-3.53	0.00	11.53	36.99	40.52	52.05	52.05
406	32.56	-12.17	-0.53	-9.97	20.39	32.03	22.59	32.56
407	24.59	8.47	-5.49	10.67	33.06	19.10	35.26	35.26
408	16.63	-14.07	15.15	18.35	2.56	31.78	34.98	34.98
409	8.65	6.57	5.41	5.29	15.22	14.06	13.94	15.22
410	-3.84	14.16	15.76	-19.32	10.32	11.92	-23.16	23.16
411	-11.80	-10.31	-10.50	-11.78	-22.11	-22.30	-23.58	23.58
412	-19.78	10.33	10.14	8.86	-9.45	-9.64	-10.92	19.78
413	-27.74	-15.68	-14.69	-11.99	-43.42	-42.43	-39.73	43.42
414	-35.71	4.96	-7.64	8.65	-30.75	-43.35	-27.06	43.35
415	-43.68	-14.35	13.00	2.22	-58.03	-30.68	-41.46	58.03
416	-51.65	6.29	-11.43	0.00	-45.36	-63.08	-51.65	63.08
417	-59.61	1.50	9.21	0.00	-58.11	-50.40	-59.61	59.61
418	-101.37	0.00	2.90	0.00	-101.37	-98.47	-101.37	101.37



<CASE1>



<CASE2>



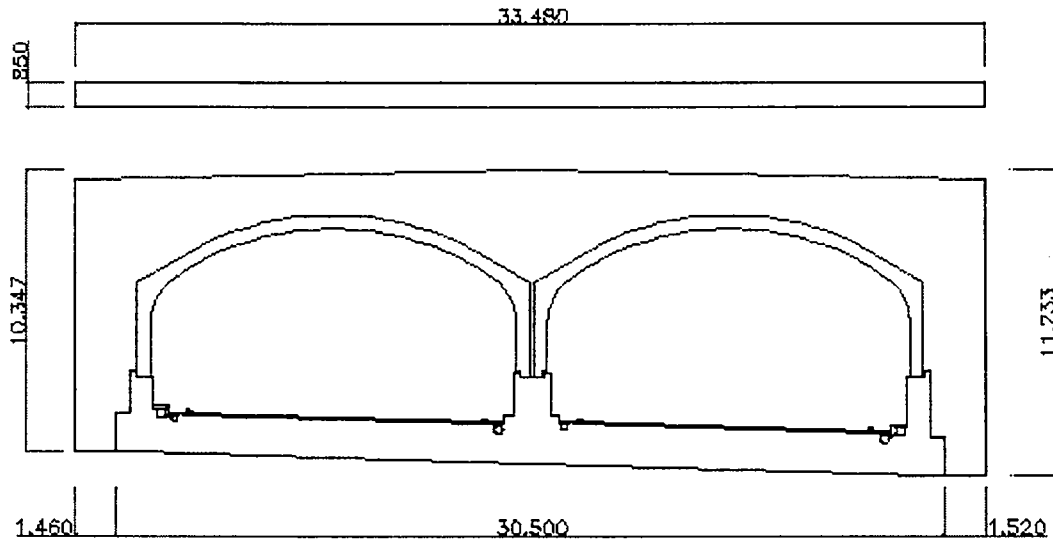
<CASE3>

5) 마 감 벽

1. 검토 내용

- P.A.B를 적용하여 복개 아치 시공 후 복개 아치 라멘의 전, 후면에 마감벽을 시공하도록함.
- 마감벽은 독립기초 벽체와 P.A.B에 커플러로 연결한다.

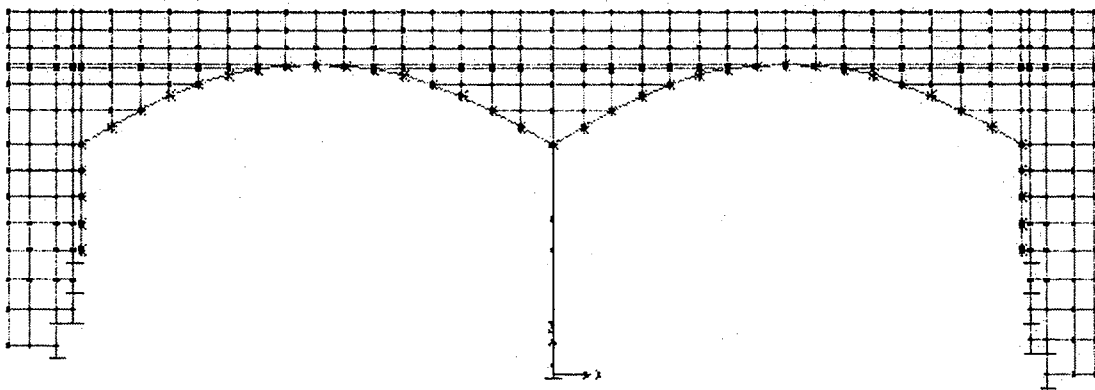
2. 마감벽 단면



3. 검토 방법

- 마감벽을 Sap2000을 이용하여 Shell(Thick)으로 모델링하여 검토함.

1) 모델링



① P.A.B 연결부

P.A.B와 마감벽이 커플러에 의해 연결되므로 P.A.B의 거동이 마감벽에 영향을 미치는 것을 구속조건에 고려하여야한다. 마감벽 설계에 필요한 결과는 Z축 방향의 처짐과 X,Z축의 회전이므로 U2,R2,R3를 고정시켜서 입력함.

② 기초 연결부

P.A.B와 마감벽이 커플러에 의해 연결되고 기초가 고정이므로 고정단

2) 구조물 및 토질 설계 제원

① 콘크리트 & 철근 제원

- $f_{ck} = 270 \text{ kg/cm}^2$
- $f_y = 4000 \text{ kg/cm}^2$

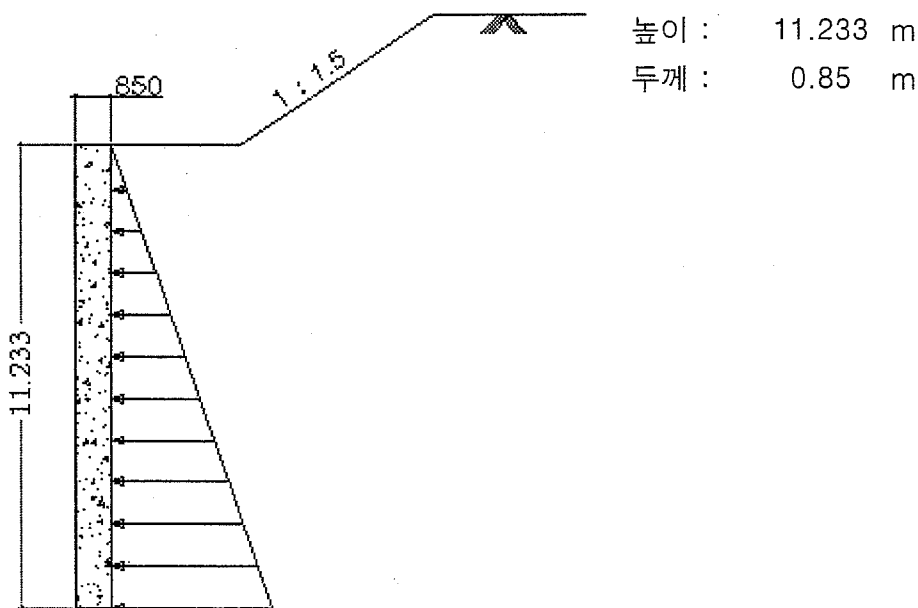
② 토질 정수

- 뒷채움, 토피 흙 $\gamma_s = 1.9 \text{ t/m}^3$
- 흙 내부 마찰각 $\phi = 30^\circ$
- 성토구배각도 $\beta = \tan^{-1}(1/1.5) = 33.69^\circ$
- 정지토압 : $K_0 = (1 - \sin\phi)(1 + \sin\beta) = (1 - \sin 30)(1 + \sin 33.69) = 0.777$

3) 절점 구속조건

- 현장타설 마감벽과 P.A.B의 현장타설 벽체부는 커플러를 이용하여 상호간 체결하도록 함.
- P.A.B 상부슬래브와 마감벽의 이음부는 P.A.B로부터 커플러를 이용하여 마감벽과 이음함

4) 작용하중산정



① 사하중 : SAP2000 입력 데이터 참조

② 토압 $Ph = \frac{1}{2} \times 1.9 \times 11.233^2 = 0.000$

5) 하중조합

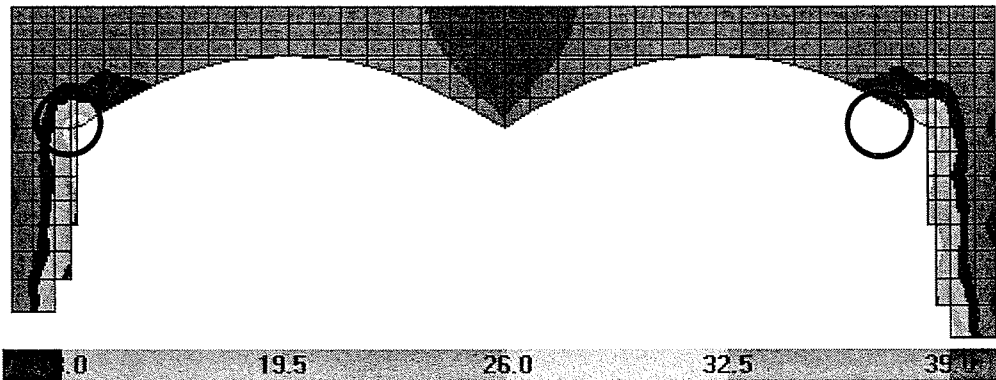
CASE1 = 사하중 + 수평토압

CASE2 = 1.3 사하중 + 1.7수평토압 (도로교 설계 기준 적용)

4.검토결과

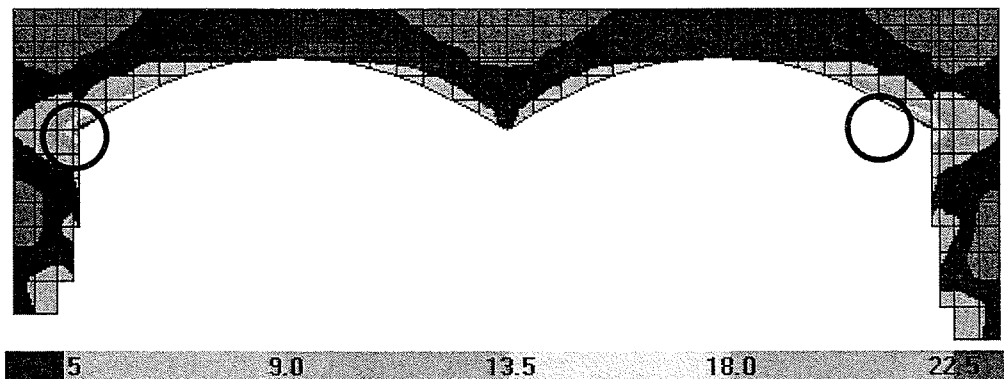
- 단면 설계시에는 CASE2 , 처짐검토시에는 CASE1을 활용함.

1) Mu11(수평방향 모멘트 검토)



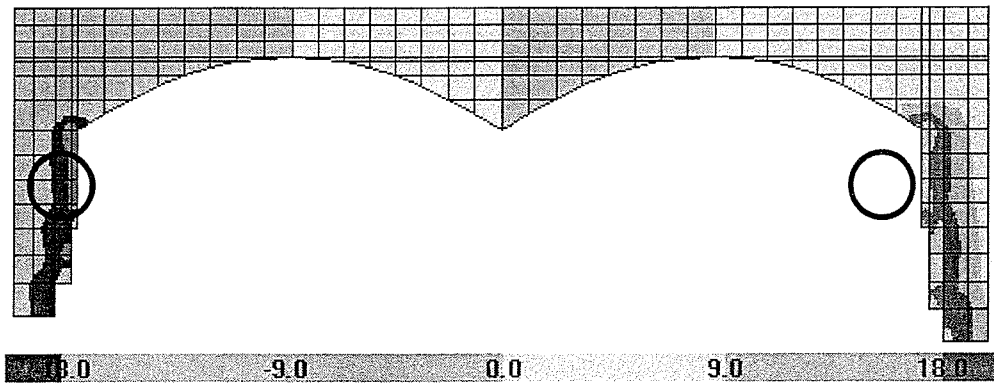
MAX Mu11 = 38.0 t-m

2) Mu22(연직방향 모멘트 검토)



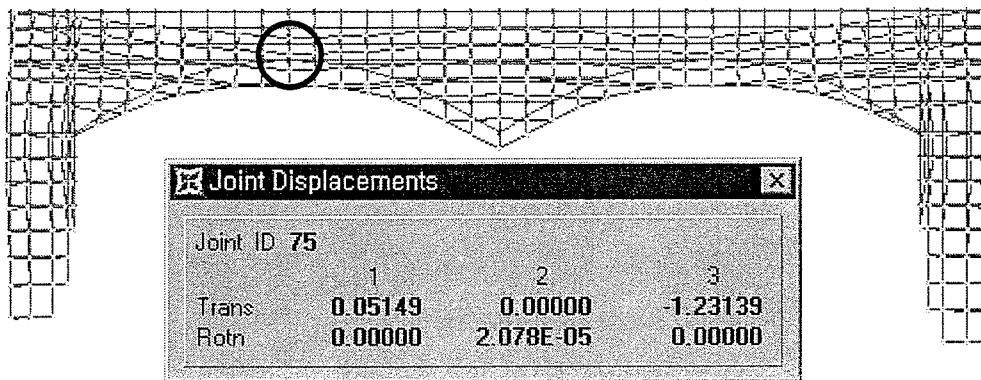
MAX Mu22 = 24.00 t-m

3) V13 (수평방향 전단력)

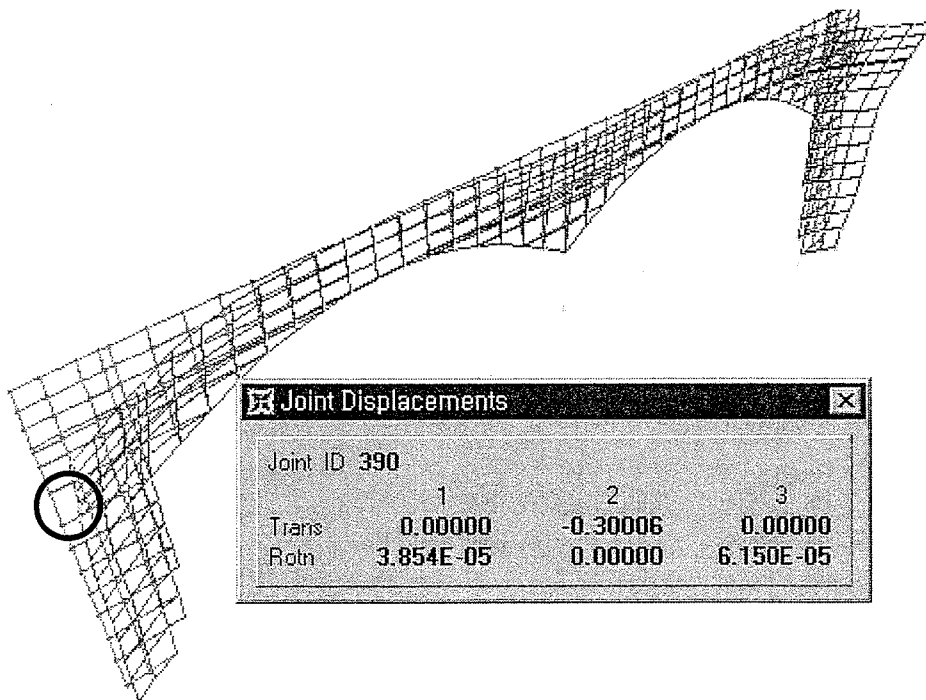


V13 = 31.00 t

3) 처짐량 검토



연직 처짐량 : P.A.R Arch 슬래브 상단에서의 연직 방향 처짐량은 1.230mm



마감벽의 수평 변위 : 마감벽 배면에서 토압으로 인해 발생하는 변위량은 구조물 전면으로 0.300mm가 발생되는 것으로 검토되었음.

4) 철근량 계산

① 수평방향 검토 (Mu11)

▷ 검토 조건

$$\begin{aligned}f_{ck} &= 270.0 \text{ kgf/cm}^2 & f_y &= 4000.0 \text{ kgf/cm}^2 \\ \beta_1 &= 0.850 & \phi_b &= 0.85 & \phi_s &= 0.80 \\ p_b &= (0.85 \times \beta_1 \times f_{ck} / f_y) \times [6000 / (6000 + f_y)] = 0.02926 \\ p_{\max} &= 0.75 \times p_b = 0.02195 \\ p_{\min} &= \max(0.80 \sqrt{f_{ck}} / f_y, 14 / f_y) = 0.00350\end{aligned}$$

$$\begin{aligned}\text{계수 모멘트 } M_u &= 38.000 \text{ tf}\cdot\text{m} \\ \text{단면의 두께 } H &= 85.000 \text{ cm} & \text{단면 폭 } B &= 100.000 \text{ cm} \\ \text{유효 깊이 } D &= 75.000 \text{ cm} & \text{피복 두께 } D_c &= 10.000 \text{ cm}\end{aligned}$$

▷ 휨모멘트 검토

$$\begin{aligned}\text{소요등가응력깊이 } a &= 2.644 \text{ cm로 가정} \\ A_s &= M_u / \{\phi_b \cdot f_y \cdot (D - a/2)\} = 15.169 \text{ cm}^2 \\ a &= (A_s \cdot f_y) / (0.85 \cdot f_{ck} \cdot B) = 2.644 \text{ cm} \quad \therefore \text{가정과 비슷함 O.K}\end{aligned}$$

$$\begin{aligned}P_{\text{req}} &= [M_u / \{\phi_b \cdot f_y \cdot (D - a/2)\}] / (B \cdot D) = 0.00202 \Rightarrow 4/3 P_{\text{req}} = 0.00270 \\ \therefore \text{필요철근량 } \text{req.} A_s &= P_{\text{req}} \times (B \cdot D) = 15.169 \text{ cm}^2\end{aligned}$$

$$\begin{aligned}\text{Used } A_s &= H22 @ 15.00 \text{ cm} \quad (D_c = 10.00 \text{ cm}) \\ &= 25.807 \text{ cm}^2 \quad \therefore P = A_s / (B \cdot D) = 0.00344\end{aligned}$$

$$4/3 P_{\text{req}} \leq P \leq P_{\min} \quad \therefore \text{O.K}$$

$$\begin{aligned}a &= (A_s \cdot f_y) / (0.85 \cdot f_{ck} \cdot B) = 4.498 \text{ cm} \\ \phi M_n &= \phi_b \cdot f_y \cdot A_s \cdot (D - a/2) = 6383371.000 \text{ kgf}\cdot\text{cm} \\ &= 63.834 \text{ tf}\cdot\text{m} \geq M_u = 38.000 \text{ tf}\cdot\text{m} \quad \therefore \text{O.K}\end{aligned}$$

② 수직방향 검토 (Mu22)

▷ 검토 조건

$$\begin{aligned} f_{ck} &= 270.0 \text{ kgf/cm}^2 & f_y &= 4000.0 \text{ kgf/cm}^2 \\ \beta_1 &= 0.850 & \phi_b &= 0.85 & \phi_s &= 0.80 \\ p_b &= (0.85 \times \beta_1 \times f_{ck} / f_y) \times [6000 / (6000 + f_y)] = 0.02926 \\ p_{\max} &= 0.75 \times p_b = 0.02195 \\ p_{\min} &= \max(0.80 \sqrt{f_{ck} / f_y}, 14 / f_y) = 0.00350 \end{aligned}$$

$$\begin{aligned} \text{계수 모멘트 } M_u &= 24.000 \text{ tf}\cdot\text{m} \\ \text{단면의 두께 } H &= 85.000 \text{ cm} & \text{단 면 폭 } B &= 100.000 \text{ cm} \\ \text{유효 깊이 } D &= 75.000 \text{ cm} & \text{피복 두께 } D_c &= 10.000 \text{ cm} \end{aligned}$$

▷ 휨모멘트 검토

$$\begin{aligned} \text{소요등가응력깊이 } a &= 1.659 \text{ cm로 가정} \\ A_s &= M_u / \{\phi_b \cdot f_y \cdot (D - a/2)\} = 9.517 \text{ cm}^2 \\ a &= (A_s \cdot f_y) / (0.85 \cdot f_{ck} \cdot B) = 1.659 \text{ cm} \quad \therefore \text{가정과 비슷함 O.K} \end{aligned}$$

$$\begin{aligned} P_{\text{req}} &= [M_u / \{\phi_b \cdot f_y \cdot (D - a/2)\}] / (B \cdot D) = 0.00127 \Rightarrow 4/3 P_{\text{req}} = 0.00169 \\ \therefore \text{필요철근량 } \text{req.} A_s &= P_{\text{req}} \times (B \cdot D) = 9.517 \text{ cm}^2 \end{aligned}$$

$$\begin{aligned} \text{Used } A_s &= H19 @ 15.00 \text{ cm} \quad (D_c = 10.00 \text{ cm}) \\ &= 19.100 \text{ cm}^2 \quad \therefore P = A_s / (B \cdot D) = 0.00255 \end{aligned}$$

$$4/3 P_{\text{req}} \leq P \leq P_{\min} \quad \therefore \text{O.K}$$

$$\begin{aligned} a &= (A_s \cdot f_y) / (0.85 \cdot f_{ck} \cdot B) = 3.329 \text{ cm} \\ \phi M_n &= \phi_b \cdot f_y \cdot A_s \cdot (D - a/2) = 4762408.000 \text{ kgf}\cdot\text{cm} \\ &= 47.624 \text{ tf}\cdot\text{m} \geq M_u = 24.000 \text{ tf}\cdot\text{m} \quad \therefore \text{O.K} \end{aligned}$$

③ 수평방향 전단 검토 (V13)

▷ 검토 조건

$$\begin{aligned}f_{ck} &= 270.0 \text{ kgf/cm}^2 & f_y &= 4000.0 \text{ kgf/cm}^2 \\ \beta_1 &= 0.850 & \phi_b &= 0.85 & \phi_s &= 0.80 \\ p_b &= (0.85 \times \beta_1 \times f_{ck} / f_y) \times [6000 / (6000 + f_y)] = 0.02926 \\ p_{\max} &= 0.75 \times p_b = 0.02195 \\ p_{\min} &= \max(0.80 \sqrt{f_{ck}} / f_y, 14 / f_y) = 0.00350\end{aligned}$$

$$\text{계수 전단력 } V_u = 31.000 \text{ tonf}$$

$$\text{단면의 두께 } H = 85.000 \text{ cm} \quad \text{단 면 폭 } B = 100.000 \text{ cm}$$

$$\text{유효 깊이 } D = 75.000 \text{ cm} \quad \text{피복 두께 } D_c = 10.000 \text{ cm}$$

▷ 전단력 검토

$$\text{콘크리트 설계전단강도 } \phi_v V_c = \phi_v \cdot 0.53 \sqrt{f_{ck}} \cdot B \cdot D / 1000 = 52.25 \text{ ton}$$

$$0.5 \cdot \phi_v V_c < V_u \leq \phi_v V_s \dots \text{최소 전단보강철근 필요}$$

$$\text{소요 } A_v/s = \text{최소 } A_v/s = (3.5 \cdot B) / f_y = 0.09 \text{ cm}^2/\text{cm}$$

$$\text{사용전단철근 : 철근(Ds)=H16} \quad \text{다리수(Ns)=2 EA} \quad \text{간격(s)=45.0 cm}$$

$$\text{사용철근량 } A_v = \text{철근면적} \cdot N_s = 3.97 \text{ cm}^2 > \text{소요철근량 } A_v = 3.94 \text{ cm}^2 \dots \text{만족}$$

$$\text{철근 설계전단강도 } \phi_v V_s = \phi_v \cdot A_v \cdot f_y \cdot D / (s \cdot 1000) = 21.18 \text{ ton}$$

$$\text{설계전단강도 } \phi_v V_n = \phi_v V_c + \phi_v V_s = 73.44 \text{ ton}$$

$$> \text{설계전단력 } V_u = 31.00 \text{ ton} \dots \text{만족}$$

6) LIFTING 안정검토

P.C Arch Box Segment의 시공중 안정성(인양 및 설치) 검토

가. 검토 목적

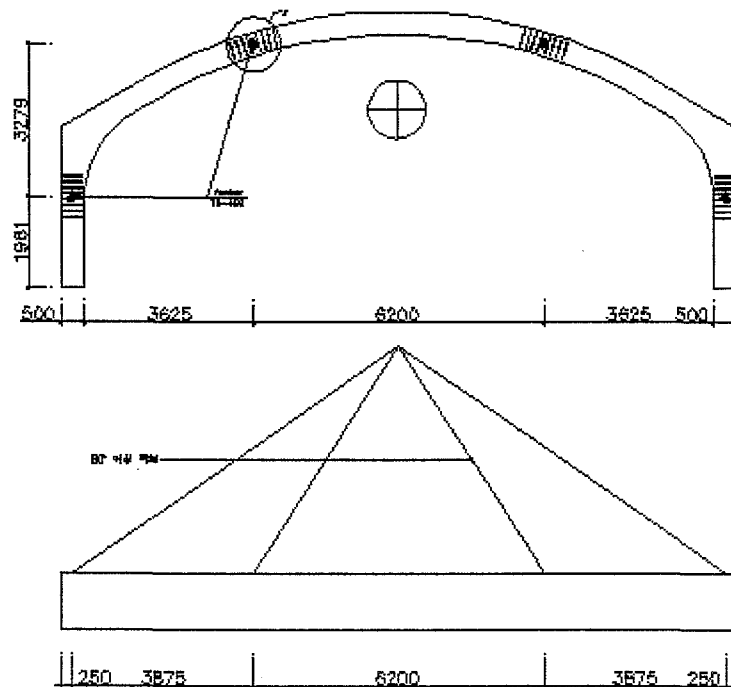
제작장에서 P.A.B를 바닥 거푸집에서 인양하여 야적장으로 옮기는 경우 케이블 연결부에서의 콘크리트 인장력 및 P.A.B 본체에서의 인장력 발생량을 검토하여 인양시 구조적으로 안정한지 확인하고자 한다.

제작된 P.A.B를 현장에서 조립 설치하기 위한 연결부의 위치가 적정하고 또한 P.A.B 본체에 미치는 영향을 확인함.

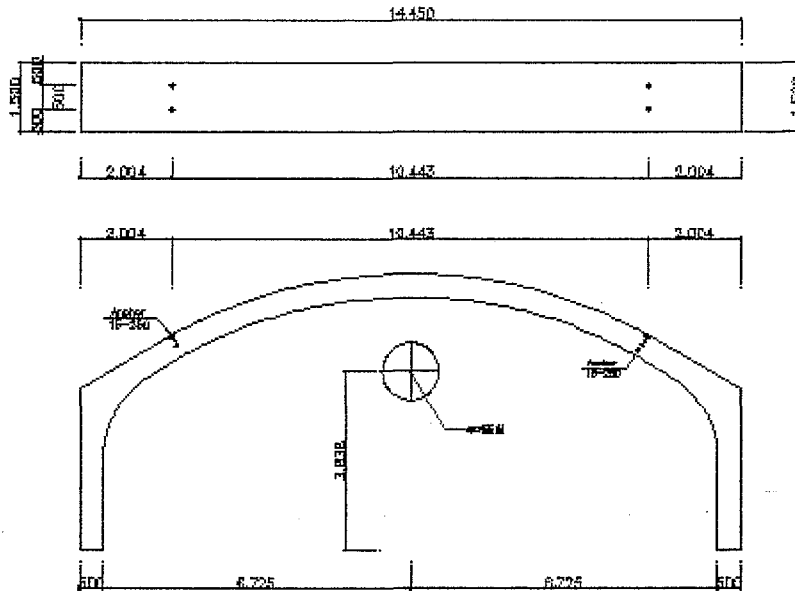
나. 검토 내용 및 결과

Cable의 길이 : 각 약 11m로 가정.

위치 : 그림 1, 2 참조



< 그림-1 탈형시 Anchor 위치도 >



< 그림-2 설치시 Anchor 위치도 >

1) P.A.B 구조물 본체 인양시

① 구조물 본체 응력

탈형시 강도 : $f_{ck} = 200 \text{ kg/cm}^2$ (가정)

허용휨인장응력 : $f_{ta} = 1.06 \sqrt{f_{ck}} = 15.0 \text{ kg/cm}^2$

(콘크리트 구조 설계 기준 15.3 (3) ① p243쪽)

P.A.B 구조물 본체에 걸쳐 전 구간이 허용휨인장응력이하 이므로 P.A.B 본체는 인양 중 구조적으로 안정함.

Anchor는 둘레에 철근을 보강하여 설치함. (그림 3, 4 참조)

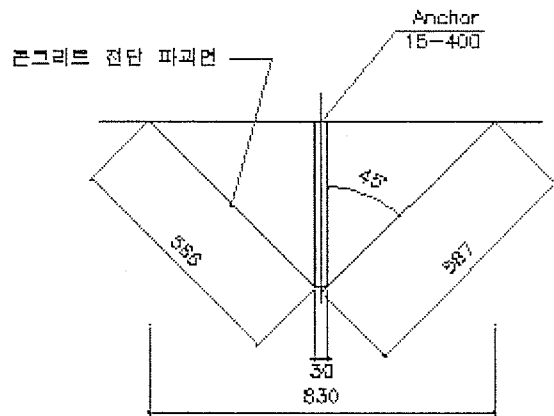
② 구조물 본체 처짐

탈형시 상단부 변위는 내측으로 0.0676mm, 하단부 변위는 내측으로 0.00225mm이며 운용 및 탈형시 구조물은 안전함. (그림 - 5, 6 참조)

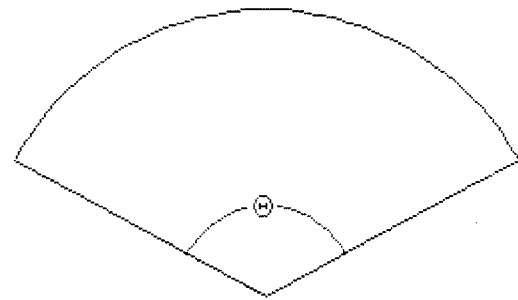
③ 구조물 인양시 인양고리에 대한 전단파괴 검토

PAB 1SEG 중량 : 42.75 ton

한개의 인양고리에 걸리는 하중 : $42.75/4 = 10.69$ ton (인양시 하중이 한쪽으로만 걸리는 경우)



< 콘크리트 전단 파괴형상 >



< 전단 파괴면 전개도 >

콘크리트 허용전단강도 = $0.25 \sqrt{f_{ck}} bd$ (도로교 설계기준 2000 p.28)

bd : 콘크리트 전단 파괴면의 넓이

전단 파괴면 전개도에서

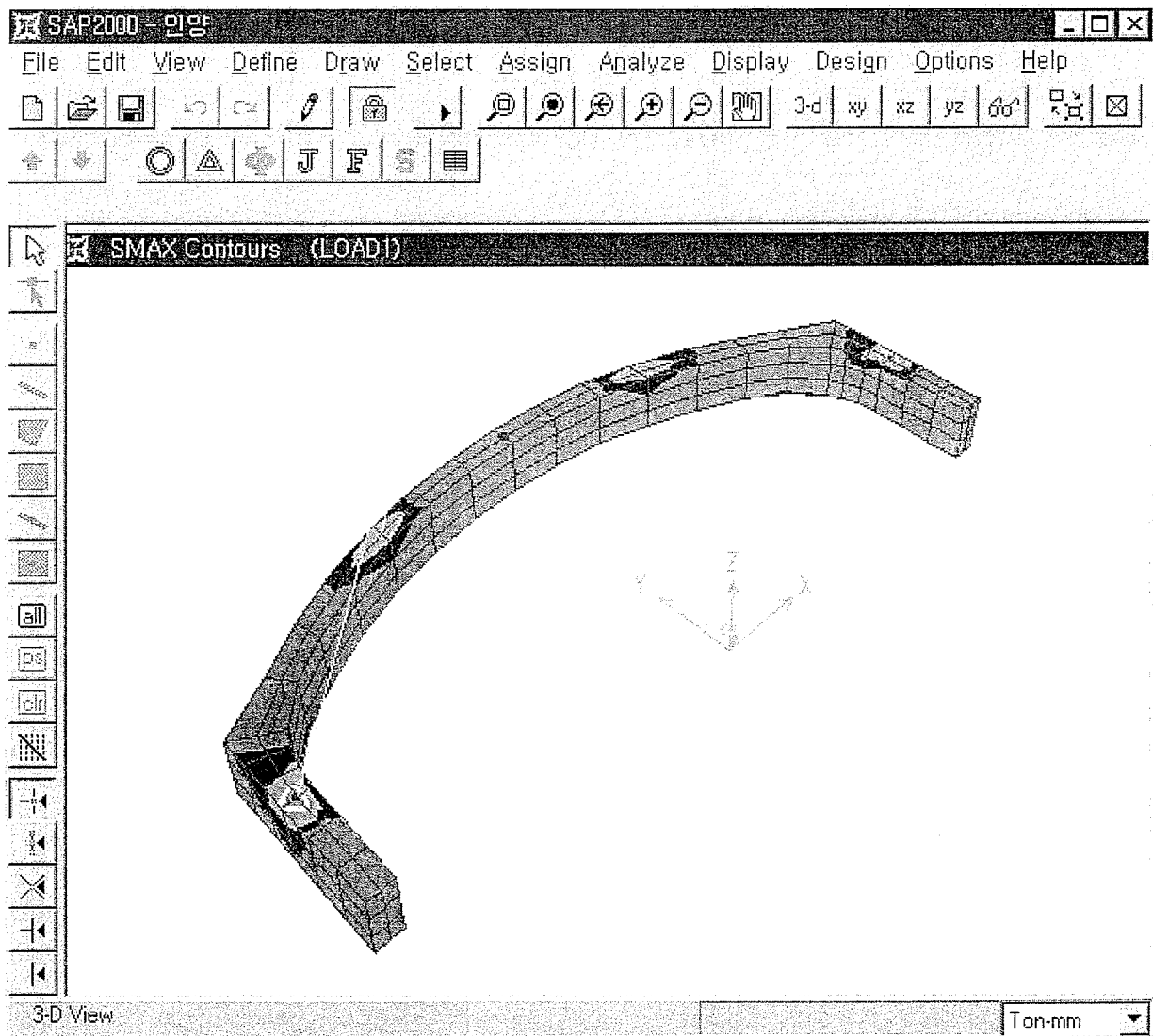
$$2 \times \frac{1}{2} \times 587 \times \theta / 360 = 2 \times \frac{1}{2} \times 830 / 2$$

$$\theta = 254.5^\circ$$

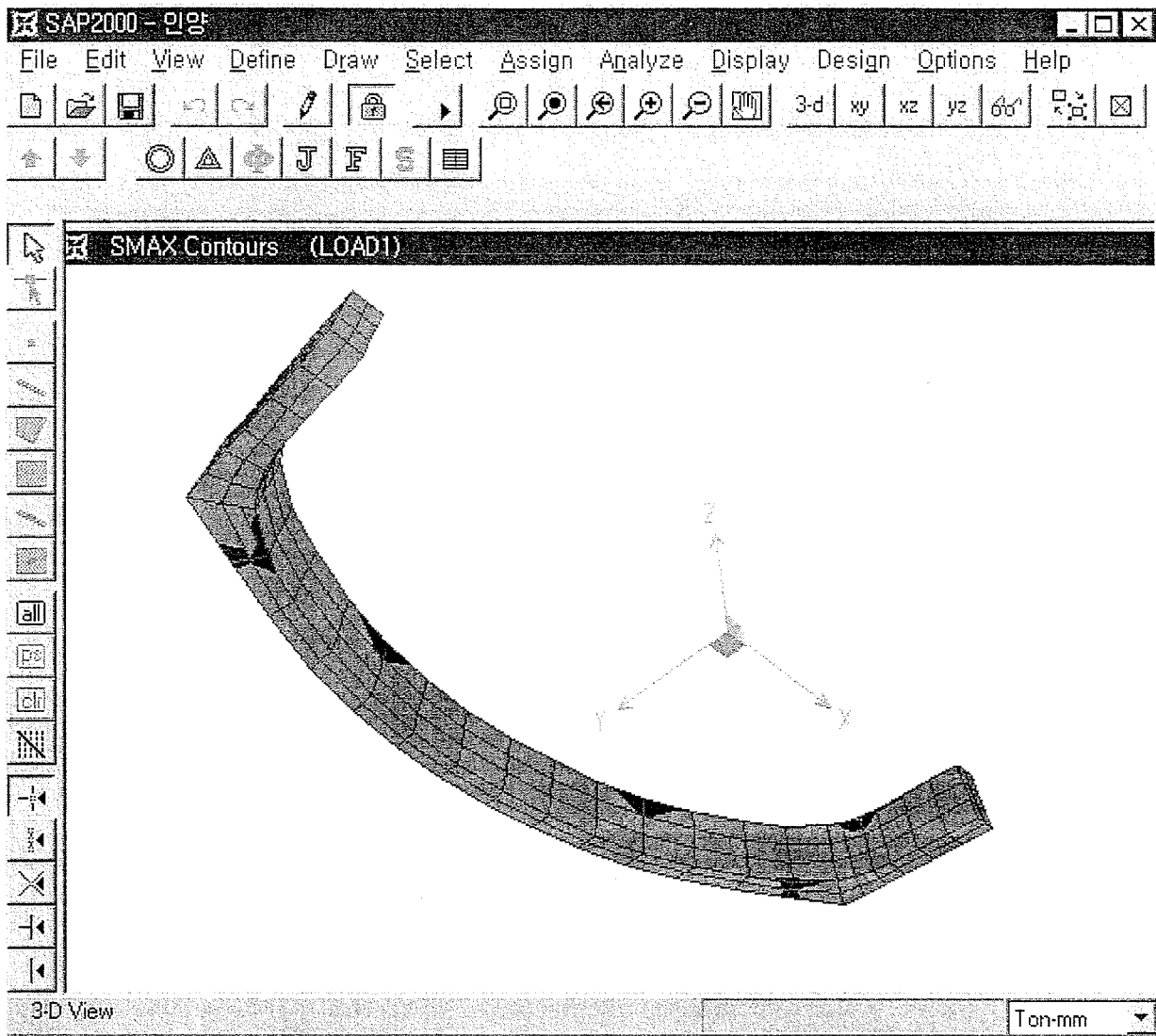
$$bd = \frac{1}{2} \times (587^2 - (587-566)^2) \times 254.5 / 360 = 764285 \text{ mm}^2 = 7642.85 \text{ cm}^2$$

$$\text{콘크리트 허용 전단강도} = 0.25 \sqrt{f_{ck}} bd = 0.25 \sqrt{200} \times 7642.85 = 27021.67 \text{ kg} = 27.021 \text{ ton}$$

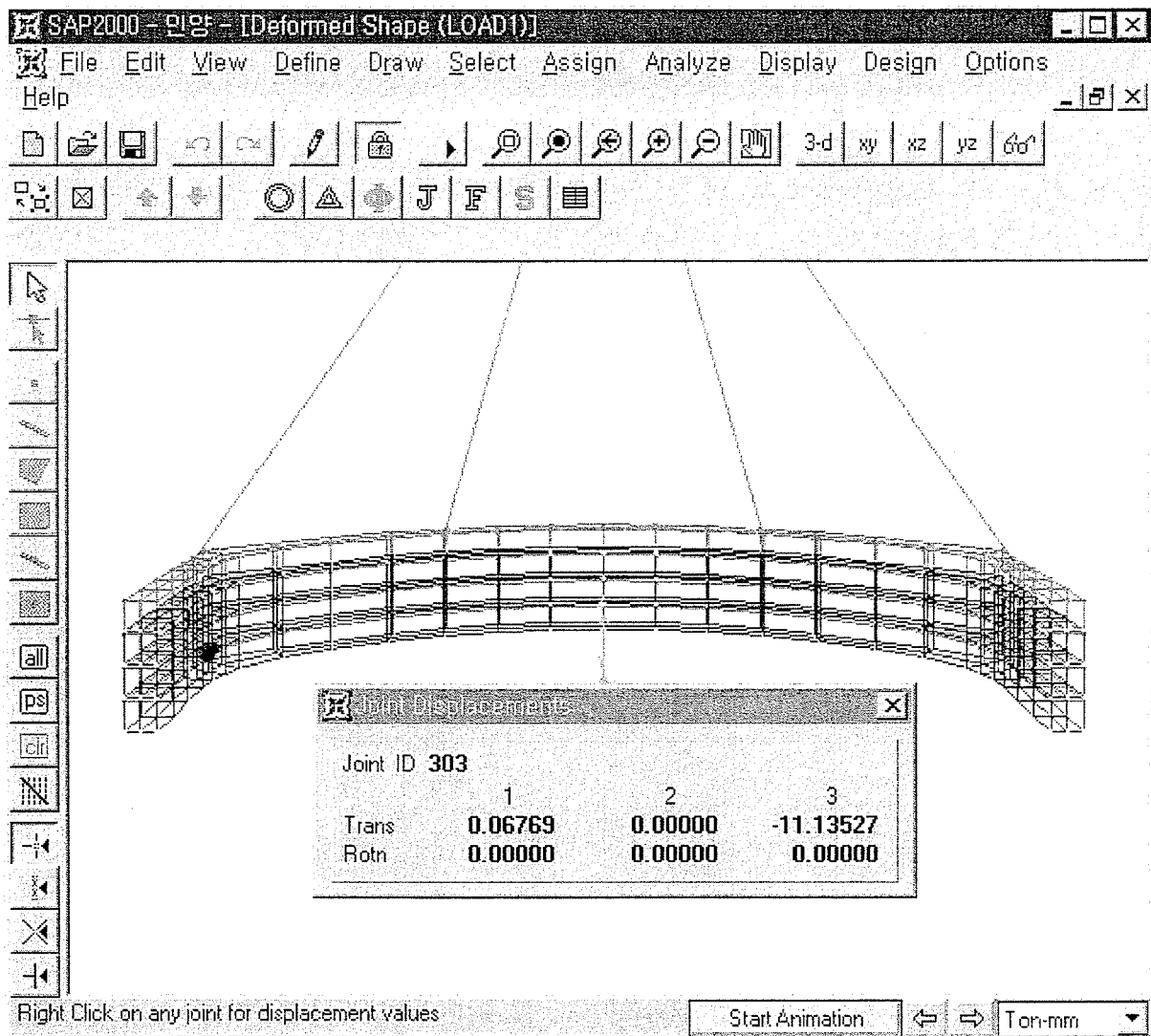
$27.021 > 10.69$ ton 이므로 전단파괴에 대해 안전함.



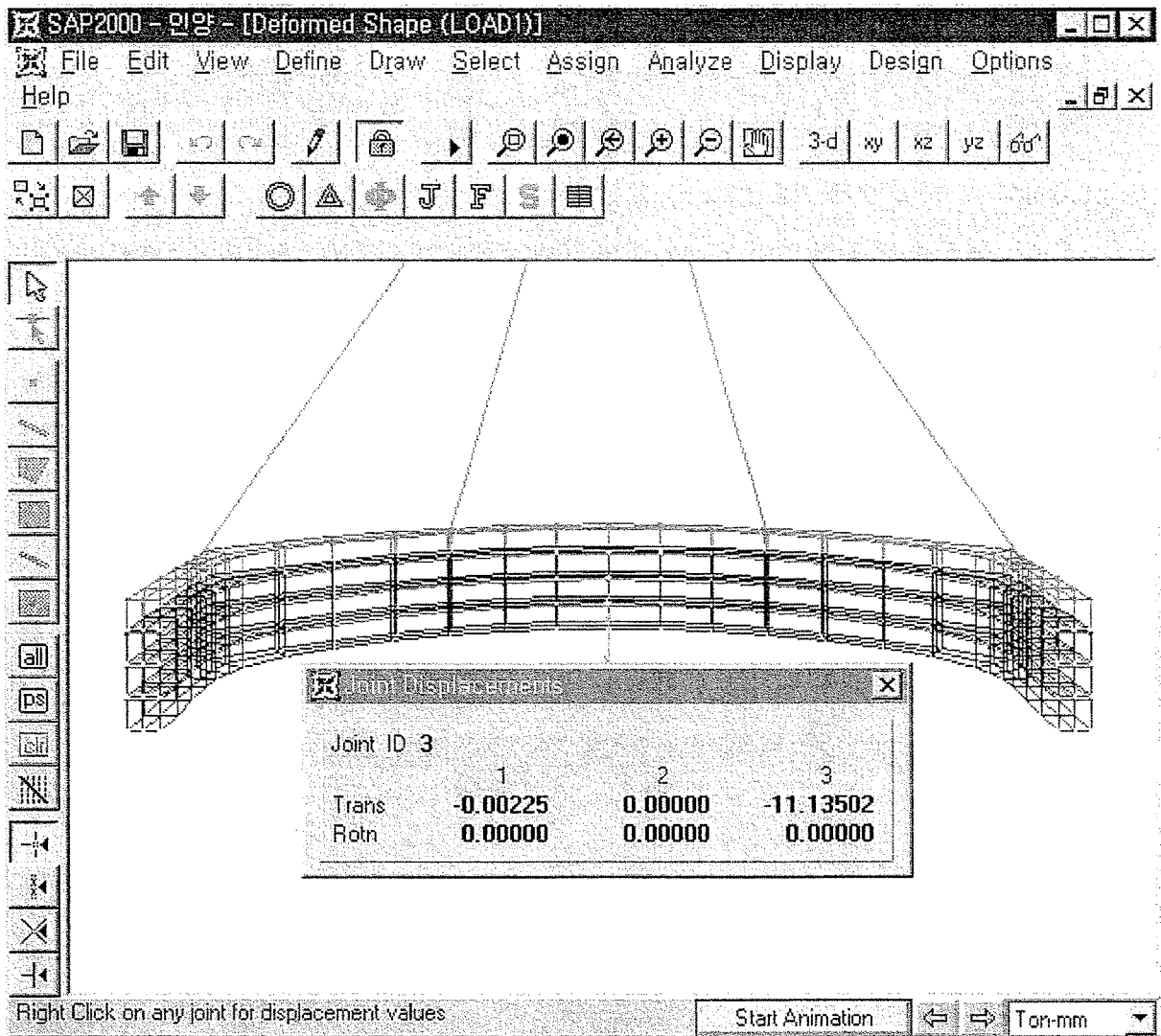
< 그림-3 인양시 P.A.B 상부 응력 분포도 >



< 그림-4 인양시 P.A.B 하부 응력 분포도 >



< 그림-5 인양시 P.A.B 상단에서의 변위 >



< 그림-6 민양시 P.A.B 하단에서의 변위 >

3) P.A.B구조물 본체 설치시

① 구조물 본체 응력

설치시 강도 : $f_{ck} = 400 \text{ kg/cm}^2$ (가정)

허용휨인장응력 : $f_{ta} = 1.06 \sqrt{f_{ck}} = 21.2 \text{ kg/cm}^2$

(콘크리트 구조 설계 기준 15.3 (3) ① p243쪽)

P.A.R 구조물 본체 및 Lifting Anchor 둘레에서의 발생인장 응력이 허용휨인장응력이하로 구조적으로 안정함. (그림 7, 8 참조)

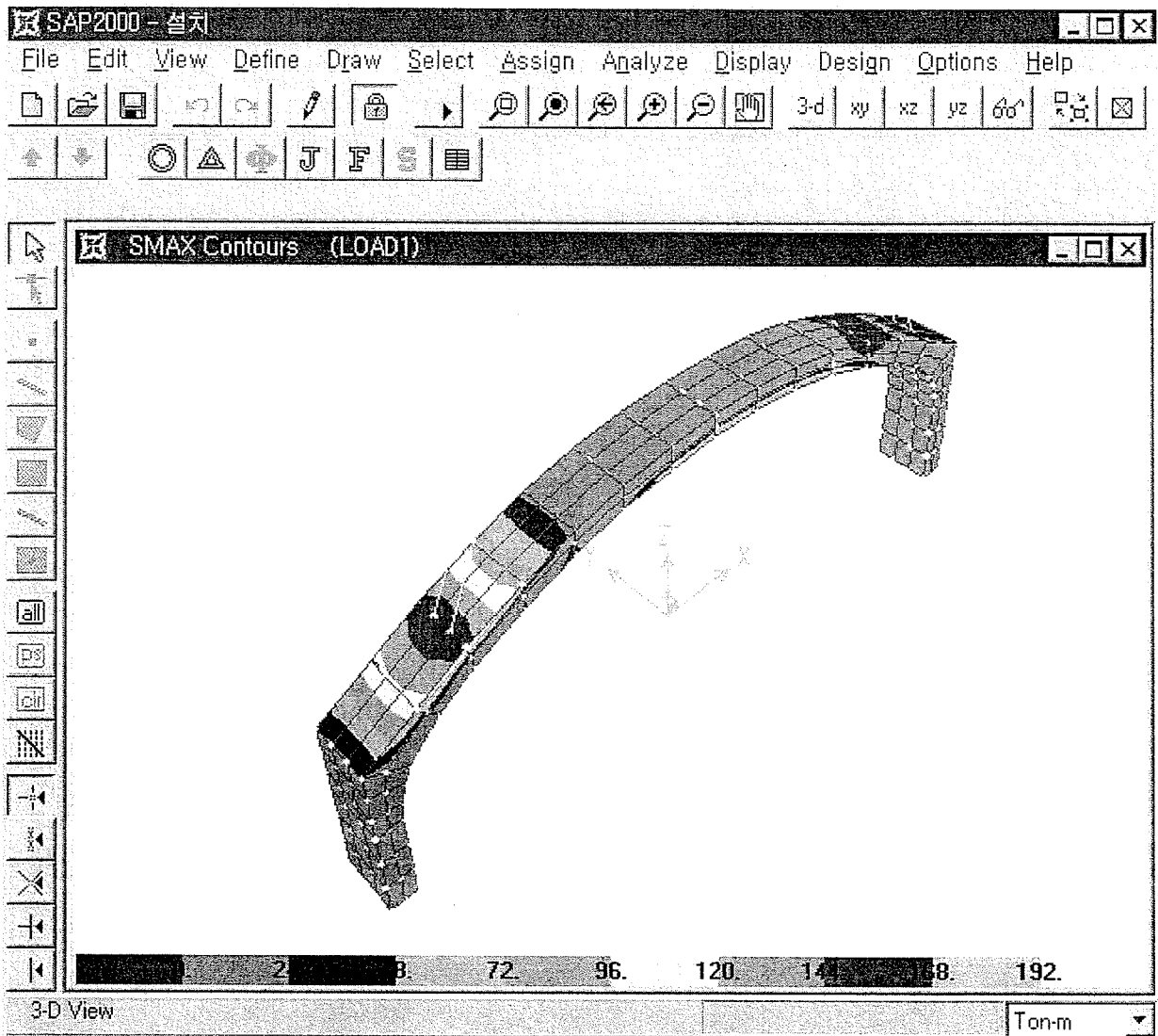
② 구조물 본체 처짐

설치시 P.A.B 벽체 하단부 변위는 내측으로 0.0958mm이며 변위량이 미소함.

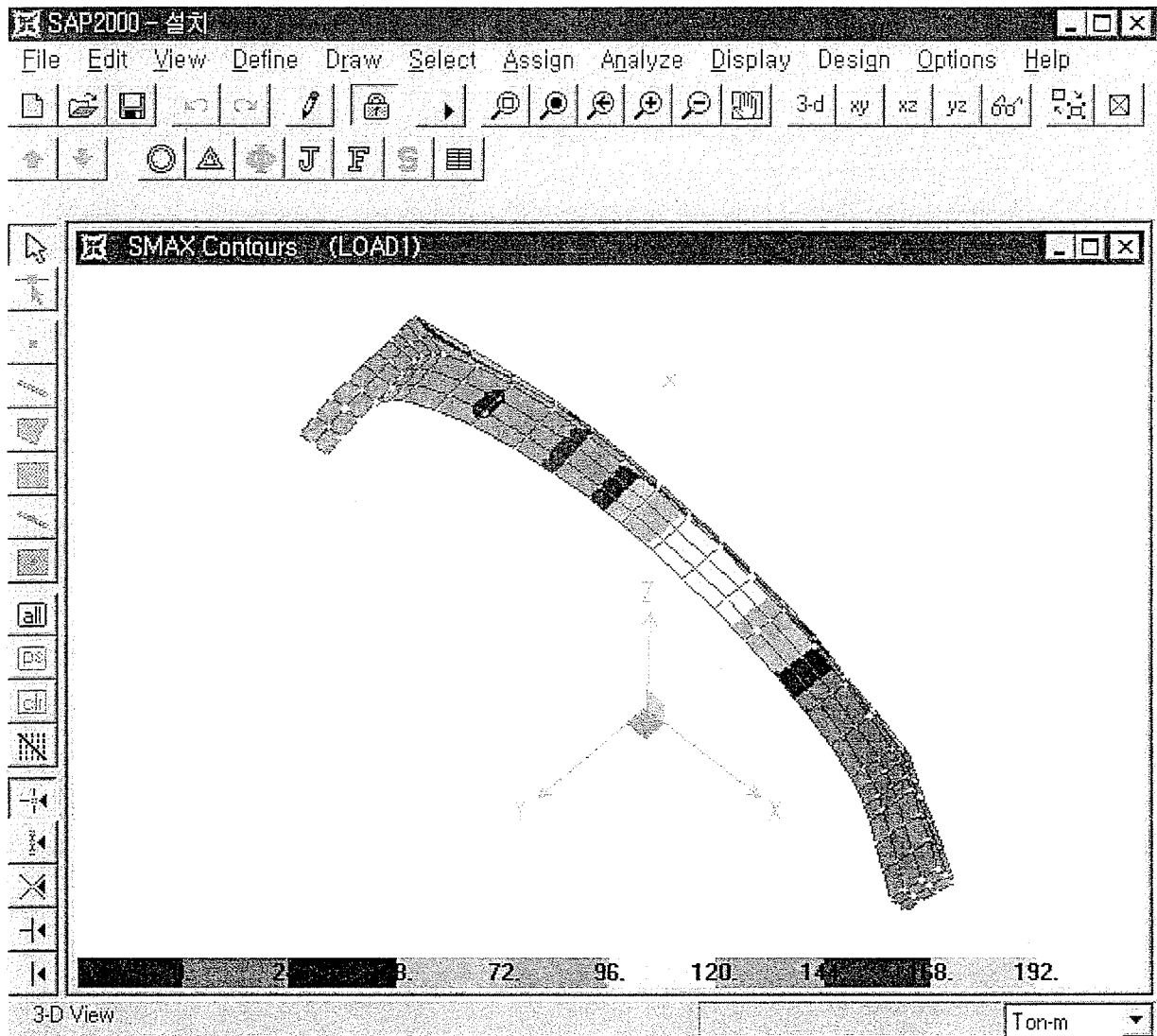
(그림 - 9 참조)

③ 구조물 설치시 인양고리에 대한 전단파괴 검토

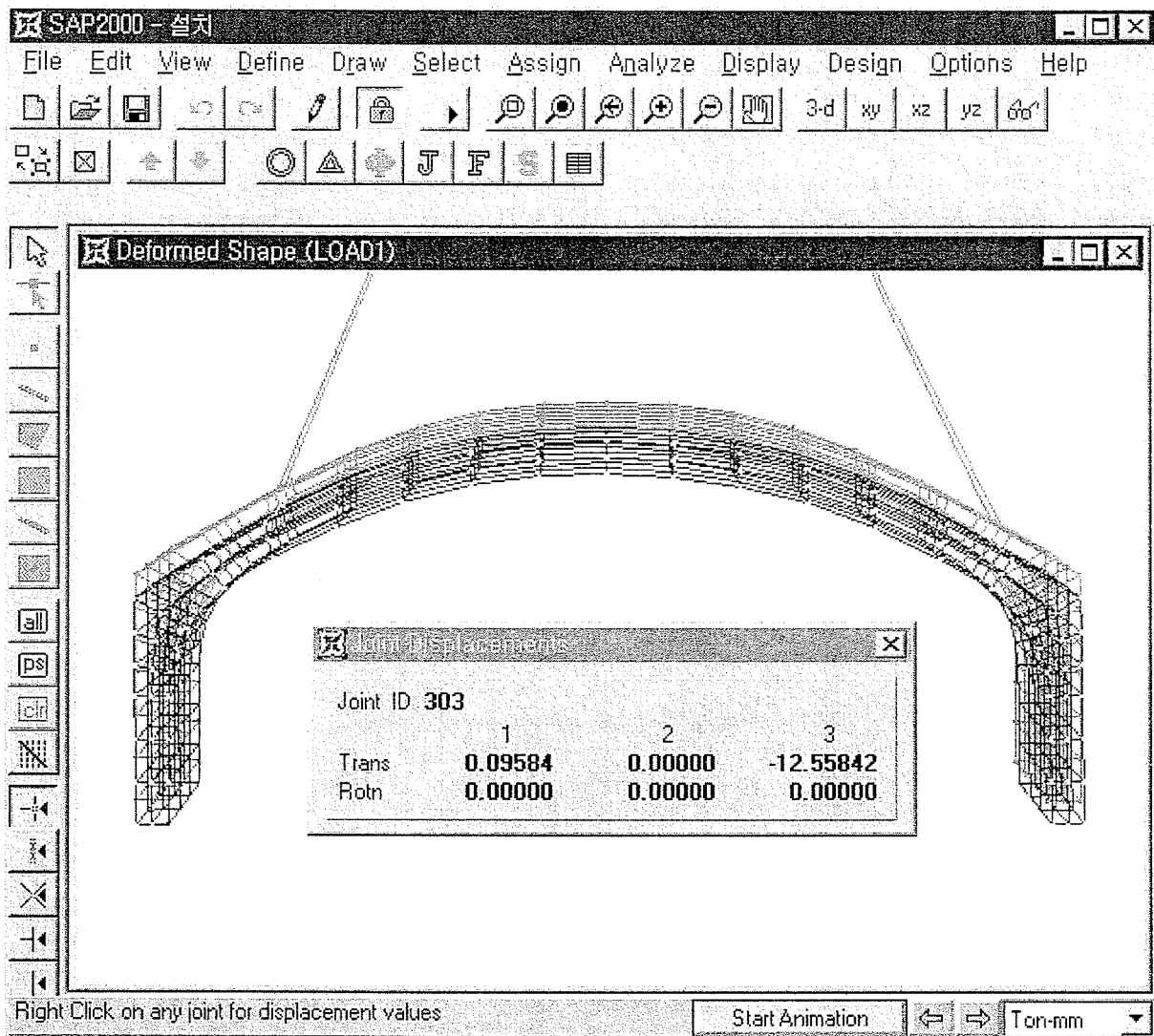
인양시와 같은 형상의 앵커를 사용하므로 인양시와 동일함.



< 그림-7 설치시 P.A.B 상부 응력 분포도 >



< 그림-8 설치시 P.A.B 하부 응력 분포도 >



< 그림-9 설치시 P.A.B 하단에서의 변위 >

7) 허용지지력 계산근거

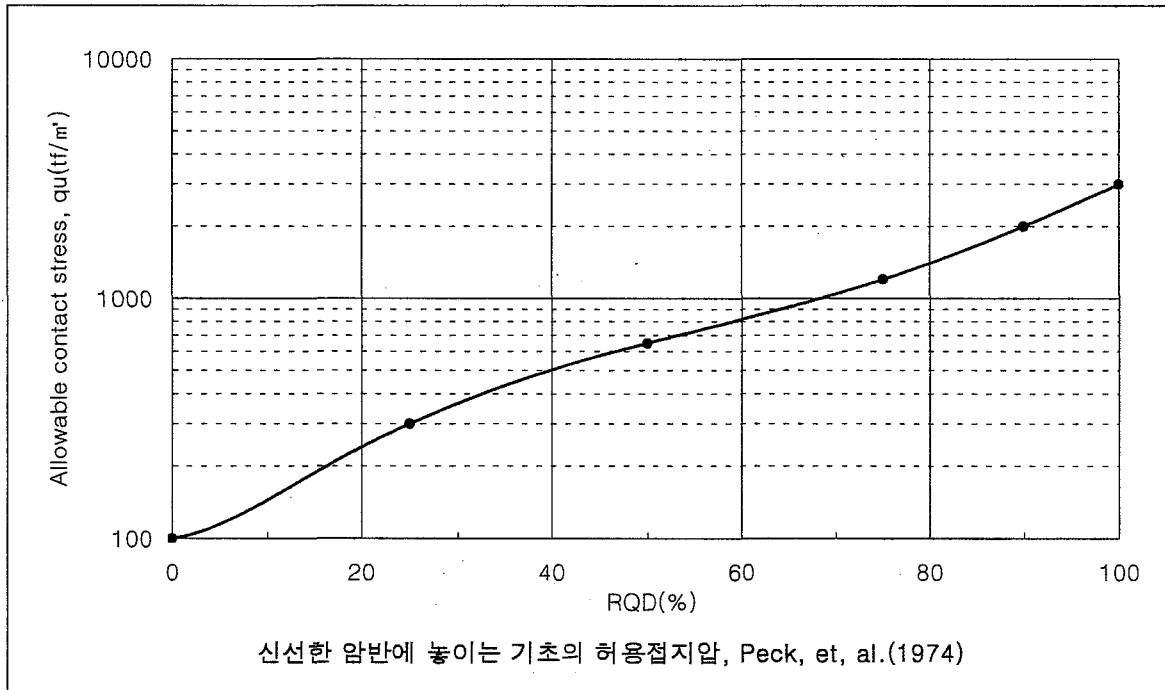
■ 암반에 지지되는 직접기초의 허용지지력

1. 지지층의 암반특성

위 치	공번	TCR/RQD (%)	일축압축강도 (kg/cm ²)	절리간격 (cm)	절리틈새 (mm)	비 고
터널부	CB-7	50 / 0	2,090	< 6	> 5	

2. Peck et. al.의 방법(1974) - 도로교설계기준해설(하부구조편, 2001. 9)

- 불연속면의 틈새가 치밀하게 밀착되었을 경우 적용(<3mm)
- RQD와 허용접지압과의 관계로부터 산정(RQD는 기초바닥면 아래 0.25B 이내의 암질을 적용)
- 단, 허용접지압(qa)이 무결암의 일축압축강도(qu)보다 크면 qa=qu로 간주한다.



• 허용지지력 산정

위 치	공번	TCR/RQD (%)	일축압축강도 (kg/cm ²)	절리틈새 (mm)	적용여부	qa (tf/m ²)	비 고
터널부	CB-7	50 / 0	2090	< 5	NG	-	

3. C.G.S(Canadian Geotechnical Society, 1985) 방법 - 도로교설계기준해설(하부구조편, 2001. 9)

- 파쇄나 절리가 발달한 암반(불연속면간격≥30cm, 틈새≥5mm인 경우, 수평하중이 없는 경우 적용)
- 단, 퇴적암반의 경우, 층리가 수평하여야 함.

여기서, qa : 허용지지력(kg/cm²)

$$q_a = K_{sp} \times q_u$$

$$K_{sp} = (3+C/Bf)/(10\sqrt{(1+300\delta/C)})$$

적용조건 : $0.05 < C/B_f < 2.0$

q_u : 코아의 평균일축압축강도(kg/cm²)

$0 < \delta/C < 0.02$

C : 불연속면의 간격(mm)

B_f : 기초폭(mm)

δ : 불연속면의 틈새(mm)

• 허용지지력 산정

위 치	공번	TCR/RQD (%)	일축강도 (kg/cm ²)	절리간격 (C,mm)	절리틈새 (δ , mm)	기초폭 (B _f ,mm)	C/B _f	δ/C	적용 여부	K _{sp}	q _a (tf/m ²)
터널부	CB-7	50 / 0	2090	< 60	> 5	#####	0.002	0.083	NG	-	-

4. AASHTO(1996) 방법 - 도로교설계기준해설(하부구조편, 2001. 9)

- 공학적 분류에 의해 암반의 상태를 정량적으로 평가할수 있는 경우 적용(최소안전율 3적용)

$$q_u = N_{ms} \times C_0$$

여기서, N_{ms} : 암석의 종류에 따라 정해지는 값

C_0 : 암석의 일축압축강도(kg/cm²)

- 파쇄나 절리가 발달한 암반에 놓인 기초의 극한지지력 산정을 위한 N_{ms} 계수(Hoek, 1983 의 자료 수정)

암반 등급	일반사항	RMR 등급	NGI 등급	RQD (%)	N_{ms}				
					A	B	C	D	E
우수	절리간격 3m이상의 신선암	100	500	95~100	3.8	4.3	5.0	5.2	6.1
매우 양호	절리간격 0.9~3m이며, 절리면이 거칠며 치밀하게 밀착되어 있고 풍화되어 있	85	100	90~95	1.4	1.6	1.9	2	2.3
양호	절리간격 0.9~3.0m이며, 절리면이 약간 교란되고 풍화된 신선암	65	10	75~90	0.28	0.32	0.38	0.4	0.46
보통	절리간격 0.9~3.0m의 여러 세트의 적당히 풍화된 절리를 가진 암석	44	1	50~75	0.049	0.056	0.066	0.069	0.081
불량	절리간격이 2~50cm의 약간의 충전물이 있으며 풍화된 절리를 가진 암석	23	0.1	25~50	0.015	0.016	0.019	0.02	0.024
매우 불량	5cm보다 작은 간격의 수없이 많은 풍화된 절리를 가진 암석	3	0.01	<25	상응하는 사질토의 극한지지력을 사용				

(주) RMR : Geomechanics Rock Mass Rating System - Bieniawski(1989)

NGI : Norwegian Geotechnical Institute Rock Mass Classification System, Barton(1974)

RQD : Rock Quality Designation

Nms : 암석의 종류에 따라 정해지는 값으로, 다음표에 따른다(해설표5.6.5)

• 해설 표 5.6.5 암석의 종류에 따른 일축압축강도의 대표적인 범위

암석분류	일 반 사 항	암 석 명	$C_0(\text{kg/cm}^2)$	
A	잘발달된 결정질 벽개를 가진 탄산염암	돌로마이트	336	~ 3,150
		석회암	245	~ 2,940
		대리석	385	~ 2,450
B	점토질암	규질점토암	294	~ 1,470
		점토암	14	~ 84
		이회암	532	~ 1,960
		천매암	245	~ 2,450
		미사암	98	~ 1,190
		세일	70	~ 357
		점판암	1,470	~ 2,100
C	강한결정과 약한 벽개를 가진 사질 암석	역암	336	~ 2,240
		사암	679	~ 1,750
		규암	630	~ 3,850
D	세립질의 화성암 결정질 암석	안산암	980	~ 1,820
		휘록암	217	~ 5,810
E	조립질의 화성암과 변성암의 결정질 암	각섬암	1,190	~ 2,800
		반려암	1,260	~ 3,150
		편마암	245	~ 3,150
		화강암	147	~ 3,430
		석영섬록암	98	~ 980
		편암	98	~ 1,470
		섬장암	1,820	~ 4,340

• 허용지지력 산정

위 치	공번	TCR/RQD (%)	일축압축강도 (kg/cm^2)	N_{ms}	적용여부	q_u (tf/m^2)	q_a (tf/m^2)
터널부	CB-7	50 / 0	2,090	0.016	NG	-	-

5. 확대기초의 지지력 경험치(NAVFAC DM7, 1982)에 의한 방법 - 구조물기초 설계기준(1997)

지 지 층	현장연경도 상태	허용지지력(tf/m ²)		
		범 위	추천값	
괴상의 결정질 화강암, 변성암 : 화강암, 섬록암, 현무암, 완전히 고결된 역암	경질의 신선한 암	650 ~ 1070	860	
엽리성 변성암 : 슬레이트, 편암	중간 경질의 신선한 암	320 ~ 430	375	
퇴적암 : 시멘트화된 경질의 셰일, 실트암, 사암, 동공이 없는 석회암	중간 경질의 신선한 암	160 ~ 270	215	
풍화되거나 파쇄된 모암, 이질암(셰일) 이외의 모든암, RQD<25	연암	85 ~ 130	85	
컴팩션 셰일(Compaction shale)이나 신선한 이질암	연암	85 ~ 160	105	
입도분포가 양호한 세립토 모래자갈의 혼합물 : 빙하퇴적물, 하드팬(Hardpan), 점성토 섞인 자갈(GW-GC, GC, SC)	매우조밀함	85 ~ 130	105	
자갈, 자갈-모래 혼합물, 호박돌-자갈 혼합물(GW, GP, SW, SP)	매우조밀함	65 ~ 105	75	
	중간정도 조밀	40 ~ 75	50	
	느슨함	20 ~ 65	30	
입자가 굵거나 중간정도의 모래, 자갈이 약간섞인 모래(SW, SP)	매우조밀함	40 ~ 65	40	
	중간정도 조밀	20 ~ 40	30	
	느슨함	10 ~ 30	15	
가는 모래, 실트질이나 점토질 중간정도 입도나 굵은 모래(SW, SM, SC)	매우조밀함	30 ~ 50	30	
	중간정도 조밀	20 ~ 40	25	
	느슨함	10 ~ 30	15	
균질한 점토, 모래질이나 실트질 점토(CL, CH)	굳음	30 ~ 60	40	
	중간정도 굳음	10 ~ 30	20	
	느슨함	5 ~ 10	5	
실트, 모래질 실트, 점토질 실트, 교호된(varved) 실트-점토-세사층	매우굳음	20 ~ 40	30	
	중간정도 굳음	10 ~ 30	15	
	연함	5 ~ 10	5	

- ※ ① 일반활하중 및 영구 횡하중을 포함한 편심하중에 의한 후팅의 최대 접지압력이 위 표의 공칭 경험값을 초과해서는 않된다.
- ② 바람이나 지진같은 일시적인 하중에 의한 접지압은 공칭 경험값의 1/3을 초과할수 없다.
- ③ 연한 암반이나 토층 지반에서 기초는 인접 최저 지표고로 부터 최소 0.5m는 근입되어야 한다.
- ④ 연한 암반이나 사질토 지반에서는 ③에서 규정한 초소 근입깊이(0.5m)로 부터 근입깊이가 0.3m 증가할때 마다 공칭 경험값의 5%를 할증하여 사용한다.
- ⑤ 경질 또는 중간정도 경질인 암에서는 기초가 암표면에 놓일 경우 표에 제시된 경험값을 사용하고, 근입깊이가 암표면으로부터 0.3m 증가할때마다 공칭 경험값의 10%를 할증한다.

• 허용지지력 산정

위 치	공번	TCR/RQD (%)	일축압축강도 (kg/cm ²)	qa (tf/m ²)
터널부	CB-7	50 / 0	2,090	85

6. 허용지지력의 결정

위 치	공번	TCR/RQD (%)	일축강도 (kg/cm ²)	기초폭 (Bf,mm)	Peck의 방법(tf/m ²)	C.G.S 방법(tf/m ²)	AASHTO 방법(tf/m ²)	NAVFAC의 경험치(tf/m ²)	적용 (tf/m ²)
터널부	CB-7	50 / 0	2,090	30,500	-	-	-	85	85

8) 전산 INPUT DATA

; File D:\SAP2000DATA\만영개확석터널\가설.\$2k
saved 9-18-02 10:36:02 in Ton-m

SYSTEM

DOF=UX,UZ,RY LENGTH=m FORCE=Ton LINES=59

JOINT

1 X=-14.25 Y=0 Z=-5.679
2 X=-14.25 Y=0 Z=-5.026
3 X=-14.25 Y=0 Z=-4.372
4 X=-14.25 Y=0 Z=-3.719
5 X=-14.23 Y=0 Z=-3.293
6 X=-14.166 Y=0 Z=-2.86
7 X=-14.107 Y=0 Z=-2.444
8 X=-13.748 Y=0 Z=-2.165
9 X=-13.294 Y=0 Z=-1.832
10 X=-12.092 Y=0 Z=-1.131
11 X=-10.887 Y=0 Z=-.608
12 X=-9.683 Y=0 Z=-.256
13 X=-8.479 Y=0 Z=-.057
14 X=-7.275 Y=0 Z=0
15 X=-6.071 Y=0 Z=-.057
16 X=-4.867 Y=0 Z=-.256
17 X=-3.663 Y=0 Z=-.608
18 X=-2.458 Y=0 Z=-1.131
19 X=-1.256 Y=0 Z=-1.832
20 X=-.795 Y=0 Z=-2.165
21 X=-.443 Y=0 Z=-2.444
22 X=-.369 Y=0 Z=-2.86
23 X=-.318 Y=0 Z=-3.293
24 X=-.3 Y=0 Z=-3.719
25 X=-.3 Y=0 Z=-4.372
26 X=-.3 Y=0 Z=-5.026
27 X=-.3 Y=0 Z=-5.679
101 X=-14.325 Y=0 Z=-5.679
102 X=-14.325 Y=0 Z=-7.052
201 X=0 Y=0 Z=-5.679
202 X=0 Y=0 Z=-7.475
301 X=14.325 Y=0 Z=-5.679
302 X=14.325 Y=0 Z=-7.938
401 X=-15.25 Y=0 Z=-7.764
402 X=-14.325 Y=0 Z=-7.764
403 X=-13.9 Y=0 Z=-7.777
404 X=-13.017 Y=0 Z=-7.804
405 X=-12.133 Y=0 Z=-7.83
406 X=-11.25 Y=0 Z=-7.857
407 X=-10.367 Y=0 Z=-7.883
408 X=-9.484 Y=0 Z=-7.91
409 X=-8.6 Y=0 Z=-7.936
410 X=-7.717 Y=0 Z=-7.963
411 X=-6.834 Y=0 Z=-7.989
412 X=-5.95 Y=0 Z=-8.016
413 X=-5.067 Y=0 Z=-8.042
414 X=-4.184 Y=0 Z=-8.069
415 X=-3.3 Y=0 Z=-8.098
416 X=-2.417 Y=0 Z=-8.122
417 X=-1.534 Y=0 Z=-8.148
418 X=-.65 Y=0 Z=-8.175
419 X=0 Y=0 Z=-8.194
420 X=.65 Y=0 Z=-8.214
421 X=1.534 Y=0 Z=-8.241
422 X=2.417 Y=0 Z=-8.267
423 X=3.3 Y=0 Z=-8.291
424 X=4.184 Y=0 Z=-8.32
425 X=5.067 Y=0 Z=-8.347
426 X=5.95 Y=0 Z=-8.373
427 X=6.834 Y=0 Z=-8.4
428 X=7.717 Y=0 Z=-8.426
429 X=8.6 Y=0 Z=-8.453
430 X=9.484 Y=0 Z=-8.479
431 X=10.367 Y=0 Z=-8.506
432 X=11.25 Y=0 Z=-8.532
433 X=12.133 Y=0 Z=-8.559
434 X=13.017 Y=0 Z=-8.585
435 X=13.9 Y=0 Z=-8.612
436 X=14.325 Y=0 Z=-8.625
437 X=15.25 Y=0 Z=-8.625

PATTERN

NAME=TEMP
NAME=PRES

SPRING

ADD=401 U3=201064.2
ADD=402 U3=293445
ADD=403 U3=284315.6
ADD=404 U3=384087
ADD=405 U3=384087

ADD=406 U3=383869.6
ADD=407 U3=383869.6
ADD=408 U3=384087
ADD=409 U3=384087
ADD=410 U3=383869.6
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ADD=419 U1=10000 U3=282576.7
ADD=420 U3=333440.5
ADD=421 U3=384087
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ADD=431 U3=383869.6
ADD=432 U3=383869.6
ADD=433 U3=384087
ADD=434 U3=384087
ADD=435 U3=284315.6
ADD=436 U3=293445
ADD=437 U3=201064.2

MATERIAL

NAME=CONC IDES=C M=.2448 W=2.5
T=0 E=2800000 U=.2 A=.00001
NAME=STEEL IDES=S
T=0 E=2E+10 U=.3 A=.0000117 FY=25310.51
NAME=RIGID IDES=C
T=0 E=2464750 U=.3 A=.00001
NAME=CONC1 IDES=C M=.2448 W=2.5
T=0 E=2464750 U=.2 A=.00001

FRAME SECTION

NAME=T1 MAT=CONC SH=R T=.5,1 A=.5
J=2.861003E-02 I=1.041667E-02,4.897667E-02
AS=.4166667,.4166667
NAME=T2 MAT=CONC SH=R T=.542,1 A=.542
J=3.508126E-02 I=1.326834E-02,4.516667E-02
AS=.4516667,.4516667
NAME=T3 MAT=CONC SH=R T=.675,1 A=.675
J=5.967503E-02 I=2.562891E-02,.05625
AS=.5625,.5625
NAME=T4 MAT=CONC SH=R T=.916,1 A=.916
J=.1170223 I=6.404794E-02,7.633334E-02
AS=.7633333,.7633333
NAME=T5 MAT=CONC SH=R T=.68,1 A=.68
J=6.070982E-02 I=2.620267E-02,5.666667E-02
AS=.5666667,.5666667
NAME=T6 MAT=CONC SH=R T=.553,1 A=.553
J=3.688483E-02 I=.0140927,4.608333E-02
AS=.4608333,.4608333
NAME=T7 MAT=CONC SH=R T=.511,1 A=.511
J=3.024029E-02 I=.0111194,4.258334E-02
AS=.4258333,.4258333
NAME=T8 MAT=CONC SH=R T=.5,1 A=.5
J=2.861003E-02 I=1.041667E-02,4.897667E-02
AS=.4166667,.4166667
NAME=FOOT MAT=CONC1 SH=R T=1.4,1 A=1.4
J=.2612221 I=.2286666,.1166667
AS=1.166667,1.166667
NAME=WALL MAT=CONC1 SH=R T=.85,1 A=.85
J=9.985562E-02 I=4.117709E-02,7.083333E-02
AS=.7083334,.7083334
NAME=RIGID MAT=RIGID SH=R T=10,10 A=100
J=1408.333 I=833.5623,833.5623
AS=83.56233,83.56233
NAME=WALL1 MAT=CONC1 SH=R T=1.3,1 A=1.3
J=.2294606 I=.1830833,.1083333
AS=1.083333,1.083333
NAME=VAR1 TYPE=NONPR
SEC=T1,T2 EIVAR=1,1 L=.426
NAME=VAR2 TYPE=NONPR
SEC=T2,T3 EIVAR=1,1 L=.436
NAME=VAR3 TYPE=NONPR
SEC=T3,T4 EIVAR=1,1 L=.422
NAME=VAR4 TYPE=NONPR
SEC=T4,T5 EIVAR=1,1 L=.455
NAME=VAR5 TYPE=NONPR
SEC=T5,T6 EIVAR=1,1 L=.563

NAME=VAR6 TYPE=NONPR
SEC=T6,T7 EIVAR=1,1 L=1.392
NAME=VAR7 TYPE=NONPR
SEC=T7,T8 EIVAR=1,1 L=1.313

FRAME

1 J=1,2 SEC=T1 NSEG=1 ANG=180 IREL=R3
2 J=2,3 SEC=T1 NSEG=1 ANG=180
3 J=3,4 SEC=T1 NSEG=1 ANG=180
4 J=4,5 SEC=VAR1 NSEG=1 ANG=0
5 J=5,6 SEC=VAR2 NSEG=1 ANG=0
6 J=6,7 SEC=VAR3 NSEG=1 ANG=0
7 J=7,8 SEC=VAR4 NSEG=1 ANG=0
8 J=8,9 SEC=VAR5 NSEG=1 ANG=0
9 J=9,10 SEC=VAR6 NSEG=1 ANG=0
10 J=10,11 SEC=VAR7 NSEG=1 ANG=0
11 J=11,12 SEC=T8 NSEG=1 ANG=0
12 J=12,13 SEC=T8 NSEG=1 ANG=0
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14 J=14,15 SEC=T8 NSEG=1 ANG=0
15 J=15,16 SEC=T8 NSEG=1 ANG=0
16 J=16,17 SEC=T8 NSEG=1 ANG=0
17 J=17,18 SEC=VAR7 NSEG=1 ANG=0
18 J=18,19 SEC=VAR6 NSEG=1 ANG=0
19 J=19,20 SEC=VAR5 NSEG=1 ANG=0
20 J=20,21 SEC=VAR4 NSEG=1 ANG=0
21 J=21,22 SEC=VAR3 NSEG=1 ANG=0
22 J=22,23 SEC=VAR2 NSEG=1 ANG=0
23 J=23,24 SEC=VAR1 NSEG=1 ANG=0
24 J=24,25 SEC=T1 NSEG=1 ANG=0
25 J=25,26 SEC=T1 NSEG=1 ANG=0
26 J=26,27 SEC=T1 NSEG=1 ANG=0 JREL=R3
86 J=201,27 SEC=RIGID NSEG=1 ANG=0
88 J=1,101 SEC=RIGID NSEG=1 ANG=0
101 J=102,101 SEC=WALL NSEG=1 ANG=180
102 J=402,102 SEC=WALL NSEG=1 ANG=180
IOFF=.02475 RIGID=0
201 J=202,201 SEC=WALL1 NSEG=1 ANG=0
202 J=419,202 SEC=WALL1 NSEG=1 ANG=0
IOFF=.375 RIGID=0
301 J=301,302 SEC=WALL NSEG=1 ANG=0
302 J=302,436 SEC=WALL NSEG=1 ANG=0
JOFF=.4875 RIGID=0
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401 J=402,403 SEC=FOOT NSEG=1 ANG=0
IOFF=.075 RIGID=0
402 J=403,404 SEC=FOOT NSEG=1 ANG=0
403 J=404,405 SEC=FOOT NSEG=1 ANG=0
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416 J=417,418 SEC=FOOT NSEG=1 ANG=0
417 J=418,419 SEC=FOOT NSEG=1 ANG=0
JOFF=.3 RIGID=0
418 J=419,420 SEC=FOOT NSEG=1 ANG=0
IOFF=.3 RIGID=0
419 J=420,421 SEC=FOOT NSEG=1 ANG=0
420 J=421,422 SEC=FOOT NSEG=1 ANG=0
421 J=422,423 SEC=FOOT NSEG=1 ANG=0
422 J=423,424 SEC=FOOT NSEG=1 ANG=0
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432 J=433,434 SEC=FOOT NSEG=1 ANG=0
433 J=434,435 SEC=FOOT NSEG=1 ANG=0
434 J=435,436 SEC=FOOT NSEG=1 ANG=0
JOFF=.075 RIGID=0
435 J=436,437 SEC=FOOT NSEG=1 ANG=0

LOAD

NAME=SW SW=1 CSYS=0

OUTPUT

; No Output Requested

END

; The following data is used for graphics, design
and pushover analysis.
; If changes are made to the analysis data above,
then the following data
; should be checked for consistency.

SAP2000 V7.40 SUPPLEMENTAL DATA

GRID GLOBAL X "1" -15.925
GRID GLOBAL Y "2" 0
GRID GLOBAL Z "3" -9.116
GRID GLOBAL X "4" 0
GRID GLOBAL Z "5" 0
GRID GLOBAL X "6" 15.925
MATERIAL STEEL FY 25310.51
MATERIAL CONC FYREBAR 42184.18 FYSHEAR 28122.79
FC 2812.579 FCSHEAR 2812.579
MATERIAL RIGID FYREBAR 42184.18 FYSHEAR
28122.79 FC 2812.579 FCSHEAR 2812.579
MATERIAL CONC1 FYREBAR 42184.18 FYSHEAR
28122.79 FC 2812.579 FCSHEAR 2812.579
CONCRETESECTION T1 COLUMN COVER .055 REBAR
RR-3-3
CONCRETESECTION T2 COLUMN COVER .0574 REBAR
RR-3-3
CONCRETESECTION T3 COLUMN COVER .0672 REBAR
RR-3-3
CONCRETESECTION T4 COLUMN COVER .0871 REBAR
RR-3-3
CONCRETESECTION T5 COLUMN COVER .0863 REBAR
RR-3-3
CONCRETESECTION T6 COLUMN COVER .0644 REBAR
RR-3-3
CONCRETESECTION T7 COLUMN COVER .0529 REBAR
RR-3-3
CONCRETESECTION T8 COLUMN COVER .05 REBAR
RR-3-3
CONCRETESECTION FOOT COLUMN COVER .14 REBAR
RR-3-3
CONCRETESECTION WALL COLUMN COVER .057 REBAR
RR-3-3
CONCRETESECTION RIGID COLUMN COVER 1 REBAR
RR-3-3
CONCRETESECTION WALL1 COLUMN COVER .14 REBAR
RR-3-3
STATICLOAD SW TYPE DEAD
END SUPPLEMENTAL DATA

; File D:\SAP2000DATA\란영게착식터널\MAT1.\$2k
saved 10-9-02 9:58:52 in Ton-m

SYSTEM

DOF=UX,UZ,RY LENGTH=m FORCE=Ton LINES=59

JOINT

1 X=-14.25 Y=0 Z=-5.679
2 X=-14.25 Y=0 Z=-5.026
3 X=-14.25 Y=0 Z=-4.372
4 X=-14.25 Y=0 Z=-3.719
5 X=-14.23 Y=0 Z=-3.293
6 X=-14.166 Y=0 Z=-2.86
7 X=-14.107 Y=0 Z=-2.444
8 X=-13.748 Y=0 Z=-2.165
9 X=-13.294 Y=0 Z=-1.832
10 X=-12.092 Y=0 Z=-1.131
11 X=-10.887 Y=0 Z=-.608
12 X=-9.683 Y=0 Z=-.256
13 X=-8.479 Y=0 Z=-.057
14 X=-7.275 Y=0 Z=0
15 X=-6.071 Y=0 Z=-.057
16 X=-4.867 Y=0 Z=-.256
17 X=-3.663 Y=0 Z=-.608
18 X=-2.458 Y=0 Z=-1.131
19 X=-1.256 Y=0 Z=-1.832
20 X=-.795 Y=0 Z=-2.165
21 X=-.443 Y=0 Z=-2.444
22 X=-.369 Y=0 Z=-2.86
23 X=-.318 Y=0 Z=-3.293
24 X=-.3 Y=0 Z=-3.719
25 X=-.3 Y=0 Z=-4.372
26 X=-.3 Y=0 Z=-5.026
27 X=-.3 Y=0 Z=-5.679
28 X=.3 Y=0 Z=-5.679
29 X=.3 Y=0 Z=-5.026
30 X=.3 Y=0 Z=-4.372
31 X=.3 Y=0 Z=-3.719
32 X=.318 Y=0 Z=-3.293
33 X=.369 Y=0 Z=-2.86
34 X=.443 Y=0 Z=-2.444
35 X=.795 Y=0 Z=-2.165
36 X=1.256 Y=0 Z=-1.832
37 X=2.458 Y=0 Z=-1.131
38 X=3.663 Y=0 Z=-.608
39 X=4.867 Y=0 Z=-.256
40 X=6.071 Y=0 Z=-.057
41 X=7.275 Y=0 Z=0
42 X=8.479 Y=0 Z=-.057
43 X=9.683 Y=0 Z=-.256
44 X=10.887 Y=0 Z=-.608
45 X=12.092 Y=0 Z=-1.131
46 X=13.294 Y=0 Z=-1.832
47 X=13.748 Y=0 Z=-2.165
48 X=14.107 Y=0 Z=-2.444
49 X=14.166 Y=0 Z=-2.86
50 X=14.23 Y=0 Z=-3.293
51 X=14.25 Y=0 Z=-3.719
52 X=14.25 Y=0 Z=-4.372
53 X=14.25 Y=0 Z=-5.026
54 X=14.25 Y=0 Z=-5.679
101 X=-14.325 Y=0 Z=-5.679
102 X=-14.325 Y=0 Z=-7.052
201 X=0 Y=0 Z=-5.679
202 X=0 Y=0 Z=-7.475
301 X=14.325 Y=0 Z=-5.679
302 X=14.325 Y=0 Z=-7.938
401 X=-15.25 Y=0 Z=-7.764
402 X=-14.325 Y=0 Z=-7.764
403 X=-13.9 Y=0 Z=-7.777
404 X=-13.017 Y=0 Z=-7.804
405 X=-12.133 Y=0 Z=-7.83
406 X=-11.25 Y=0 Z=-7.857
407 X=-10.367 Y=0 Z=-7.883
408 X=-9.484 Y=0 Z=-7.91
409 X=-8.6 Y=0 Z=-7.936
410 X=-7.717 Y=0 Z=-7.963
411 X=-6.834 Y=0 Z=-7.989
412 X=-5.95 Y=0 Z=-8.016
413 X=-5.067 Y=0 Z=-8.042
414 X=-4.184 Y=0 Z=-8.069
415 X=-3.3 Y=0 Z=-8.098
416 X=-2.417 Y=0 Z=-8.122
417 X=-1.534 Y=0 Z=-8.148
418 X=-.65 Y=0 Z=-8.175
419 X=0 Y=0 Z=-8.194
420 X=.65 Y=0 Z=-8.214
421 X=1.534 Y=0 Z=-8.241

422 X=2.417 Y=0 Z=-8.267
423 X=3.3 Y=0 Z=-8.291
424 X=4.184 Y=0 Z=-8.32
425 X=5.067 Y=0 Z=-8.347
426 X=5.95 Y=0 Z=-8.373
427 X=6.834 Y=0 Z=-8.4
428 X=7.717 Y=0 Z=-8.426
429 X=8.6 Y=0 Z=-8.453
430 X=9.484 Y=0 Z=-8.479
431 X=10.367 Y=0 Z=-8.506
432 X=11.25 Y=0 Z=-8.532
433 X=12.133 Y=0 Z=-8.559
434 X=13.017 Y=0 Z=-8.585
435 X=13.9 Y=0 Z=-8.612
436 X=14.325 Y=0 Z=-8.625
437 X=15.25 Y=0 Z=-8.625

PATTERN

NAME=TEMP
NAME=PRES

SPRING

ADD=401 U3=201064.2
ADD=402 U3=293445
ADD=403 U3=284315.6
ADD=404 U3=384087
ADD=405 U3=384087
ADD=406 U3=383869.6
ADD=407 U3=383869.6
ADD=408 U3=384087
ADD=409 U3=384087
ADD=410 U3=383869.6
ADD=411 U3=384087
ADD=412 U3=384087
ADD=413 U3=383869.6
ADD=414 U3=384087
ADD=415 U3=384087
ADD=416 U3=383869.6
ADD=417 U3=384087
ADD=418 U3=333440.5
ADD=419 U1=10000 U3=282576.7
ADD=420 U3=333440.5
ADD=421 U3=384087
ADD=422 U3=383869.6
ADD=423 U3=384087
ADD=424 U3=384087
ADD=425 U3=383869.6
ADD=426 U3=384087
ADD=427 U3=384087
ADD=428 U3=383869.6
ADD=429 U3=384087
ADD=430 U3=384087
ADD=431 U3=383869.6
ADD=432 U3=383869.6
ADD=433 U3=384087
ADD=434 U3=384087
ADD=435 U3=284315.6
ADD=436 U3=293445
ADD=437 U3=201064.2

MATERIAL

NAME=CONC IDES=C M=.2448 W=2.5
T=0 E=2800000 U=.2 A=.00001
NAME=STEEL IDES=S
T=0 E=2E+10 U=.3 A=.0000117 FY=25310.51
NAME=RIGID IDES=C
T=0 E=2464750 U=.3 A=.00001
NAME=CONC1 IDES=C M=.2448 W=2.5
T=0 E=2464750 U=.2 A=.00001

FRAME SECTION

NAME=T1 MAT=CONC SH=R T=.5,1 A=.5
J=2.861003E-02 I=1.041667E-02,4.897667E-02
AS=.4166667,.4166667
NAME=T2 MAT=CONC SH=R T=.542,1 A=.542
J=3.508126E-02 I=1.326834E-02,4.516667E-02
AS=.4516667,.4516667
NAME=T3 MAT=CONC SH=R T=.675,1 A=.675
J=5.967503E-02 I=2.562891E-02,.05625
AS=.5625,.5625
NAME=T4 MAT=CONC SH=R T=.916,1 A=.916
J=.1170223 I=6.404794E-02,7.633334E-02
AS=.7633333,.7633333
NAME=T5 MAT=CONC SH=R T=.68,1 A=.68
J=6.070982E-02 I=2.620267E-02,5.666667E-02
AS=.5666667,.5666667
NAME=T6 MAT=CONC SH=R T=.553,1 A=.553
J=3.688483E-02 I=.0140927,4.608333E-02
AS=.4608333,.4608333
NAME=T7 MAT=CONC SH=R T=.511,1 A=.511

J=3.024029E-02 I=.0111194,4.258334E-02
AS=.4258333,.4258333
NAME=T8 MAT=CONC SH=R T=.5,1 A=.5
J=2.861003E-02 I=1.041667E-02,4.897667E-02
AS=.4166667,.4166667
NAME=FOOT MAT=CONC1 SH=R T=1.4,1 A=1.4
J=.2612221 I=.2286666,.1166667
AS=1.166667,1.166667
NAME=WALL MAT=CONC1 SH=R T=.85,1 A=.85
J=9.985562E-02 I=4.117709E-02,7.083333E-02
AS=.7083334,.7083334
NAME=RIGID MAT=RIGID SH=R T=10,10 A=100
J=1408.333 I=833.5623,833.5623
AS=83.56233,83.56233
NAME=WALL1 MAT=CONC1 SH=R T=1.3,1 A=1.3
J=.2294606 I=.1830833,.1083333
AS=1.083333,1.083333
NAME=VAR1 TYPE=NONPR
SEC=T1,T2 EIVAR=1,1 L=.426
NAME=VAR2 TYPE=NONPR
SEC=T2,T3 EIVAR=1,1 L=.436
NAME=VAR3 TYPE=NONPR
SEC=T3,T4 EIVAR=1,1 L=.422
NAME=VAR4 TYPE=NONPR
SEC=T4,T5 EIVAR=1,1 L=.455
NAME=VAR5 TYPE=NONPR
SEC=T5,T6 EIVAR=1,1 L=.563
NAME=VAR6 TYPE=NONPR
SEC=T6,T7 EIVAR=1,1 L=1.392
NAME=VAR7 TYPE=NONPR
SEC=T7,T8 EIVAR=1,1 L=1.313

FRAME

1	J=1,2	SEC=T1	NSEG=1	ANG=180	IREL=R3
2	J=2,3	SEC=T1	NSEG=1	ANG=180	
3	J=3,4	SEC=T1	NSEG=1	ANG=180	
4	J=4,5	SEC=VAR1	NSEG=1	ANG=0	
5	J=5,6	SEC=VAR2	NSEG=1	ANG=0	
6	J=6,7	SEC=VAR3	NSEG=1	ANG=0	
7	J=7,8	SEC=VAR4	NSEG=1	ANG=0	
8	J=8,9	SEC=VAR5	NSEG=1	ANG=0	
9	J=9,10	SEC=VAR6	NSEG=1	ANG=0	
10	J=10,11	SEC=VAR7	NSEG=1	ANG=0	
11	J=11,12	SEC=T8	NSEG=1	ANG=0	
12	J=12,13	SEC=T8	NSEG=1	ANG=0	
13	J=13,14	SEC=T8	NSEG=1	ANG=0	
14	J=14,15	SEC=T8	NSEG=1	ANG=0	
15	J=15,16	SEC=T8	NSEG=1	ANG=0	
16	J=16,17	SEC=T8	NSEG=1	ANG=0	
17	J=17,18	SEC=VAR7	NSEG=1	ANG=0	
18	J=18,19	SEC=VAR6	NSEG=1	ANG=0	
19	J=19,20	SEC=VAR5	NSEG=1	ANG=0	
20	J=20,21	SEC=VAR4	NSEG=1	ANG=0	
21	J=21,22	SEC=VAR3	NSEG=1	ANG=0	
22	J=22,23	SEC=VAR2	NSEG=1	ANG=0	
23	J=23,24	SEC=VAR1	NSEG=1	ANG=0	
24	J=24,25	SEC=T1	NSEG=1	ANG=0	
25	J=25,26	SEC=T1	NSEG=1	ANG=0	
26	J=26,27	SEC=T1	NSEG=1	ANG=0	JREL=R3
27	J=28,29	SEC=T1	NSEG=1	ANG=180	IREL=R3
28	J=29,30	SEC=T1	NSEG=1	ANG=180	
29	J=30,31	SEC=T1	NSEG=1	ANG=180	
30	J=31,32	SEC=VAR1	NSEG=1	ANG=0	
31	J=32,33	SEC=VAR2	NSEG=1	ANG=0	
32	J=33,34	SEC=VAR3	NSEG=1	ANG=0	
33	J=34,35	SEC=VAR4	NSEG=1	ANG=0	
34	J=35,36	SEC=VAR5	NSEG=1	ANG=0	
35	J=36,37	SEC=VAR6	NSEG=1	ANG=0	
36	J=37,38	SEC=VAR7	NSEG=1	ANG=0	
37	J=38,39	SEC=T8	NSEG=1	ANG=0	
38	J=39,40	SEC=T8	NSEG=1	ANG=0	
39	J=40,41	SEC=T8	NSEG=1	ANG=0	
40	J=41,42	SEC=T8	NSEG=1	ANG=0	
41	J=42,43	SEC=T8	NSEG=1	ANG=0	
42	J=43,44	SEC=T8	NSEG=1	ANG=0	
43	J=44,45	SEC=VAR7	NSEG=1	ANG=0	
44	J=45,46	SEC=VAR6	NSEG=1	ANG=0	
45	J=46,47	SEC=VAR5	NSEG=1	ANG=0	
46	J=47,48	SEC=VAR4	NSEG=1	ANG=0	
47	J=48,49	SEC=VAR3	NSEG=1	ANG=0	
48	J=49,50	SEC=VAR2	NSEG=1	ANG=0	
49	J=50,51	SEC=VAR1	NSEG=1	ANG=0	
50	J=51,52	SEC=T1	NSEG=1	ANG=0	
52	J=52,53	SEC=T1	NSEG=1	ANG=0	
53	J=53,54	SEC=T1	NSEG=1	ANG=0	JREL=R3
85	J=28,201	SEC=RIGID	NSEG=1	ANG=0	
86	J=201,27	SEC=RIGID	NSEG=1	ANG=0	
87	J=301,54	SEC=RIGID	NSEG=1	ANG=0	
88	J=1,101	SEC=RIGID	NSEG=1	ANG=0	
101	J=102,101	SEC=WALL	NSEG=1	ANG=180	

102	J=402,102	SEC=WALL	NSEG=1	ANG=180
IOFF=.02475	RIGID=0			
201	J=202,201	SEC=WALL1	NSEG=1	ANG=0
202	J=419,202	SEC=WALL1	NSEG=1	ANG=0
IOFF=.375	RIGID=0			
301	J=301,302	SEC=WALL	NSEG=1	ANG=0
302	J=302,436	SEC=WALL	NSEG=1	ANG=0
JOFF=.4875	RIGID=0			
400	J=401,402	SEC=FOOT	NSEG=1	ANG=0
401	J=402,403	SEC=FOOT	NSEG=1	ANG=0
IOFF=.075	RIGID=0			
402	J=403,404	SEC=FOOT	NSEG=1	ANG=0
403	J=404,405	SEC=FOOT	NSEG=1	ANG=0
404	J=405,406	SEC=FOOT	NSEG=1	ANG=0
405	J=406,407	SEC=FOOT	NSEG=1	ANG=0
406	J=407,408	SEC=FOOT	NSEG=1	ANG=0
407	J=408,409	SEC=FOOT	NSEG=1	ANG=0
408	J=409,410	SEC=FOOT	NSEG=1	ANG=0
409	J=410,411	SEC=FOOT	NSEG=1	ANG=0
410	J=411,412	SEC=FOOT	NSEG=1	ANG=0
411	J=412,413	SEC=FOOT	NSEG=1	ANG=0
412	J=413,414	SEC=FOOT	NSEG=1	ANG=0
413	J=414,415	SEC=FOOT	NSEG=1	ANG=0
414	J=415,416	SEC=FOOT	NSEG=1	ANG=0
415	J=416,417	SEC=FOOT	NSEG=1	ANG=0
416	J=417,418	SEC=FOOT	NSEG=1	ANG=0
417	J=418,419	SEC=FOOT	NSEG=1	ANG=0
JOFF=.3	RIGID=0			
418	J=419,420	SEC=FOOT	NSEG=1	ANG=0
IOFF=.3	RIGID=0			
419	J=420,421	SEC=FOOT	NSEG=1	ANG=0
420	J=421,422	SEC=FOOT	NSEG=1	ANG=0
421	J=422,423	SEC=FOOT	NSEG=1	ANG=0
422	J=423,424	SEC=FOOT	NSEG=1	ANG=0
423	J=424,425	SEC=FOOT	NSEG=1	ANG=0
424	J=425,426	SEC=FOOT	NSEG=1	ANG=0
425	J=426,427	SEC=FOOT	NSEG=1	ANG=0
426	J=427,428	SEC=FOOT	NSEG=1	ANG=0
427	J=428,429	SEC=FOOT	NSEG=1	ANG=0
428	J=429,430	SEC=FOOT	NSEG=1	ANG=0
429	J=430,431	SEC=FOOT	NSEG=1	ANG=0
430	J=431,432	SEC=FOOT	NSEG=1	ANG=0
431	J=432,433	SEC=FOOT	NSEG=1	ANG=0
432	J=433,434	SEC=FOOT	NSEG=1	ANG=0
433	J=434,435	SEC=FOOT	NSEG=1	ANG=0
434	J=435,436	SEC=FOOT	NSEG=1	ANG=0
JOFF=.075	RIGID=0			
435	J=436,437	SEC=FOOT	NSEG=1	ANG=0

LOAD

NAME=SW SW=1

NAME=PV

TYPE=DISTRIBUTED SPAN

ADD=5	RD=0,1	UZ=-12.459,-11.602
ADD=6	RD=0,1	UZ=-11.602,-10.778
ADD=7	RD=0,1	UZ=-10.778,-10.226
ADD=8	RD=0,1	UZ=-10.226,-9.566
ADD=9	RD=0,1	UZ=-9.566,-8.179
ADD=10	RD=0,1	UZ=-8.179,-7.143
ADD=11	RD=0,1	UZ=-7.143,-6.446
ADD=12	RD=0,1	UZ=-6.446,-6.052
ADD=13	RD=0,1	UZ=-6.052,-5.939
ADD=14	RD=0,1	UZ=-5.939,-6.052
ADD=15	RD=0,1	UZ=-6.052,-6.446
ADD=16	RD=0,1	UZ=-6.446,-7.143
ADD=17	RD=0,1	UZ=-7.143,-8.179
ADD=18	RD=0,1	UZ=-8.179,-9.566
ADD=19	RD=0,1	UZ=-9.566,-10.226
ADD=20	RD=0,1	UZ=-10.226,-10.778
ADD=21	RD=0,1	UZ=-10.778,-11.602
ADD=22	RD=0,1	UZ=-11.602,-12.459
ADD=31	RD=0,1	UZ=-12.459,-11.602
ADD=32	RD=0,1	UZ=-11.602,-10.778
ADD=33	RD=0,1	UZ=-10.778,-10.226
ADD=34	RD=0,1	UZ=-10.226,-9.566
ADD=35	RD=0,1	UZ=-9.566,-8.179
ADD=36	RD=0,1	UZ=-8.179,-7.143
ADD=37	RD=0,1	UZ=-7.143,-6.446
ADD=38	RD=0,1	UZ=-6.446,-6.052
ADD=39	RD=0,1	UZ=-6.052,-5.939
ADD=40	RD=0,1	UZ=-5.939,-6.052
ADD=41	RD=0,1	UZ=-6.052,-6.446
ADD=42	RD=0,1	UZ=-6.446,-7.143
ADD=43	RD=0,1	UZ=-7.143,-8.179
ADD=44	RD=0,1	UZ=-8.179,-9.566
ADD=45	RD=0,1	UZ=-9.566,-10.226
ADD=46	RD=0,1	UZ=-10.226,-10.778
ADD=47	RD=0,1	UZ=-10.778,-11.602
ADD=48	RD=0,1	UZ=-11.602,-12.459

NAME=PH

TYPE=DISTRIBUTED SPAN

ADD=102 RD=0,1 UX=10.463,9.787
ADD=101 RD=0,1 UX=9.787,8.483
ADD=1 RD=0,1 UX=8.483,7.862
ADD=2 RD=0,1 UX=7.862,7.241
ADD=3 RD=0,1 UX=7.241,6.621
ADD=4 RD=0,1 UX=6.621,6.216
ADD=5 RD=0,1 UX=6.216,5.805
ADD=6 RD=0,1 UX=5.805,5.409
ADD=7 RD=0,1 UX=5.409,5.144
ADD=8 RD=0,1 UX=5.144,4.828
ADD=9 RD=0,1 UX=4.828,4.162
ADD=10 RD=0,1 UX=4.162,3.665
ADD=11 RD=0,1 UX=3.665,3.331
ADD=12 RD=0,1 UX=3.331,3.142
ADD=13 RD=0,1 UX=3.142,3.088
ADD=14 RD=0,1 UX=-3.088,-3.142
ADD=15 RD=0,1 UX=-3.142,-3.331
ADD=16 RD=0,1 UX=-3.331,-3.665
ADD=17 RD=0,1 UX=-3.665,-4.162
ADD=18 RD=0,1 UX=-4.162,-4.828
ADD=19 RD=0,1 UX=-4.828,-5.144
ADD=20 RD=0,1 UX=-5.144,-5.409
ADD=21 RD=0,1 UX=-5.409,-5.805
ADD=22 RD=0,1 UX=-5.805,-6.216
ADD=23 RD=0,1 UX=-6.216,-6.621
ADD=24 RD=0,1 UX=-6.621,-7.241
ADD=25 RD=0,1 UX=-7.241,-7.862
ADD=26 RD=0,1 UX=-7.862,-8.483
ADD=27 RD=0,1 UX=8.483,7.862
ADD=28 RD=0,1 UX=7.862,7.241
ADD=29 RD=0,1 UX=7.241,6.621
ADD=30 RD=0,1 UX=6.621,6.216
ADD=31 RD=0,1 UX=6.216,5.805
ADD=32 RD=0,1 UX=5.805,5.409
ADD=33 RD=0,1 UX=5.409,5.144
ADD=34 RD=0,1 UX=5.144,4.828
ADD=35 RD=0,1 UX=4.828,4.162
ADD=36 RD=0,1 UX=4.162,3.665
ADD=37 RD=0,1 UX=3.665,3.331
ADD=38 RD=0,1 UX=3.331,3.142
ADD=39 RD=0,1 UX=3.142,3.088
ADD=40 RD=0,1 UX=-3.088,-3.142
ADD=41 RD=0,1 UX=-3.142,-3.331
ADD=42 RD=0,1 UX=-3.331,-3.665
ADD=43 RD=0,1 UX=-3.665,-4.162
ADD=44 RD=0,1 UX=-4.162,-4.828
ADD=45 RD=0,1 UX=-4.828,-5.144
ADD=46 RD=0,1 UX=-5.144,-5.409
ADD=47 RD=0,1 UX=-5.409,-5.805
ADD=48 RD=0,1 UX=-5.805,-6.216
ADD=49 RD=0,1 UX=-6.216,-6.621
ADD=50 RD=0,1 UX=-6.621,-7.241
ADD=52 RD=0,1 UX=-7.241,-7.862
ADD=53 RD=0,1 UX=-7.862,-8.483
ADD=301 RD=0,1 UX=-8.483,-10.629
ADD=302 RD=0,1 UX=-10.629,-11.281

NAME=PVW

TYPE=DISTRIBUTED SPAN

ADD=5 RD=0,1 UZ=-7.986,-7.58
ADD=6 RD=0,1 UZ=-7.58,-7.189
ADD=7 RD=0,1 UZ=-7.189,-6.928
ADD=8 RD=0,1 UZ=-6.928,-6.615
ADD=9 RD=0,1 UZ=-6.615,-5.958
ADD=10 RD=0,1 UZ=-5.958,-5.468
ADD=11 RD=0,1 UZ=-5.468,-5.137
ADD=12 RD=0,1 UZ=-5.137,-4.951
ADD=13 RD=0,1 UZ=-4.951,-4.897
ADD=14 RD=0,1 UZ=-4.897,-4.951
ADD=15 RD=0,1 UZ=-4.951,-5.137
ADD=16 RD=0,1 UZ=-5.137,-5.468
ADD=17 RD=0,1 UZ=-5.468,-5.958
ADD=18 RD=0,1 UZ=-5.958,-6.615
ADD=19 RD=0,1 UZ=-6.615,-6.928
ADD=20 RD=0,1 UZ=-6.928,-7.189
ADD=21 RD=0,1 UZ=-7.189,-7.58
ADD=22 RD=0,1 UZ=-7.58,-7.986
ADD=30 RD=0,1 UZ=-7.986,-7.58
ADD=31 RD=0,1 UZ=-7.58,-7.189
ADD=33 RD=0,1 UZ=-7.189,-6.928
ADD=34 RD=0,1 UZ=-6.928,-6.615
ADD=35 RD=0,1 UZ=-6.615,-5.958
ADD=36 RD=0,1 UZ=-5.958,-5.468
ADD=37 RD=0,1 UZ=-5.468,-5.137
ADD=38 RD=0,1 UZ=-5.137,-4.951
ADD=39 RD=0,1 UZ=-4.951,-4.897
ADD=40 RD=0,1 UZ=-4.897,-4.951
ADD=41 RD=0,1 UZ=-4.951,-5.137
ADD=42 RD=0,1 UZ=-5.137,-5.468
ADD=43 RD=0,1 UZ=-5.468,-5.958

ADD=44 RD=0,1 UZ=-5.958,-6.615
ADD=45 RD=0,1 UZ=-6.615,-6.928
ADD=46 RD=0,1 UZ=-6.928,-7.189
ADD=47 RD=0,1 UZ=-7.189,-7.58
ADD=48 RD=0,1 UZ=-7.58,-7.986

NAME=PHW

TYPE=DISTRIBUTED SPAN

ADD=1 RD=0,1 UX=5.018,4.724
ADD=2 RD=0,1 UX=4.724,4.43
ADD=3 RD=0,1 UX=4.43,4.136
ADD=4 RD=0,1 UX=4.136,3.944
ADD=5 RD=0,1 UX=3.944,3.75
ADD=6 RD=0,1 UX=3.75,3.562
ADD=7 RD=0,1 UX=3.562,3.437
ADD=8 RD=0,1 UX=3.437,3.287
ADD=9 RD=0,1 UX=3.287,2.971
ADD=10 RD=0,1 UX=2.971,2.736
ADD=11 RD=0,1 UX=2.736,2.578
ADD=12 RD=0,1 UX=2.578,2.488
ADD=13 RD=0,1 UX=2.488,2.463
ADD=14 RD=0,1 UX=-2.463,-2.488
ADD=15 RD=0,1 UX=-2.488,-2.578
ADD=16 RD=0,1 UX=-2.578,-2.736
ADD=17 RD=0,1 UX=-2.736,-2.971
ADD=18 RD=0,1 UX=-2.971,-3.287
ADD=19 RD=0,1 UX=-3.287,-3.437
ADD=20 RD=0,1 UX=-3.437,-3.562
ADD=21 RD=0,1 UX=-5.409,-5.805
ADD=22 RD=0,1 UX=-5.805,-6.216
ADD=23 RD=0,1 UX=-6.216,-6.621
ADD=24 RD=0,1 UX=-6.621,-7.241
ADD=25 RD=0,1 UX=-7.241,-7.862
ADD=26 RD=0,1 UX=-7.862,-8.483
ADD=27 RD=0,1 UX=8.483,7.862
ADD=28 RD=0,1 UX=7.862,7.241
ADD=29 RD=0,1 UX=7.241,6.621
ADD=30 RD=0,1 UX=6.621,6.216
ADD=31 RD=0,1 UX=6.216,5.805
ADD=32 RD=0,1 UX=5.805,5.409
ADD=33 RD=0,1 UX=3.562,3.437
ADD=34 RD=0,1 UX=3.437,3.287
ADD=35 RD=0,1 UX=3.287,2.971
ADD=36 RD=0,1 UX=2.971,2.736
ADD=37 RD=0,1 UX=2.736,2.578
ADD=38 RD=0,1 UX=2.578,2.488
ADD=39 RD=0,1 UX=2.488,2.463
ADD=40 RD=0,1 UX=-2.463,-2.488
ADD=41 RD=0,1 UX=-2.488,-2.578
ADD=42 RD=0,1 UX=-2.578,-2.736
ADD=43 RD=0,1 UX=-2.736,-2.971
ADD=44 RD=0,1 UX=-2.971,-3.287
ADD=45 RD=0,1 UX=-3.287,-3.437
ADD=46 RD=0,1 UX=-3.437,-3.562
ADD=47 RD=0,1 UX=-3.562,-3.75
ADD=48 RD=0,1 UX=-3.75,-3.944
ADD=49 RD=0,1 UX=-3.944,-4.136
ADD=50 RD=0,1 UX=-4.136,-4.43
ADD=52 RD=0,1 UX=-4.43,-4.724
ADD=53 RD=0,1 UX=-4.724,-5.018
ADD=102 RD=0,1 UX=5.956,5.636
ADD=302 RD=0,1 UX=-6.035,-6.344
ADD=101 RD=0,1 UX=5.636,5.018
ADD=301 RD=0,1 UX=-5.018,-6.035

NAME=PW

TYPE=DISTRIBUTED SPAN

ADD=1 RD=0,1 U2=-6.929,-6.276
ADD=2 RD=0,1 U2=-6.276,-5.622
ADD=3 RD=0,1 U2=-5.622,-4.969
ADD=4 RD=0,1 U2=-4.969,-4.543
ADD=5 RD=0,1 U2=-4.543,-4.11
ADD=6 RD=0,1 U2=-4.11,-3.694
ADD=7 RD=0,1 U2=-3.694,-3.415
ADD=8 RD=0,1 U2=-3.415,-3.082
ADD=9 RD=0,1 U2=-3.082,-2.381
ADD=10 RD=0,1 U2=-2.381,-1.858
ADD=11 RD=0,1 U2=-1.858,-1.506
ADD=12 RD=0,1 U2=-1.506,-1.307
ADD=13 RD=0,1 U2=-1.307,-1.25
ADD=14 RD=0,1 U2=-1.25,-1.307
ADD=15 RD=0,1 U2=-1.307,-1.506
ADD=16 RD=0,1 U2=-1.506,-1.858
ADD=17 RD=0,1 U2=-1.858,-2.381
ADD=18 RD=0,1 U2=-2.381,-3.082
ADD=19 RD=0,1 U2=-3.082,-3.415
ADD=20 RD=0,1 U2=-3.415,-3.694
ADD=33 RD=0,1 U2=-3.694,-3.415
ADD=34 RD=0,1 U2=-3.415,-3.082
ADD=35 RD=0,1 U2=-3.082,-2.381
ADD=36 RD=0,1 U2=-2.381,-1.858
ADD=37 RD=0,1 U2=-1.858,-1.506

ADD=38 RD=0,1 UZ=-1.506,-1.307
ADD=39 RD=0,1 UZ=-1.307,-1.25
ADD=40 RD=0,1 UZ=-1.25,-1.307
ADD=41 RD=0,1 UZ=-1.307,-1.506
ADD=42 RD=0,1 UZ=-1.506,-3.5628
ADD=43 RD=0,1 UZ=-3.5628,-2.381
ADD=44 RD=0,1 UZ=-2.381,-3.082
ADD=45 RD=0,1 UZ=-3.082,-3.415
ADD=46 RD=0,1 UZ=-3.415,-3.694
ADD=47 RD=0,1 UZ=-3.694,-4.11
ADD=48 RD=0,1 UZ=-4.11,-4.543
ADD=49 RD=0,1 UZ=-4.543,-4.969
ADD=50 RD=0,1 UZ=-4.969,-5.622
ADD=52 RD=0,1 UZ=-5.622,-6.276
ADD=53 RD=0,1 UZ=-6.276,-6.929
ADD=102 RD=0,1 UZ=-9.014,-8.302
ADD=101 RD=0,1 UZ=-8.302,-6.929
ADD=302 RD=0,1 UZ=-9.188,-9.875
ADD=301 RD=0,1 UZ=-6.929,-9.188
ADD=400 RD=0,1 UZ=9.714,9.714
ADD=401 RD=0,1 UZ=9.714,9.727
ADD=402 RD=0,1 UZ=9.727,9.754
ADD=403 RD=0,1 UZ=9.754,9.78
ADD=404 RD=0,1 UZ=9.78,9.807
ADD=405 RD=0,1 UZ=9.807,9.833
ADD=406 RD=0,1 UZ=9.833,9.86
ADD=407 RD=0,1 UZ=9.86,9.886
ADD=408 RD=0,1 UZ=9.886,9.913
ADD=409 RD=0,1 UZ=9.913,9.939
ADD=410 RD=0,1 UZ=9.939,9.966
ADD=411 RD=0,1 UZ=9.966,9.992
ADD=412 RD=0,1 UZ=9.992,10.019
ADD=413 RD=0,1 UZ=10.019,10.048
ADD=414 RD=0,1 UZ=10.048,10.072
ADD=415 RD=0,1 UZ=10.072,10.098
ADD=416 RD=0,1 UZ=10.098,10.125
ADD=417 RD=0,1 UZ=10.125,10.144
ADD=418 RD=0,1 UZ=10.144,10.164
ADD=419 RD=0,1 UZ=10.164,10.191
ADD=420 RD=0,1 UZ=10.191,10.217
ADD=421 RD=0,1 UZ=10.217,10.241
ADD=422 RD=0,1 UZ=10.241,10.27
ADD=423 RD=0,1 UZ=10.27,10.297
ADD=424 RD=0,1 UZ=10.297,10.323
ADD=425 RD=0,1 UZ=10.323,10.35
ADD=426 RD=0,1 UZ=10.35,10.376
ADD=427 RD=0,1 UZ=10.376,10.403
ADD=428 RD=0,1 UZ=10.403,10.429
ADD=429 RD=0,1 UZ=10.429,10.456
ADD=430 RD=0,1 UZ=10.456,10.482
ADD=431 RD=0,1 UZ=10.482,10.509
ADD=432 RD=0,1 UZ=10.509,10.535
ADD=433 RD=0,1 UZ=10.535,10.562
ADD=434 RD=0,1 UZ=10.562,10.575
ADD=435 RD=0,1 UZ=10.575,10.575

NAME=PL

TYPE=CONCENTRATED SPAN

ADD=415 RD=.755 UZ=-9.6
ADD=413 RD=.717 UZ=-9.6
ADD=412 RD=.415 UZ=-9.6
ADD=410 RD=.321 UZ=-9.6
ADD=408 RD=.962 UZ=-9.6
ADD=406 RD=.925 UZ=-9.6
ADD=420 RD=.245 UZ=-9.6
ADD=422 RD=.283 UZ=-9.6
ADD=423 RD=.642 UZ=-9.6
ADD=425 RD=.679 UZ=-9.6
ADD=427 RD=.038 UZ=-9.6
ADD=429 RD=.076 UZ=-9.6

NAME=PVL

TYPE=DISTRIBUTED SPAN

ADD=5 RD=0,1 UZ=-1.186,-1.186
ADD=6 RD=0,1 UZ=-1.186,-1.186
ADD=7 RD=0,1 UZ=-1.186,-1.186
ADD=8 RD=0,1 UZ=-1.186,-1.186
ADD=9 RD=0,1 UZ=-1.186,-1.186
ADD=10 RD=0,1 UZ=-1.186,-1.186
ADD=11 RD=0,1 UZ=-1.186,-1.186
ADD=12 RD=0,1 UZ=-1.186,-1.186
ADD=13 RD=0,1 UZ=-1.186,-1.186
ADD=14 RD=0,1 UZ=-1.186,-1.186
ADD=15 RD=0,1 UZ=-1.186,-1.186
ADD=16 RD=0,1 UZ=-1.186,-1.186
ADD=17 RD=0,1 UZ=-1.186,-1.186
ADD=18 RD=0,1 UZ=-1.186,-1.186
ADD=19 RD=0,1 UZ=-1.186,-1.186
ADD=20 RD=0,1 UZ=-1.186,-1.186
ADD=21 RD=0,1 UZ=-1.186,-1.186
ADD=22 RD=0,1 UZ=-1.186,-1.186
ADD=31 RD=0,1 UZ=-1.186,-1.186

ADD=32 RD=0,1 UZ=-1.186,-1.186
ADD=33 RD=0,1 UZ=-1.186,-1.186
ADD=34 RD=0,1 UZ=-1.186,-1.186
ADD=35 RD=0,1 UZ=-1.186,-1.186
ADD=36 RD=0,1 UZ=-1.186,-1.186
ADD=37 RD=0,1 UZ=-1.186,-1.186
ADD=38 RD=0,1 UZ=-1.186,-1.186
ADD=39 RD=0,1 UZ=-1.186,-1.186
ADD=40 RD=0,1 UZ=-1.186,-1.186
ADD=41 RD=0,1 UZ=-1.186,-1.186
ADD=42 RD=0,1 UZ=-1.186,-1.186
ADD=43 RD=0,1 UZ=-1.186,-1.186
ADD=44 RD=0,1 UZ=-1.186,-1.186
ADD=45 RD=0,1 UZ=-1.186,-1.186
ADD=46 RD=0,1 UZ=-1.186,-1.186
ADD=47 RD=0,1 UZ=-1.186,-1.186
ADD=48 RD=0,1 UZ=-1.186,-1.186

COMBO

NAME=COMB1

LOAD=SW SF=1.3
LOAD=PV SF=1.5
LOAD=PH SF=1.7

NAME=COMB2

LOAD=SW SF=1.3
LOAD=PV SF=1.5
LOAD=PH SF=.65

NAME=COMB3

LOAD=SW SF=1.3
LOAD=PVW SF=1.5
LOAD=PHW SF=1.7
LOAD=PW SF=1.3

NAME=COMB4

LOAD=SW SF=1.3
LOAD=PVW SF=1.5
LOAD=PHW SF=.65
LOAD=PW SF=1.3

NAME=COMB5

LOAD=SW SF=1.3
LOAD=PV SF=1.5
LOAD=PH SF=1.7
LOAD=PVL SF=1.3

NAME=COMB6

LOAD=SW SF=1.3
LOAD=PV SF=1.5
LOAD=PH SF=.65
LOAD=PVL SF=1.3

NAME=COMB7

LOAD=SW SF=1
LOAD=PV SF=1
LOAD=PH SF=1

NAME=COMB8

LOAD=SW SF=1
LOAD=PV SF=1
LOAD=PH SF=1
LOAD=PL SF=1

NAME=COMB9

LOAD=SW SF=1
LOAD=PV SF=1
LOAD=PH SF=.5

NAME=COMB10

LOAD=SW SF=1
LOAD=PV SF=1
LOAD=PH SF=.5
LOAD=PL SF=1

NAME=COMB11

LOAD=SW SF=1
LOAD=PVW SF=1
LOAD=PHW SF=1

NAME=COMB12

LOAD=SW SF=1
LOAD=PVW SF=1
LOAD=PHW SF=1
LOAD=PL SF=1

NAME=ENVE TYPE=ENVE

COMB=COMB1 SF=1
COMB=COMB2 SF=1
COMB=COMB5 SF=1

OUTPUT

; No Output Requested

END

; The following data is used for graphics, design
and pushover analysis.
; If changes are made to the analysis data above,
then the following data
; should be checked for consistency.
SAP2000 V7.10 SUPPLEMENTAL DATA

```

GRID GLOBAL X "1" -15.25
GRID GLOBAL Y "2" 0
GRID GLOBAL Z "3" -8.625
GRID GLOBAL X "4" 0
GRID GLOBAL Z "5" 0
GRID GLOBAL X "6" 15.25
MATERIAL STEEL FY 25310.51
MATERIAL CONC FYREBAR 40000 FYSHEAR 28122.79 FC
4000 FCSHEAR 2812.279
MATERIAL RIGID FYREBAR 40000 FYSHEAR 28122.79
FC 4000 FCSHEAR 2812.279
MATERIAL CONCL FYREBAR 40000 FYSHEAR 28122.79
FC 4000 FCSHEAR 2812.279
CONCRETESECTION T1 COLUMN COVER .05 REBAR
RR-3-3
CONCRETESECTION T2 COLUMN COVER .0542 REBAR
RR-3-3
CONCRETESECTION T3 COLUMN COVER .0675 REBAR
RR-3-3
CONCRETESECTION T4 COLUMN COVER .0916 REBAR
RR-3-3
CONCRETESECTION T5 COLUMN COVER .068 REBAR
RR-3-3
CONCRETESECTION T6 COLUMN COVER .0553 REBAR
RR-3-3
CONCRETESECTION T7 COLUMN COVER .0511 REBAR
RR-3-3
CONCRETESECTION T8 COLUMN COVER .05 REBAR
RR-3-3
CONCRETESECTION FOOT COLUMN COVER .14 REBAR
RR-3-3
CONCRETESECTION WALL COLUMN COVER .085 REBAR
RR-3-3
CONCRETESECTION RIGID COLUMN COVER 1 REBAR
RR-3-3
CONCRETESECTION WALL1 COLUMN COVER .13 REBAR
RR-3-3
STATICLOAD SW TYPE DEAD
STATICLOAD PV TYPE DEAD
STATICLOAD PH TYPE DEAD
STATICLOAD PVW TYPE DEAD
STATICLOAD PHW TYPE DEAD
STATICLOAD PW TYPE DEAD
STATICLOAD PL TYPE DEAD
STATICLOAD PVL TYPE DEAD
END SUPPLEMENTAL DATA

```

; File D:\SAP2000DATA\만영계착식터널\MAT3.\$2k
saved 10-9-02 9:59:57 in Ton-m

SYSTEM

DOF=UX,UZ,RY LENGTH=m FORCE=Ton LINES=59

JOINT

1 X=-14.25 Y=0 Z=-5.679
2 X=-14.25 Y=0 Z=-5.026
3 X=-14.25 Y=0 Z=-4.372
4 X=-14.25 Y=0 Z=-3.719
5 X=-14.23 Y=0 Z=-3.293
6 X=-14.166 Y=0 Z=-2.86
7 X=-14.107 Y=0 Z=-2.444
8 X=-13.748 Y=0 Z=-2.165
9 X=-13.294 Y=0 Z=-1.832
10 X=-12.092 Y=0 Z=-1.131
11 X=-10.887 Y=0 Z=-.608
12 X=-9.683 Y=0 Z=-.256
13 X=-8.479 Y=0 Z=-.057
14 X=-7.275 Y=0 Z=0
15 X=-6.071 Y=0 Z=-.057
16 X=-4.867 Y=0 Z=-.256
17 X=-3.663 Y=0 Z=-.608
18 X=-2.458 Y=0 Z=-1.131
19 X=-1.256 Y=0 Z=-1.832
20 X=-.795 Y=0 Z=-2.165
21 X=-.443 Y=0 Z=-2.444
22 X=-.369 Y=0 Z=-2.86
23 X=-.318 Y=0 Z=-3.293
24 X=-.3 Y=0 Z=-3.719
25 X=-.3 Y=0 Z=-4.372
26 X=-.3 Y=0 Z=-5.026
27 X=-.3 Y=0 Z=-5.679
28 X=.3 Y=0 Z=-5.679
29 X=.3 Y=0 Z=-5.026
30 X=.3 Y=0 Z=-4.372
31 X=.3 Y=0 Z=-3.719
32 X=.318 Y=0 Z=-3.293
33 X=.369 Y=0 Z=-2.86
34 X=.443 Y=0 Z=-2.444
35 X=.795 Y=0 Z=-2.165
36 X=1.256 Y=0 Z=-1.832
37 X=2.458 Y=0 Z=-1.131
38 X=3.663 Y=0 Z=-.608
39 X=4.867 Y=0 Z=-.256
40 X=6.071 Y=0 Z=-.057
41 X=7.275 Y=0 Z=0
42 X=8.479 Y=0 Z=-.057
43 X=9.683 Y=0 Z=-.256
44 X=10.887 Y=0 Z=-.608
45 X=12.092 Y=0 Z=-1.131
46 X=13.294 Y=0 Z=-1.832
47 X=13.748 Y=0 Z=-2.165
48 X=14.107 Y=0 Z=-2.444
49 X=14.166 Y=0 Z=-2.86
50 X=14.23 Y=0 Z=-3.293
51 X=14.25 Y=0 Z=-3.719
52 X=14.25 Y=0 Z=-4.372
53 X=14.25 Y=0 Z=-5.026
54 X=14.25 Y=0 Z=-5.679
101 X=-14.325 Y=0 Z=-5.679
102 X=-14.325 Y=0 Z=-7.052
201 X=0 Y=0 Z=-5.679
202 X=0 Y=0 Z=-7.475
301 X=14.325 Y=0 Z=-5.679
302 X=14.325 Y=0 Z=-7.938
401 X=-15.25 Y=0 Z=-7.764
402 X=-14.325 Y=0 Z=-7.764
403 X=-13.9 Y=0 Z=-7.777
404 X=-13.017 Y=0 Z=-7.804
405 X=-12.133 Y=0 Z=-7.83
406 X=-11.25 Y=0 Z=-7.857
407 X=-10.367 Y=0 Z=-7.883
408 X=-9.484 Y=0 Z=-7.91
409 X=-8.6 Y=0 Z=-7.936
410 X=-7.717 Y=0 Z=-7.963
411 X=-6.834 Y=0 Z=-7.989
412 X=-5.95 Y=0 Z=-8.016
413 X=-5.067 Y=0 Z=-8.042
414 X=-4.184 Y=0 Z=-8.069
415 X=-3.3 Y=0 Z=-8.098
416 X=-2.417 Y=0 Z=-8.122
417 X=-1.534 Y=0 Z=-8.148
418 X=-.65 Y=0 Z=-8.175
419 X=0 Y=0 Z=-8.194
420 X=.65 Y=0 Z=-8.214
421 X=1.534 Y=0 Z=-8.241

422 X=2.417 Y=0 Z=-8.267
423 X=3.3 Y=0 Z=-8.291
424 X=4.184 Y=0 Z=-8.32
425 X=5.067 Y=0 Z=-8.347
426 X=5.95 Y=0 Z=-8.373
427 X=6.834 Y=0 Z=-8.4
428 X=7.717 Y=0 Z=-8.426
429 X=8.6 Y=0 Z=-8.453
430 X=9.484 Y=0 Z=-8.479
431 X=10.367 Y=0 Z=-8.506
432 X=11.25 Y=0 Z=-8.532
433 X=12.133 Y=0 Z=-8.559
434 X=13.017 Y=0 Z=-8.585
435 X=13.9 Y=0 Z=-8.612
436 X=14.325 Y=0 Z=-8.625
437 X=15.25 Y=0 Z=-8.625

PATTERN

NAME=TEMP
NAME=PRES

SPRING

ADD=401 U3=201064.2
ADD=402 U3=293445
ADD=418 U3=333440.5
ADD=419 U1=10000 U3=282576.7
ADD=420 U3=333440.5
ADD=436 U3=293445
ADD=437 U3=201064.2

MATERIAL

NAME=CONC IDES=C M=.2448 W=2.5
T=0 E=2800000 U=.2 A=.00001
NAME=STEEL IDES=S
T=0 E=2E+10 U=.3 A=.0000117 FY=25310.51
NAME=RIGID IDES=C
T=0 E=2464750 U=.3 A=.00001
NAME=CONC1 IDES=C M=.2448 W=2.5
T=0 E=2464750 U=.2 A=.00001

FRAME SECTION

NAME=T1 MAT=CONC SH=R T=.5,1 A=.5
J=2.861003E-02 I=1.041667E-02,4.897667E-02
AS=.4166667,.4166667
NAME=T2 MAT=CONC SH=R T=.542,1 A=.542
J=3.508126E-02 I=1.326834E-02,4.516667E-02
AS=.4516667,.4516667
NAME=T3 MAT=CONC SH=R T=.675,1 A=.675
J=5.967503E-02 I=2.562891E-02,.05625
AS=.5625,.5625
NAME=T4 MAT=CONC SH=R T=.916,1 A=.916
J=.1170223 I=6.404794E-02,7.633334E-02
AS=.7633333,.7633333
NAME=T5 MAT=CONC SH=R T=.68,1 A=.68
J=6.070982E-02 I=2.620267E-02,5.666667E-02
AS=.5666667,.5666667
NAME=T6 MAT=CONC SH=R T=.553,1 A=.553
J=3.688483E-02 I=.0140927,4.608333E-02
AS=.4608333,.4608333
NAME=T7 MAT=CONC SH=R T=.511,1 A=.511
J=3.024029E-02 I=.0111194,4.258334E-02
AS=.4258333,.4258333
NAME=T8 MAT=CONC SH=R T=.5,1 A=.5
J=2.861003E-02 I=1.041667E-02,4.897667E-02
AS=.4166667,.4166667
NAME=FOOT MAT=CONC1 SH=R T=1.4,1 A=1.4
J=.2612221 I=.2286666,.1166667
AS=1.166667,1.166667
NAME=WALL MAT=CONC1 SH=R T=.85,1 A=.85
J=9.985562E-02 I=4.117709E-02,7.083333E-02
AS=.7083334,.7083334
NAME=RIGID MAT=RIGID SH=R T=10,10 A=100
J=1408.333 I=833.5623,833.5623
AS=83.56233,83.56233
NAME=WALL1 MAT=CONC1 SH=R T=1.3,1 A=1.3
J=.2294606 I=.1830833,.1083333
AS=1.083333,1.083333
NAME=VAR1 TYPE=NONPR
SEC=T1,T2 EIVAR=1,1 L=.426
NAME=VAR2 TYPE=NONPR
SEC=T2,T3 EIVAR=1,1 L=.436
NAME=VAR3 TYPE=NONPR
SEC=T3,T4 EIVAR=1,1 L=.422
NAME=VAR4 TYPE=NONPR
SEC=T4,T5 EIVAR=1,1 L=.455
NAME=VAR5 TYPE=NONPR
SEC=T5,T6 EIVAR=1,1 L=.563
NAME=VAR6 TYPE=NONPR
SEC=T6,T7 EIVAR=1,1 L=1.392
NAME=VAR7 TYPE=NONPR

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SEC=T7,T8 EIVAR=1,1 L=1.313

FRAME
1 J=1,2 SEC=T1 NSEG=1 ANG=180 IREL=R3
2 J=2,3 SEC=T1 NSEG=1 ANG=180
3 J=3,4 SEC=T1 NSEG=1 ANG=180
4 J=4,5 SEC=VAR1 NSEG=1 ANG=0
5 J=5,6 SEC=VAR2 NSEG=1 ANG=0
6 J=6,7 SEC=VAR3 NSEG=1 ANG=0
7 J=7,8 SEC=VAR4 NSEG=1 ANG=0
8 J=8,9 SEC=VAR5 NSEG=1 ANG=0
9 J=9,10 SEC=VAR6 NSEG=1 ANG=0
10 J=10,11 SEC=VAR7 NSEG=1 ANG=0
11 J=11,12 SEC=T8 NSEG=1 ANG=0
12 J=12,13 SEC=T8 NSEG=1 ANG=0
13 J=13,14 SEC=T8 NSEG=1 ANG=0
14 J=14,15 SEC=T8 NSEG=1 ANG=0
15 J=15,16 SEC=T8 NSEG=1 ANG=0
16 J=16,17 SEC=T8 NSEG=1 ANG=0
17 J=17,18 SEC=VAR7 NSEG=1 ANG=0
18 J=18,19 SEC=VAR6 NSEG=1 ANG=0
19 J=19,20 SEC=VAR5 NSEG=1 ANG=0
20 J=20,21 SEC=VAR4 NSEG=1 ANG=0
21 J=21,22 SEC=VAR3 NSEG=1 ANG=0
22 J=22,23 SEC=VAR2 NSEG=1 ANG=0
23 J=23,24 SEC=VAR1 NSEG=1 ANG=0
24 J=24,25 SEC=T1 NSEG=1 ANG=0
25 J=25,26 SEC=T1 NSEG=1 ANG=0
26 J=26,27 SEC=T1 NSEG=1 ANG=0 JREL=R3
27 J=28,29 SEC=T1 NSEG=1 ANG=180 IREL=R3
28 J=29,30 SEC=T1 NSEG=1 ANG=180
29 J=30,31 SEC=T1 NSEG=1 ANG=180
30 J=31,32 SEC=VAR1 NSEG=1 ANG=0
31 J=32,33 SEC=VAR2 NSEG=1 ANG=0
32 J=33,34 SEC=VAR3 NSEG=1 ANG=0
33 J=34,35 SEC=VAR4 NSEG=1 ANG=0
34 J=35,36 SEC=VAR5 NSEG=1 ANG=0
35 J=36,37 SEC=VAR6 NSEG=1 ANG=0
36 J=37,38 SEC=VAR7 NSEG=1 ANG=0
37 J=38,39 SEC=T8 NSEG=1 ANG=0
38 J=39,40 SEC=T8 NSEG=1 ANG=0
39 J=40,41 SEC=T8 NSEG=1 ANG=0
40 J=41,42 SEC=T8 NSEG=1 ANG=0
41 J=42,43 SEC=T8 NSEG=1 ANG=0
42 J=43,44 SEC=T8 NSEG=1 ANG=0
43 J=44,45 SEC=VAR7 NSEG=1 ANG=0
44 J=45,46 SEC=VAR6 NSEG=1 ANG=0
45 J=46,47 SEC=VAR5 NSEG=1 ANG=0
46 J=47,48 SEC=VAR4 NSEG=1 ANG=0
47 J=48,49 SEC=VAR3 NSEG=1 ANG=0
48 J=49,50 SEC=VAR2 NSEG=1 ANG=0
49 J=50,51 SEC=VAR1 NSEG=1 ANG=0
50 J=51,52 SEC=T1 NSEG=1 ANG=0
52 J=52,53 SEC=T1 NSEG=1 ANG=0
53 J=53,54 SEC=T1 NSEG=1 ANG=0 JREL=R3
85 J=28,201 SEC=RIGID NSEG=1 ANG=0
86 J=201,27 SEC=RIGID NSEG=1 ANG=0
87 J=301,54 SEC=RIGID NSEG=1 ANG=0
88 J=1,101 SEC=RIGID NSEG=1 ANG=0
101 J=102,101 SEC=WALL NSEG=1 ANG=180
102 J=402,102 SEC=WALL NSEG=1 ANG=180
IOFF=.02475 RIGID=0
201 J=202,201 SEC=WALL1 NSEG=1 ANG=0
202 J=419,202 SEC=WALL1 NSEG=1 ANG=0
IOFF=.375 RIGID=0
301 J=301,302 SEC=WALL NSEG=1 ANG=0
302 J=302,436 SEC=WALL NSEG=1 ANG=0
JOFF=.4875 RIGID=0
400 J=401,402 SEC=FOOT NSEG=1 ANG=0
401 J=402,403 SEC=FOOT NSEG=1 ANG=0
IOFF=.075 RIGID=0
402 J=403,404 SEC=FOOT NSEG=1 ANG=0
403 J=404,405 SEC=FOOT NSEG=1 ANG=0
404 J=405,406 SEC=FOOT NSEG=1 ANG=0
405 J=406,407 SEC=FOOT NSEG=1 ANG=0
406 J=407,408 SEC=FOOT NSEG=1 ANG=0
407 J=408,409 SEC=FOOT NSEG=1 ANG=0
408 J=409,410 SEC=FOOT NSEG=1 ANG=0
409 J=410,411 SEC=FOOT NSEG=1 ANG=0
410 J=411,412 SEC=FOOT NSEG=1 ANG=0
411 J=412,413 SEC=FOOT NSEG=1 ANG=0
412 J=413,414 SEC=FOOT NSEG=1 ANG=0
413 J=414,415 SEC=FOOT NSEG=1 ANG=0
414 J=415,416 SEC=FOOT NSEG=1 ANG=0
415 J=416,417 SEC=FOOT NSEG=1 ANG=0
416 J=417,418 SEC=FOOT NSEG=1 ANG=0
417 J=418,419 SEC=FOOT NSEG=1 ANG=0
JOFF=.3 RIGID=0
418 J=419,420 SEC=FOOT NSEG=1 ANG=0
IOFF=.3 RIGID=0

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419 J=420,421 SEC=FOOT NSEG=1 ANG=0
420 J=421,422 SEC=FOOT NSEG=1 ANG=0
421 J=422,423 SEC=FOOT NSEG=1 ANG=0
422 J=423,424 SEC=FOOT NSEG=1 ANG=0
423 J=424,425 SEC=FOOT NSEG=1 ANG=0
424 J=425,426 SEC=FOOT NSEG=1 ANG=0
425 J=426,427 SEC=FOOT NSEG=1 ANG=0
426 J=427,428 SEC=FOOT NSEG=1 ANG=0
427 J=428,429 SEC=FOOT NSEG=1 ANG=0
428 J=429,430 SEC=FOOT NSEG=1 ANG=0
429 J=430,431 SEC=FOOT NSEG=1 ANG=0
430 J=431,432 SEC=FOOT NSEG=1 ANG=0
431 J=432,433 SEC=FOOT NSEG=1 ANG=0
432 J=433,434 SEC=FOOT NSEG=1 ANG=0
433 J=434,435 SEC=FOOT NSEG=1 ANG=0
434 J=435,436 SEC=FOOT NSEG=1 ANG=0
JOFF=.075 RIGID=0
435 J=436,437 SEC=FOOT NSEG=1 ANG=0

LOAD
NAME=SW SW=1
NAME=PV
TYPE=DISTRIBUTED SPAN
ADD=5 RD=0,1 UZ=-12.459,-11.602
ADD=6 RD=0,1 UZ=-11.602,-10.778
ADD=7 RD=0,1 UZ=-10.778,-10.226
ADD=8 RD=0,1 UZ=-10.226,-9.566
ADD=9 RD=0,1 UZ=-9.566,-8.179
ADD=10 RD=0,1 UZ=-8.179,-7.143
ADD=11 RD=0,1 UZ=-7.143,-6.446
ADD=12 RD=0,1 UZ=-6.446,-6.052
ADD=13 RD=0,1 UZ=-6.052,-5.939
ADD=14 RD=0,1 UZ=-5.939,-6.052
ADD=15 RD=0,1 UZ=-6.052,-6.446
ADD=16 RD=0,1 UZ=-6.446,-7.143
ADD=17 RD=0,1 UZ=-7.143,-8.179
ADD=18 RD=0,1 UZ=-8.179,-9.566
ADD=19 RD=0,1 UZ=-9.566,-10.226
ADD=20 RD=0,1 UZ=-10.226,-10.778
ADD=21 RD=0,1 UZ=-10.778,-11.602
ADD=22 RD=0,1 UZ=-11.602,-12.459
ADD=31 RD=0,1 UZ=-12.459,-11.602
ADD=32 RD=0,1 UZ=-11.602,-10.778
ADD=33 RD=0,1 UZ=-10.778,-10.226
ADD=34 RD=0,1 UZ=-10.226,-9.566
ADD=35 RD=0,1 UZ=-9.566,-8.179
ADD=36 RD=0,1 UZ=-8.179,-7.143
ADD=37 RD=0,1 UZ=-7.143,-6.446
ADD=38 RD=0,1 UZ=-6.446,-6.052
ADD=39 RD=0,1 UZ=-6.052,-5.939
ADD=40 RD=0,1 UZ=-5.939,-6.052
ADD=41 RD=0,1 UZ=-6.052,-6.446
ADD=42 RD=0,1 UZ=-6.446,-7.143
ADD=43 RD=0,1 UZ=-7.143,-8.179
ADD=44 RD=0,1 UZ=-8.179,-9.566
ADD=45 RD=0,1 UZ=-9.566,-10.226
ADD=46 RD=0,1 UZ=-10.226,-10.778
ADD=47 RD=0,1 UZ=-10.778,-11.602
ADD=48 RD=0,1 UZ=-11.602,-12.459
NAME=PH
TYPE=DISTRIBUTED SPAN
ADD=102 RD=0,1 UX=10.463,9.787
ADD=101 RD=0,1 UX=9.787,8.483
ADD=1 RD=0,1 UX=8.483,7.862
ADD=2 RD=0,1 UX=7.862,7.241
ADD=3 RD=0,1 UX=7.241,6.621
ADD=4 RD=0,1 UX=6.621,6.216
ADD=5 RD=0,1 UX=6.216,5.805
ADD=6 RD=0,1 UX=5.805,5.409
ADD=7 RD=0,1 UX=5.409,5.144
ADD=8 RD=0,1 UX=5.144,4.828
ADD=9 RD=0,1 UX=4.828,4.162
ADD=10 RD=0,1 UX=4.162,3.665
ADD=11 RD=0,1 UX=3.665,3.331
ADD=12 RD=0,1 UX=3.331,3.142
ADD=13 RD=0,1 UX=3.142,3.088
ADD=14 RD=0,1 UX=-3.088,-3.142
ADD=15 RD=0,1 UX=-3.142,-3.331
ADD=16 RD=0,1 UX=-3.331,-3.665
ADD=17 RD=0,1 UX=-3.665,-4.162
ADD=18 RD=0,1 UX=-4.162,-4.828
ADD=19 RD=0,1 UX=-4.828,-5.144
ADD=20 RD=0,1 UX=-5.144,-5.409
ADD=21 RD=0,1 UX=-5.409,-5.805
ADD=22 RD=0,1 UX=-5.805,-6.216
ADD=23 RD=0,1 UX=-6.216,-6.621
ADD=24 RD=0,1 UX=-6.621,-7.241
ADD=25 RD=0,1 UX=-7.241,-7.862
ADD=26 RD=0,1 UX=-7.862,-8.483
ADD=27 RD=0,1 UX=-8.483,-9.787

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ADD=28 RD=0,1 UX=7.862,7.241
ADD=29 RD=0,1 UX=7.241,6.621
ADD=30 RD=0,1 UX=6.621,6.216
ADD=31 RD=0,1 UX=6.216,5.805
ADD=32 RD=0,1 UX=5.805,5.409
ADD=33 RD=0,1 UX=5.409,5.144
ADD=34 RD=0,1 UX=5.144,4.828
ADD=35 RD=0,1 UX=4.828,4.162
ADD=36 RD=0,1 UX=4.162,3.665
ADD=37 RD=0,1 UX=3.665,3.331
ADD=38 RD=0,1 UX=3.331,3.142
ADD=39 RD=0,1 UX=3.142,3.088
ADD=40 RD=0,1 UX=-3.088,-3.142
ADD=41 RD=0,1 UX=-3.142,-3.331
ADD=42 RD=0,1 UX=-3.331,-3.665
ADD=43 RD=0,1 UX=-3.665,-4.162
ADD=44 RD=0,1 UX=-4.162,-4.828
ADD=45 RD=0,1 UX=-4.828,-5.144
ADD=46 RD=0,1 UX=-5.144,-5.409
ADD=47 RD=0,1 UX=-5.409,-5.805
ADD=48 RD=0,1 UX=-5.805,-6.216
ADD=49 RD=0,1 UX=-6.216,-6.621
ADD=50 RD=0,1 UX=-6.621,-7.241
ADD=52 RD=0,1 UX=-7.241,-7.862
ADD=53 RD=0,1 UX=-7.862,-8.483
ADD=301 RD=0,1 UX=-8.483,-10.629
ADD=302 RD=0,1 UX=-10.629,-11.281

NAME=PVW

TYPE=DISTRIBUTED SPAN

ADD=5 RD=0,1 UZ=-7.986,-7.58
ADD=6 RD=0,1 UZ=-7.58,-7.189
ADD=7 RD=0,1 UZ=-7.189,-6.928
ADD=8 RD=0,1 UZ=-6.928,-6.615
ADD=9 RD=0,1 UZ=-6.615,-5.958
ADD=10 RD=0,1 UZ=-5.958,-5.468
ADD=11 RD=0,1 UZ=-5.468,-5.137
ADD=12 RD=0,1 UZ=-5.137,-4.951
ADD=13 RD=0,1 UZ=-4.951,-4.897
ADD=14 RD=0,1 UZ=-4.897,-4.951
ADD=15 RD=0,1 UZ=-4.951,-5.137
ADD=16 RD=0,1 UZ=-5.137,-5.468
ADD=17 RD=0,1 UZ=-5.468,-5.958
ADD=18 RD=0,1 UZ=-5.958,-6.615
ADD=19 RD=0,1 UZ=-6.615,-6.928
ADD=20 RD=0,1 UZ=-6.928,-7.189
ADD=21 RD=0,1 UZ=-7.189,-7.58
ADD=22 RD=0,1 UZ=-7.58,-7.986
ADD=30 RD=0,1 UZ=-7.986,-7.58
ADD=31 RD=0,1 UZ=-7.58,-7.189
ADD=33 RD=0,1 UZ=-7.189,-6.928
ADD=34 RD=0,1 UZ=-6.928,-6.615
ADD=35 RD=0,1 UZ=-6.615,-5.958
ADD=36 RD=0,1 UZ=-5.958,-5.468
ADD=37 RD=0,1 UZ=-5.468,-5.137
ADD=38 RD=0,1 UZ=-5.137,-4.951
ADD=39 RD=0,1 UZ=-4.951,-4.897
ADD=40 RD=0,1 UZ=-4.897,-4.951
ADD=41 RD=0,1 UZ=-4.951,-5.137
ADD=42 RD=0,1 UZ=-5.137,-5.468
ADD=43 RD=0,1 UZ=-5.468,-5.958
ADD=44 RD=0,1 UZ=-5.958,-6.615
ADD=45 RD=0,1 UZ=-6.615,-6.928
ADD=46 RD=0,1 UZ=-6.928,-7.189
ADD=47 RD=0,1 UZ=-7.189,-7.58
ADD=48 RD=0,1 UZ=-7.58,-7.986

NAME=PHW

TYPE=DISTRIBUTED SPAN

ADD=1 RD=0,1 UX=5.018,4.724
ADD=2 RD=0,1 UX=4.724,4.43
ADD=3 RD=0,1 UX=4.43,4.136
ADD=4 RD=0,1 UX=4.136,3.944
ADD=5 RD=0,1 UX=3.944,3.75
ADD=6 RD=0,1 UX=3.75,3.562
ADD=7 RD=0,1 UX=3.562,3.437
ADD=8 RD=0,1 UX=3.437,3.287
ADD=9 RD=0,1 UX=3.287,2.971
ADD=10 RD=0,1 UX=2.971,2.736
ADD=11 RD=0,1 UX=2.736,2.578
ADD=12 RD=0,1 UX=2.578,2.488
ADD=13 RD=0,1 UX=2.488,2.463
ADD=14 RD=0,1 UX=-2.463,-2.488
ADD=15 RD=0,1 UX=-2.488,-2.578
ADD=16 RD=0,1 UX=-2.578,-2.736
ADD=17 RD=0,1 UX=-2.736,-2.971
ADD=18 RD=0,1 UX=-2.971,-3.287
ADD=19 RD=0,1 UX=-3.287,-3.437
ADD=20 RD=0,1 UX=-3.437,-3.562
ADD=21 RD=0,1 UX=-3.562,-3.75
ADD=22 RD=0,1 UX=-3.75,-3.944
ADD=23 RD=0,1 UX=-3.944,-4.136

ADD=24 RD=0,1 UX=-6.621,-7.241
ADD=25 RD=0,1 UX=-7.241,-7.862
ADD=26 RD=0,1 UX=-7.862,-8.483
ADD=27 RD=0,1 UX=-8.483,-7.862
ADD=28 RD=0,1 UX=7.862,7.241
ADD=29 RD=0,1 UX=7.241,6.621
ADD=30 RD=0,1 UX=6.621,6.216
ADD=31 RD=0,1 UX=5.805,5.409
ADD=32 RD=0,1 UX=5.409,5.144
ADD=33 RD=0,1 UX=5.144,4.828
ADD=34 RD=0,1 UX=4.828,4.162
ADD=35 RD=0,1 UX=4.162,3.665
ADD=36 RD=0,1 UX=3.665,3.331
ADD=37 RD=0,1 UX=3.331,3.142
ADD=38 RD=0,1 UX=3.142,3.088
ADD=39 RD=0,1 UX=-3.088,-3.142
ADD=40 RD=0,1 UX=-3.142,-3.331
ADD=41 RD=0,1 UX=-3.331,-3.665
ADD=42 RD=0,1 UX=-3.665,-4.162
ADD=43 RD=0,1 UX=-4.162,-4.828
ADD=44 RD=0,1 UX=-4.828,-5.144
ADD=45 RD=0,1 UX=-5.144,-5.409
ADD=46 RD=0,1 UX=-5.409,-5.805
ADD=47 RD=0,1 UX=-5.805,-6.216
ADD=48 RD=0,1 UX=-6.216,-6.621
ADD=49 RD=0,1 UX=-6.621,-7.241
ADD=50 RD=0,1 UX=-7.241,-7.862
ADD=51 RD=0,1 UX=-7.862,-8.483
ADD=52 RD=0,1 UX=-8.483,-7.862
ADD=53 RD=0,1 UX=-7.862,-7.241
ADD=102 RD=0,1 UX=5.956,5.636
ADD=302 RD=0,1 UX=-6.035,-6.344
ADD=101 RD=0,1 UX=5.636,5.018
ADD=301 RD=0,1 UX=-5.018,-6.035

NAME=PW

TYPE=DISTRIBUTED SPAN

ADD=1 RD=0,1 UZ=-6.929,-6.276
ADD=2 RD=0,1 UZ=-6.276,-5.622
ADD=3 RD=0,1 UZ=-5.622,-4.969
ADD=4 RD=0,1 UZ=-4.969,-4.543
ADD=5 RD=0,1 UZ=-4.543,-4.11
ADD=6 RD=0,1 UZ=-4.11,-3.694
ADD=7 RD=0,1 UZ=-3.694,-3.415
ADD=8 RD=0,1 UZ=-3.415,-3.082
ADD=9 RD=0,1 UZ=-3.082,-2.381
ADD=10 RD=0,1 UZ=-2.381,-1.858
ADD=11 RD=0,1 UZ=-1.858,-1.506
ADD=12 RD=0,1 UZ=-1.506,-1.307
ADD=13 RD=0,1 UZ=-1.307,-1.25
ADD=14 RD=0,1 UZ=-1.25,-1.307
ADD=15 RD=0,1 UZ=-1.307,-1.506
ADD=16 RD=0,1 UZ=-1.506,-1.858
ADD=17 RD=0,1 UZ=-1.858,-2.381
ADD=18 RD=0,1 UZ=-2.381,-3.082
ADD=19 RD=0,1 UZ=-3.082,-3.415
ADD=20 RD=0,1 UZ=-3.415,-3.694
ADD=33 RD=0,1 UZ=-3.694,-3.415
ADD=34 RD=0,1 UZ=-3.415,-3.082
ADD=35 RD=0,1 UZ=-3.082,-2.381
ADD=36 RD=0,1 UZ=-2.381,-1.858
ADD=37 RD=0,1 UZ=-1.858,-1.506
ADD=38 RD=0,1 UZ=-1.506,-1.307
ADD=39 RD=0,1 UZ=-1.307,-1.25
ADD=40 RD=0,1 UZ=-1.25,-1.307
ADD=41 RD=0,1 UZ=-1.307,-1.506
ADD=42 RD=0,1 UZ=-1.506,-1.858
ADD=43 RD=0,1 UZ=-1.858,-2.381
ADD=44 RD=0,1 UZ=-2.381,-3.082
ADD=45 RD=0,1 UZ=-3.082,-3.415
ADD=46 RD=0,1 UZ=-3.415,-3.694
ADD=47 RD=0,1 UZ=-3.694,-4.11
ADD=48 RD=0,1 UZ=-4.11,-4.543
ADD=49 RD=0,1 UZ=-4.543,-4.969
ADD=50 RD=0,1 UZ=-4.969,-5.622
ADD=52 RD=0,1 UZ=-5.622,-6.276
ADD=53 RD=0,1 UZ=-6.276,-6.929
ADD=102 RD=0,1 UZ=-9.014,-8.302
ADD=101 RD=0,1 UZ=-8.302,-6.929
ADD=302 RD=0,1 UZ=-9.188,-9.875
ADD=301 RD=0,1 UZ=-6.929,-9.188
ADD=400 RD=0,1 UZ=9.714,9.714
ADD=401 RD=0,1 UZ=9.714,9.727
ADD=402 RD=0,1 UZ=9.727,9.754
ADD=403 RD=0,1 UZ=9.754,9.78
ADD=404 RD=0,1 UZ=9.78,9.807
ADD=405 RD=0,1 UZ=9.807,9.833
ADD=406 RD=0,1 UZ=9.833,9.86
ADD=407 RD=0,1 UZ=9.86,9.886
ADD=408 RD=0,1 UZ=9.886,9.913
ADD=409 RD=0,1 UZ=9.913,9.939
ADD=410 RD=0,1 UZ=9.939,9.966

ADD=411 RD=0,1 UZ=9.966,9.992
ADD=412 RD=0,1 UZ=9.992,10.019
ADD=413 RD=0,1 UZ=10.019,10.048
ADD=414 RD=0,1 UZ=10.048,10.072
ADD=415 RD=0,1 UZ=10.072,10.098
ADD=416 RD=0,1 UZ=10.098,10.125
ADD=417 RD=0,1 UZ=10.125,10.144
ADD=418 RD=0,1 UZ=10.144,10.164
ADD=419 RD=0,1 UZ=10.164,10.191
ADD=420 RD=0,1 UZ=10.191,10.217
ADD=421 RD=0,1 UZ=10.217,10.241
ADD=422 RD=0,1 UZ=10.241,10.27
ADD=423 RD=0,1 UZ=10.27,10.297
ADD=424 RD=0,1 UZ=10.297,10.323
ADD=425 RD=0,1 UZ=10.323,10.35
ADD=426 RD=0,1 UZ=10.35,10.376
ADD=427 RD=0,1 UZ=10.376,10.403
ADD=428 RD=0,1 UZ=10.403,10.429
ADD=429 RD=0,1 UZ=10.429,10.456
ADD=430 RD=0,1 UZ=10.456,10.482
ADD=431 RD=0,1 UZ=10.482,10.509
ADD=432 RD=0,1 UZ=10.509,10.535
ADD=433 RD=0,1 UZ=10.535,10.562
ADD=434 RD=0,1 UZ=10.562,10.575
ADD=435 RD=0,1 UZ=10.575,10.575

NAME=PL

TYPE=CONCENTRATED SPAN

ADD=415 RD=.755 UZ=-9.6
ADD=413 RD=.717 UZ=-9.6
ADD=412 RD=.415 UZ=-9.6
ADD=410 RD=.321 UZ=-9.6
ADD=408 RD=.962 UZ=-9.6
ADD=406 RD=.925 UZ=-9.6
ADD=420 RD=.245 UZ=-9.6
ADD=422 RD=.283 UZ=-9.6
ADD=423 RD=.642 UZ=-9.6
ADD=425 RD=.679 UZ=-9.6
ADD=427 RD=.038 UZ=-9.6
ADD=429 RD=.076 UZ=-9.6

NAME=PVL

TYPE=DISTRIBUTED SPAN

ADD=5 RD=0,1 UZ=-1.186,-1.186
ADD=6 RD=0,1 UZ=-1.186,-1.186
ADD=7 RD=0,1 UZ=-1.186,-1.186
ADD=8 RD=0,1 UZ=-1.186,-1.186
ADD=9 RD=0,1 UZ=-1.186,-1.186
ADD=10 RD=0,1 UZ=-1.186,-1.186
ADD=11 RD=0,1 UZ=-1.186,-1.186
ADD=12 RD=0,1 UZ=-1.186,-1.186
ADD=13 RD=0,1 UZ=-1.186,-1.186
ADD=14 RD=0,1 UZ=-1.186,-1.186
ADD=15 RD=0,1 UZ=-1.186,-1.186
ADD=16 RD=0,1 UZ=-1.186,-1.186
ADD=17 RD=0,1 UZ=-1.186,-1.186
ADD=18 RD=0,1 UZ=-1.186,-1.186
ADD=19 RD=0,1 UZ=-1.186,-1.186
ADD=20 RD=0,1 UZ=-1.186,-1.186
ADD=21 RD=0,1 UZ=-1.186,-1.186
ADD=22 RD=0,1 UZ=-1.186,-1.186
ADD=31 RD=0,1 UZ=-1.186,-1.186
ADD=32 RD=0,1 UZ=-1.186,-1.186
ADD=33 RD=0,1 UZ=-1.186,-1.186
ADD=34 RD=0,1 UZ=-1.186,-1.186
ADD=35 RD=0,1 UZ=-1.186,-1.186
ADD=36 RD=0,1 UZ=-1.186,-1.186
ADD=37 RD=0,1 UZ=-1.186,-1.186
ADD=38 RD=0,1 UZ=-1.186,-1.186
ADD=39 RD=0,1 UZ=-1.186,-1.186
ADD=40 RD=0,1 UZ=-1.186,-1.186
ADD=41 RD=0,1 UZ=-1.186,-1.186
ADD=42 RD=0,1 UZ=-1.186,-1.186
ADD=43 RD=0,1 UZ=-1.186,-1.186
ADD=44 RD=0,1 UZ=-1.186,-1.186
ADD=45 RD=0,1 UZ=-1.186,-1.186
ADD=46 RD=0,1 UZ=-1.186,-1.186
ADD=47 RD=0,1 UZ=-1.186,-1.186
ADD=48 RD=0,1 UZ=-1.186,-1.186

COMBO

NAME=COMB1

LOAD=SW SF=1.3
LOAD=PV SF=1.5
LOAD=PH SF=1.7

NAME=COMB2

LOAD=SW SF=1.3
LOAD=PV SF=1.5
LOAD=PH SF=.65

NAME=COMB3

LOAD=SW SF=1.3
LOAD=PVW SF=1.5

LOAD=PHW SF=1.7
LOAD=PW SF=1.3
NAME=COMB4
LOAD=SW SF=1.3
LOAD=PVW SF=1.5
LOAD=PHW SF=.65
LOAD=PW SF=1.3
NAME=COMB5
LOAD=SW SF=1.3
LOAD=PV SF=1.5
LOAD=PH SF=1.7
LOAD=PVL SF=1.3
NAME=COMB6
LOAD=SW SF=1.3
LOAD=PV SF=1.5
LOAD=PH SF=.65
LOAD=PVL SF=1.3
NAME=COMB7
LOAD=SW SF=1
LOAD=PV SF=1
LOAD=PH SF=1
NAME=COMB8
LOAD=SW SF=1
LOAD=PV SF=1
LOAD=PH SF=1
LOAD=PL SF=1
NAME=COMB9
LOAD=SW SF=1
LOAD=PV SF=1
LOAD=PH SF=.5
NAME=COMB10
LOAD=SW SF=1
LOAD=PV SF=1
LOAD=PH SF=.5
LOAD=PL SF=1
NAME=COMB11
LOAD=SW SF=1
LOAD=PVW SF=1
LOAD=PHW SF=1
NAME=COMB12
LOAD=SW SF=1
LOAD=PVW SF=1
LOAD=PHW SF=1
LOAD=PL SF=1

OUTPUT

; No Output Requested

END

; The following data is used for graphics, design and pushover analysis.

; If changes are made to the analysis data above, then the following data

; should be checked for consistency.

SAP2000 V7.10 SUPPLEMENTAL DATA

GRID GLOBAL X "1" -15.25
GRID GLOBAL Y "2" 0
GRID GLOBAL Z "3" -8.625
GRID GLOBAL X "4" 0
GRID GLOBAL Z "5" 0
GRID GLOBAL X "6" 15.25
MATERIAL STEEL FY 25310.51
MATERIAL CONC FYREBAR 40000 FYSHEAR 28122.79 FC
4000 FCSHEAR 2812.279
MATERIAL RIGID FYREBAR 40000 FYSHEAR 28122.79
FC 4000 FCSHEAR 2812.279
MATERIAL CONCI FYREBAR 40000 FYSHEAR 28122.79
FC 4000 FCSHEAR 2812.279
CONCRETESECTION T1 COLUMN COVER .05 REBAR
RR-3-3
CONCRETESECTION T2 COLUMN COVER .0542 REBAR
RR-3-3
CONCRETESECTION T3 COLUMN COVER .0675 REBAR
RR-3-3
CONCRETESECTION T4 COLUMN COVER .0916 REBAR
RR-3-3
CONCRETESECTION T5 COLUMN COVER .068 REBAR
RR-3-3
CONCRETESECTION T6 COLUMN COVER .0553 REBAR
RR-3-3
CONCRETESECTION T7 COLUMN COVER .0511 REBAR
RR-3-3
CONCRETESECTION T8 COLUMN COVER .05 REBAR
RR-3-3
CONCRETESECTION FOOT COLUMN COVER .14 REBAR
RR-3-3
CONCRETESECTION WALL COLUMN COVER .085 REBAR
RR-3-3
CONCRETESECTION RIGID COLUMN COVER 1 REBAR

RR-3-3
CONCRETESECTION WALL1 COLUMN COVER .13 REBAR
RR-3-3
STATICLOAD SW TYPE DEAD
STATICLOAD PV TYPE DEAD
STATICLOAD PH TYPE DEAD
STATICLOAD PVW TYPE DEAD
STATICLOAD PHW TYPE DEAD
STATICLOAD PW TYPE DEAD
STATICLOAD PL TYPE DEAD
STATICLOAD PVL TYPE DEAD
END SUPPLEMENTAL DATA

; File D:\SAP2000DATA\만영개착식터널\MAT4.\$2k
saved 10-9-02 10:03:10 in Ton-m

SYSTEM

DOF=UX,UZ,RY LENGTH=m FORCE=Ton LINES=59

JOINT

1 X=-14.25 Y=0 Z=-5.679
2 X=-14.25 Y=0 Z=-5.026
3 X=-14.25 Y=0 Z=-4.372
4 X=-14.25 Y=0 Z=-3.719
5 X=-14.23 Y=0 Z=-3.293
6 X=-14.166 Y=0 Z=-2.86
7 X=-14.107 Y=0 Z=-2.444
8 X=-13.748 Y=0 Z=-2.165
9 X=-13.294 Y=0 Z=-1.832
10 X=-12.092 Y=0 Z=-1.131
11 X=-10.887 Y=0 Z=-.608
12 X=-9.683 Y=0 Z=-.256
13 X=-8.479 Y=0 Z=-.057
14 X=-7.275 Y=0 Z=0
15 X=-6.071 Y=0 Z=-.057
16 X=-4.867 Y=0 Z=-.256
17 X=-3.663 Y=0 Z=-.608
18 X=-2.458 Y=0 Z=-1.131
19 X=-1.256 Y=0 Z=-1.832
20 X=-.795 Y=0 Z=-2.165
21 X=-.443 Y=0 Z=-2.444
22 X=-.369 Y=0 Z=-2.86
23 X=-.318 Y=0 Z=-3.293
24 X=-.3 Y=0 Z=-3.719
25 X=-.3 Y=0 Z=-4.372
26 X=-.3 Y=0 Z=-5.026
27 X=-.3 Y=0 Z=-5.679
28 X=.3 Y=0 Z=-5.679
29 X=.3 Y=0 Z=-5.026
30 X=.3 Y=0 Z=-4.372
31 X=.3 Y=0 Z=-3.719
32 X=.318 Y=0 Z=-3.293
33 X=.369 Y=0 Z=-2.86
34 X=.443 Y=0 Z=-2.444
35 X=.795 Y=0 Z=-2.165
36 X=1.256 Y=0 Z=-1.832
37 X=2.458 Y=0 Z=-1.131
38 X=3.663 Y=0 Z=-.608
39 X=4.867 Y=0 Z=-.256
40 X=6.071 Y=0 Z=-.057
41 X=7.275 Y=0 Z=0
42 X=8.479 Y=0 Z=-.057
43 X=9.683 Y=0 Z=-.256
44 X=10.887 Y=0 Z=-.608
45 X=12.092 Y=0 Z=-1.131
46 X=13.294 Y=0 Z=-1.832
47 X=13.748 Y=0 Z=-2.165
48 X=14.107 Y=0 Z=-2.444
49 X=14.166 Y=0 Z=-2.86
50 X=14.23 Y=0 Z=-3.293
51 X=14.25 Y=0 Z=-3.719
52 X=14.25 Y=0 Z=-4.372
53 X=14.25 Y=0 Z=-5.026
54 X=14.25 Y=0 Z=-5.679
101 X=-14.325 Y=0 Z=-5.679
102 X=-14.325 Y=0 Z=-7.052
201 X=0 Y=0 Z=-5.679
202 X=0 Y=0 Z=-7.475
301 X=14.325 Y=0 Z=-5.679
302 X=14.325 Y=0 Z=-7.938
401 X=-15.25 Y=0 Z=-7.764
402 X=-14.325 Y=0 Z=-7.764
403 X=-13.9 Y=0 Z=-7.777
404 X=-13.017 Y=0 Z=-7.804
405 X=-12.133 Y=0 Z=-7.83
406 X=-11.25 Y=0 Z=-7.857
407 X=-10.367 Y=0 Z=-7.883
408 X=-9.484 Y=0 Z=-7.91
409 X=-8.6 Y=0 Z=-7.936
410 X=-7.717 Y=0 Z=-7.963
411 X=-6.834 Y=0 Z=-7.989
412 X=-5.95 Y=0 Z=-8.016
413 X=-5.067 Y=0 Z=-8.042
414 X=-4.184 Y=0 Z=-8.069
415 X=-3.3 Y=0 Z=-8.098
416 X=-2.417 Y=0 Z=-8.122
417 X=-1.534 Y=0 Z=-8.148
418 X=-.65 Y=0 Z=-8.175
419 X=0 Y=0 Z=-8.194
420 X=.65 Y=0 Z=-8.214
421 X=1.534 Y=0 Z=-8.241

422 X=2.417 Y=0 Z=-8.267
423 X=3.3 Y=0 Z=-8.291
424 X=4.184 Y=0 Z=-8.32
425 X=5.067 Y=0 Z=-8.347
426 X=5.95 Y=0 Z=-8.373
427 X=6.834 Y=0 Z=-8.4
428 X=7.717 Y=0 Z=-8.426
429 X=8.6 Y=0 Z=-8.453
430 X=9.484 Y=0 Z=-8.479
431 X=10.367 Y=0 Z=-8.506
432 X=11.25 Y=0 Z=-8.532
433 X=12.133 Y=0 Z=-8.559
434 X=13.017 Y=0 Z=-8.585
435 X=13.9 Y=0 Z=-8.612
436 X=14.325 Y=0 Z=-8.625
437 X=15.25 Y=0 Z=-8.625

PATTERN

NAME=TEMP
NAME=PRES

SPRING

ADD=401 U3=201064.2
ADD=418 U3=333440.5
ADD=419 U1=10000 U3=282576.7
ADD=420 U3=333440.5
ADD=437 U3=201064.2

MATERIAL

NAME=CONC IDES=C M=.2448 W=2.5
T=0 E=2800000 U=.2 A=.00001
NAME=STEEL IDES=S
T=0 E=2E+10 U=.3 A=.0000117 FY=25310.51
NAME=RIGID IDES=C
T=0 E=2464750 U=.3 A=.00001
NAME=CONC1 IDES=C M=.2448 W=2.5
T=0 E=2464750 U=.2 A=.00001

FRAME SECTION

NAME=T1 MAT=CONC SH=R T=.5,1 A=.5
J=2.861003E-02 I=1.041667E-02,4.897667E-02
AS=.4166667,.4166667
NAME=T2 MAT=CONC SH=R T=.542,1 A=.542
J=3.508126E-02 I=1.326834E-02,4.516667E-02
AS=.4516667,.4516667
NAME=T3 MAT=CONC SH=R T=.675,1 A=.675
J=5.967503E-02 I=2.562891E-02,.05625
AS=.5625,.5625
NAME=T4 MAT=CONC SH=R T=.916,1 A=.916
J=.1170223 I=6.404794E-02,7.633334E-02
AS=.7633333,.7633333
NAME=T5 MAT=CONC SH=R T=.68,1 A=.68
J=6.070982E-02 I=2.620267E-02,5.666667E-02
AS=.5666667,.5666667
NAME=T6 MAT=CONC SH=R T=.553,1 A=.553
J=3.688483E-02 I=.0140927,4.608333E-02
AS=.4608333,.4608333
NAME=T7 MAT=CONC SH=R T=.511,1 A=.511
J=3.024029E-02 I=.0111194,4.258334E-02
AS=.4258333,.4258333
NAME=T8 MAT=CONC SH=R T=.5,1 A=.5
J=2.861003E-02 I=1.041667E-02,4.897667E-02
AS=.4166667,.4166667
NAME=FOOT MAT=CONC1 SH=R T=1.4,1 A=1.4
J=.2612221 I=.2286666,.1166667
AS=1.166667,1.166667
NAME=WALL MAT=CONC1 SH=R T=.85,1 A=.85
J=9.985562E-02 I=4.117709E-02,7.083333E-02
AS=.7083334,.7083334
NAME=RIGID MAT=RIGID SH=R T=10,10 A=100
J=1408.333 I=833.5623,833.5623
AS=83.56233,83.56233
NAME=WALL1 MAT=CONC1 SH=R T=1.3,1 A=1.3
J=.2294606 I=.1830833,.1083333
AS=1.083333,1.083333
NAME=VAR1 TYPE=NONPR
SEC=T1,T2 EIVAR=1,1 L=.426
NAME=VAR2 TYPE=NONPR
SEC=T2,T3 EIVAR=1,1 L=.436
NAME=VAR3 TYPE=NONPR
SEC=T3,T4 EIVAR=1,1 L=.422
NAME=VAR4 TYPE=NONPR
SEC=T4,T5 EIVAR=1,1 L=.455
NAME=VAR5 TYPE=NONPR
SEC=T5,T6 EIVAR=1,1 L=.563
NAME=VAR6 TYPE=NONPR
SEC=T6,T7 EIVAR=1,1 L=1.392
NAME=VAR7 TYPE=NONPR
SEC=T7,T8 EIVAR=1,1 L=1.313

FRAME

```
1 J=1,2 SEC=T1 NSEG=1 ANG=180 IREL=R3
2 J=2,3 SEC=T1 NSEG=1 ANG=180
3 J=3,4 SEC=T1 NSEG=1 ANG=180
4 J=4,5 SEC=VAR1 NSEG=1 ANG=0
5 J=5,6 SEC=VAR2 NSEG=1 ANG=0
6 J=6,7 SEC=VAR3 NSEG=1 ANG=0
7 J=7,8 SEC=VAR4 NSEG=1 ANG=0
8 J=8,9 SEC=VAR5 NSEG=1 ANG=0
9 J=9,10 SEC=VAR6 NSEG=1 ANG=0
10 J=10,11 SEC=VAR7 NSEG=1 ANG=0
11 J=11,12 SEC=T8 NSEG=1 ANG=0
12 J=12,13 SEC=T8 NSEG=1 ANG=0
13 J=13,14 SEC=T8 NSEG=1 ANG=0
14 J=14,15 SEC=T8 NSEG=1 ANG=0
15 J=15,16 SEC=T8 NSEG=1 ANG=0
16 J=16,17 SEC=T8 NSEG=1 ANG=0
17 J=17,18 SEC=VAR7 NSEG=1 ANG=0
18 J=18,19 SEC=VAR6 NSEG=1 ANG=0
19 J=19,20 SEC=VAR5 NSEG=1 ANG=0
20 J=20,21 SEC=VAR4 NSEG=1 ANG=0
21 J=21,22 SEC=VAR3 NSEG=1 ANG=0
22 J=22,23 SEC=VAR2 NSEG=1 ANG=0
23 J=23,24 SEC=VAR1 NSEG=1 ANG=0
24 J=24,25 SEC=T1 NSEG=1 ANG=0
25 J=25,26 SEC=T1 NSEG=1 ANG=0
26 J=26,27 SEC=T1 NSEG=1 ANG=0 JREL=R3
27 J=28,29 SEC=T1 NSEG=1 ANG=180 IREL=R3
28 J=29,30 SEC=T1 NSEG=1 ANG=180
29 J=30,31 SEC=T1 NSEG=1 ANG=180
30 J=31,32 SEC=VAR1 NSEG=1 ANG=0
31 J=32,33 SEC=VAR2 NSEG=1 ANG=0
32 J=33,34 SEC=VAR3 NSEG=1 ANG=0
33 J=34,35 SEC=VAR4 NSEG=1 ANG=0
34 J=35,36 SEC=VAR5 NSEG=1 ANG=0
35 J=36,37 SEC=VAR6 NSEG=1 ANG=0
36 J=37,38 SEC=VAR7 NSEG=1 ANG=0
37 J=38,39 SEC=T8 NSEG=1 ANG=0
38 J=39,40 SEC=T8 NSEG=1 ANG=0
39 J=40,41 SEC=T8 NSEG=1 ANG=0
40 J=41,42 SEC=T8 NSEG=1 ANG=0
41 J=42,43 SEC=T8 NSEG=1 ANG=0
42 J=43,44 SEC=T8 NSEG=1 ANG=0
43 J=44,45 SEC=VAR7 NSEG=1 ANG=0
44 J=45,46 SEC=VAR6 NSEG=1 ANG=0
45 J=46,47 SEC=VAR5 NSEG=1 ANG=0
46 J=47,48 SEC=VAR4 NSEG=1 ANG=0
47 J=48,49 SEC=VAR3 NSEG=1 ANG=0
48 J=49,50 SEC=VAR2 NSEG=1 ANG=0
49 J=50,51 SEC=VAR1 NSEG=1 ANG=0
50 J=51,52 SEC=T1 NSEG=1 ANG=0
52 J=52,53 SEC=T1 NSEG=1 ANG=0
53 J=53,54 SEC=T1 NSEG=1 ANG=0 JREL=R3
85 J=28,201 SEC=RIGID NSEG=1 ANG=0
86 J=201,27 SEC=RIGID NSEG=1 ANG=0
87 J=301,54 SEC=RIGID NSEG=1 ANG=0
88 J=1,101 SEC=RIGID NSEG=1 ANG=0
101 J=102,101 SEC=WALL NSEG=1 ANG=180
102 J=402,102 SEC=WALL NSEG=1 ANG=180
IOFF=.02475 RIGID=0
201 J=202,201 SEC=WALL1 NSEG=1 ANG=0
202 J=419,202 SEC=WALL1 NSEG=1 ANG=0
IOFF=.375 RIGID=0
301 J=301,302 SEC=WALL NSEG=1 ANG=0
302 J=302,436 SEC=WALL NSEG=1 ANG=0
JOFF=.4875 RIGID=0
400 J=401,402 SEC=FOOT NSEG=1 ANG=0
401 J=402,403 SEC=FOOT NSEG=1 ANG=0
IOFF=.075 RIGID=0
402 J=403,404 SEC=FOOT NSEG=1 ANG=0
403 J=404,405 SEC=FOOT NSEG=1 ANG=0
404 J=405,406 SEC=FOOT NSEG=1 ANG=0
405 J=406,407 SEC=FOOT NSEG=1 ANG=0
406 J=407,408 SEC=FOOT NSEG=1 ANG=0
407 J=408,409 SEC=FOOT NSEG=1 ANG=0
408 J=409,410 SEC=FOOT NSEG=1 ANG=0
409 J=410,411 SEC=FOOT NSEG=1 ANG=0
410 J=411,412 SEC=FOOT NSEG=1 ANG=0
411 J=412,413 SEC=FOOT NSEG=1 ANG=0
412 J=413,414 SEC=FOOT NSEG=1 ANG=0
413 J=414,415 SEC=FOOT NSEG=1 ANG=0
414 J=415,416 SEC=FOOT NSEG=1 ANG=0
415 J=416,417 SEC=FOOT NSEG=1 ANG=0
416 J=417,418 SEC=FOOT NSEG=1 ANG=0
417 J=418,419 SEC=FOOT NSEG=1 ANG=0
JOFF=.3 RIGID=0
418 J=419,420 SEC=FOOT NSEG=1 ANG=0
IOFF=.3 RIGID=0
419 J=420,421 SEC=FOOT NSEG=1 ANG=0
420 J=421,422 SEC=FOOT NSEG=1 ANG=0
```

```
421 J=422,423 SEC=FOOT NSEG=1 ANG=0
422 J=423,424 SEC=FOOT NSEG=1 ANG=0
423 J=424,425 SEC=FOOT NSEG=1 ANG=0
424 J=425,426 SEC=FOOT NSEG=1 ANG=0
425 J=426,427 SEC=FOOT NSEG=1 ANG=0
426 J=427,428 SEC=FOOT NSEG=1 ANG=0
427 J=428,429 SEC=FOOT NSEG=1 ANG=0
428 J=429,430 SEC=FOOT NSEG=1 ANG=0
429 J=430,431 SEC=FOOT NSEG=1 ANG=0
430 J=431,432 SEC=FOOT NSEG=1 ANG=0
431 J=432,433 SEC=FOOT NSEG=1 ANG=0
432 J=433,434 SEC=FOOT NSEG=1 ANG=0
433 J=434,435 SEC=FOOT NSEG=1 ANG=0
434 J=435,436 SEC=FOOT NSEG=1 ANG=0
JOFF=.075 RIGID=0
435 J=436,437 SEC=FOOT NSEG=1 ANG=0
```

LOAD

```
NAME=SW SW=1
NAME=PV
TYPE=DISTRIBUTED SPAN
ADD=5 RD=0,1 UZ=-12.459,-11.602
ADD=6 RD=0,1 UZ=-11.602,-10.778
ADD=7 RD=0,1 UZ=-10.778,-10.226
ADD=8 RD=0,1 UZ=-10.226,-9.566
ADD=9 RD=0,1 UZ=-9.566,-8.179
ADD=10 RD=0,1 UZ=-8.179,-7.143
ADD=11 RD=0,1 UZ=-7.143,-6.446
ADD=12 RD=0,1 UZ=-6.446,-6.052
ADD=13 RD=0,1 UZ=-6.052,-5.939
ADD=14 RD=0,1 UZ=-5.939,-6.052
ADD=15 RD=0,1 UZ=-6.052,-6.446
ADD=16 RD=0,1 UZ=-6.446,-7.143
ADD=17 RD=0,1 UZ=-7.143,-8.179
ADD=18 RD=0,1 UZ=-8.179,-9.566
ADD=19 RD=0,1 UZ=-9.566,-10.226
ADD=20 RD=0,1 UZ=-10.226,-10.778
ADD=21 RD=0,1 UZ=-10.778,-11.602
ADD=22 RD=0,1 UZ=-11.602,-12.459
ADD=31 RD=0,1 UZ=-12.459,-11.602
ADD=32 RD=0,1 UZ=-11.602,-10.778
ADD=33 RD=0,1 UZ=-10.778,-10.226
ADD=34 RD=0,1 UZ=-10.226,-9.566
ADD=35 RD=0,1 UZ=-9.566,-8.179
ADD=36 RD=0,1 UZ=-8.179,-7.143
ADD=37 RD=0,1 UZ=-7.143,-6.446
ADD=38 RD=0,1 UZ=-6.446,-6.052
ADD=39 RD=0,1 UZ=-6.052,-5.939
ADD=40 RD=0,1 UZ=-5.939,-6.052
ADD=41 RD=0,1 UZ=-6.052,-6.446
ADD=42 RD=0,1 UZ=-6.446,-7.143
ADD=43 RD=0,1 UZ=-7.143,-8.179
ADD=44 RD=0,1 UZ=-8.179,-9.566
ADD=45 RD=0,1 UZ=-9.566,-10.226
ADD=46 RD=0,1 UZ=-10.226,-10.778
ADD=47 RD=0,1 UZ=-10.778,-11.602
ADD=48 RD=0,1 UZ=-11.602,-12.459
NAME=PH
TYPE=DISTRIBUTED SPAN
ADD=102 RD=0,1 UX=10.463,9.787
ADD=101 RD=0,1 UX=9.787,8.483
ADD=1 RD=0,1 UX=8.483,7.862
ADD=2 RD=0,1 UX=7.862,7.241
ADD=3 RD=0,1 UX=7.241,6.621
ADD=4 RD=0,1 UX=6.621,6.216
ADD=5 RD=0,1 UX=6.216,5.805
ADD=6 RD=0,1 UX=5.805,5.409
ADD=7 RD=0,1 UX=5.409,5.144
ADD=8 RD=0,1 UX=5.144,4.828
ADD=9 RD=0,1 UX=4.828,4.162
ADD=10 RD=0,1 UX=4.162,3.665
ADD=11 RD=0,1 UX=3.665,3.331
ADD=12 RD=0,1 UX=3.331,3.142
ADD=13 RD=0,1 UX=3.142,3.088
ADD=14 RD=0,1 UX=3.088,-3.142
ADD=15 RD=0,1 UX=-3.142,-3.331
ADD=16 RD=0,1 UX=-3.331,-3.665
ADD=17 RD=0,1 UX=-3.665,-4.162
ADD=18 RD=0,1 UX=-4.162,-4.828
ADD=19 RD=0,1 UX=-4.828,-5.144
ADD=20 RD=0,1 UX=-5.144,-5.409
ADD=21 RD=0,1 UX=-5.409,-5.805
ADD=22 RD=0,1 UX=-5.805,-6.216
ADD=23 RD=0,1 UX=-6.216,-6.621
ADD=24 RD=0,1 UX=-6.621,-7.241
ADD=25 RD=0,1 UX=-7.241,-7.862
ADD=26 RD=0,1 UX=-7.862,-8.483
ADD=27 RD=0,1 UX=8.483,7.862
ADD=28 RD=0,1 UX=7.862,7.241
ADD=29 RD=0,1 UX=7.241,6.621
```

ADD=30 RD=0,1 UX=6.621,6.216
ADD=31 RD=0,1 UX=6.216,5.805
ADD=32 RD=0,1 UX=5.805,5.409
ADD=33 RD=0,1 UX=5.409,5.144
ADD=34 RD=0,1 UX=5.144,4.828
ADD=35 RD=0,1 UX=4.828,4.162
ADD=36 RD=0,1 UX=4.162,3.665
ADD=37 RD=0,1 UX=3.665,3.331
ADD=38 RD=0,1 UX=3.331,3.142
ADD=39 RD=0,1 UX=3.142,3.088
ADD=40 RD=0,1 UX=-3.088,-3.142
ADD=41 RD=0,1 UX=-3.142,-3.331
ADD=42 RD=0,1 UX=-3.331,-3.665
ADD=43 RD=0,1 UX=-3.665,-4.162
ADD=44 RD=0,1 UX=-4.162,-4.828
ADD=45 RD=0,1 UX=-4.828,-5.144
ADD=46 RD=0,1 UX=-5.144,-5.409
ADD=47 RD=0,1 UX=-5.409,-5.805
ADD=48 RD=0,1 UX=-5.805,-6.216
ADD=49 RD=0,1 UX=-6.216,-6.621
ADD=50 RD=0,1 UX=-6.621,-7.241
ADD=52 RD=0,1 UX=-7.241,-7.862
ADD=53 RD=0,1 UX=-7.862,-8.483
ADD=301 RD=0,1 UX=-8.483,-10.629
ADD=302 RD=0,1 UX=-10.629,-11.281

NAME=PVW

TYPE=DISTRIBUTED SPAN

ADD=5 RD=0,1 UZ=-7.986,-7.58
ADD=6 RD=0,1 UZ=-7.58,-7.189
ADD=7 RD=0,1 UZ=-7.189,-6.928
ADD=8 RD=0,1 UZ=-6.928,-6.615
ADD=9 RD=0,1 UZ=-6.615,-5.958
ADD=10 RD=0,1 UZ=-5.958,-5.468
ADD=11 RD=0,1 UZ=-5.468,-5.137
ADD=12 RD=0,1 UZ=-5.137,-4.951
ADD=13 RD=0,1 UZ=-4.951,-4.897
ADD=14 RD=0,1 UZ=-4.897,-4.951
ADD=15 RD=0,1 UZ=-4.951,-5.137
ADD=16 RD=0,1 UZ=-5.137,-5.468
ADD=17 RD=0,1 UZ=-5.468,-5.958
ADD=18 RD=0,1 UZ=-5.958,-6.615
ADD=19 RD=0,1 UZ=-6.615,-6.928
ADD=20 RD=0,1 UZ=-6.928,-7.189
ADD=21 RD=0,1 UZ=-7.189,-7.58
ADD=22 RD=0,1 UZ=-7.58,-7.986
ADD=30 RD=0,1 UZ=-7.986,-7.58
ADD=31 RD=0,1 UZ=-7.58,-7.189
ADD=33 RD=0,1 UZ=-7.189,-6.928
ADD=34 RD=0,1 UZ=-6.928,-6.615
ADD=35 RD=0,1 UZ=-6.615,-5.958
ADD=36 RD=0,1 UZ=-5.958,-5.468
ADD=37 RD=0,1 UZ=-5.468,-5.137
ADD=38 RD=0,1 UZ=-5.137,-4.951
ADD=39 RD=0,1 UZ=-4.951,-4.897
ADD=40 RD=0,1 UZ=-4.897,-4.951
ADD=41 RD=0,1 UZ=-4.951,-5.137
ADD=42 RD=0,1 UZ=-5.137,-5.468
ADD=43 RD=0,1 UZ=-5.468,-5.958
ADD=44 RD=0,1 UZ=-5.958,-6.615
ADD=45 RD=0,1 UZ=-6.615,-6.928
ADD=46 RD=0,1 UZ=-6.928,-7.189
ADD=47 RD=0,1 UZ=-7.189,-7.58
ADD=48 RD=0,1 UZ=-7.58,-7.986

NAME=PHW

TYPE=DISTRIBUTED SPAN

ADD=1 RD=0,1 UX=5.018,4.724
ADD=2 RD=0,1 UX=4.724,4.43
ADD=3 RD=0,1 UX=4.43,4.136
ADD=4 RD=0,1 UX=4.136,3.944
ADD=5 RD=0,1 UX=3.944,3.75
ADD=6 RD=0,1 UX=3.75,3.562
ADD=7 RD=0,1 UX=3.562,3.437
ADD=8 RD=0,1 UX=3.437,3.287
ADD=9 RD=0,1 UX=3.287,2.971
ADD=10 RD=0,1 UX=2.971,2.736
ADD=11 RD=0,1 UX=2.736,2.578
ADD=12 RD=0,1 UX=2.578,2.488
ADD=13 RD=0,1 UX=2.488,2.463
ADD=14 RD=0,1 UX=-2.463,-2.488
ADD=15 RD=0,1 UX=-2.488,-2.578
ADD=16 RD=0,1 UX=-2.578,-2.736
ADD=17 RD=0,1 UX=-2.736,-2.971
ADD=18 RD=0,1 UX=-2.971,-3.287
ADD=19 RD=0,1 UX=-3.287,-3.437
ADD=20 RD=0,1 UX=-3.437,-3.562
ADD=21 RD=0,1 UX=-5.409,-5.805
ADD=22 RD=0,1 UX=-5.805,-6.216
ADD=23 RD=0,1 UX=-6.216,-6.621
ADD=24 RD=0,1 UX=-6.621,-7.241
ADD=25 RD=0,1 UX=-7.241,-7.862

ADD=26 RD=0,1 UX=-7.862,-8.483
ADD=27 RD=0,1 UX=8.483,7.862
ADD=28 RD=0,1 UX=7.862,7.241
ADD=29 RD=0,1 UX=7.241,6.621
ADD=30 RD=0,1 UX=6.621,6.216
ADD=31 RD=0,1 UX=6.216,5.805
ADD=32 RD=0,1 UX=5.805,5.409
ADD=33 RD=0,1 UX=3.562,3.437
ADD=34 RD=0,1 UX=3.437,3.287
ADD=35 RD=0,1 UX=3.287,2.971
ADD=36 RD=0,1 UX=2.971,2.736
ADD=37 RD=0,1 UX=2.736,2.578
ADD=38 RD=0,1 UX=2.578,2.488
ADD=39 RD=0,1 UX=2.488,2.463
ADD=40 RD=0,1 UX=-2.463,-2.488
ADD=41 RD=0,1 UX=-2.488,-2.578
ADD=42 RD=0,1 UX=-2.578,-2.736
ADD=43 RD=0,1 UX=-2.736,-2.971
ADD=44 RD=0,1 UX=-2.971,-3.287
ADD=45 RD=0,1 UX=-3.287,-3.437
ADD=46 RD=0,1 UX=-3.437,-3.562
ADD=47 RD=0,1 UX=-3.562,-3.75
ADD=48 RD=0,1 UX=-3.75,-3.944
ADD=49 RD=0,1 UX=-3.944,-4.136
ADD=50 RD=0,1 UX=-4.136,-4.43
ADD=52 RD=0,1 UX=-4.43,-4.724
ADD=53 RD=0,1 UX=-4.724,-5.018
ADD=102 RD=0,1 UX=5.956,5.636
ADD=302 RD=0,1 UX=-6.035,-6.344
ADD=101 RD=0,1 UX=5.636,5.018
ADD=301 RD=0,1 UX=-5.018,-6.035

NAME=PW

TYPE=DISTRIBUTED SPAN

ADD=1 RD=0,1 UZ=-6.929,-6.276
ADD=2 RD=0,1 UZ=-6.276,-5.622
ADD=3 RD=0,1 UZ=-5.622,-4.969
ADD=4 RD=0,1 UZ=-4.969,-4.543
ADD=5 RD=0,1 UZ=-4.543,-4.11
ADD=6 RD=0,1 UZ=-4.11,-3.694
ADD=7 RD=0,1 UZ=-3.694,-3.415
ADD=8 RD=0,1 UZ=-3.415,-3.082
ADD=9 RD=0,1 UZ=-3.082,-2.381
ADD=10 RD=0,1 UZ=-2.381,-1.858
ADD=11 RD=0,1 UZ=-1.858,-1.506
ADD=12 RD=0,1 UZ=-1.506,-1.307
ADD=13 RD=0,1 UZ=-1.307,-1.25
ADD=14 RD=0,1 UZ=-1.25,-1.307
ADD=15 RD=0,1 UZ=-1.307,-1.506
ADD=16 RD=0,1 UZ=-1.506,-1.858
ADD=17 RD=0,1 UZ=-1.858,-2.381
ADD=18 RD=0,1 UZ=-2.381,-3.082
ADD=19 RD=0,1 UZ=-3.082,-3.415
ADD=20 RD=0,1 UZ=-3.415,-3.694
ADD=33 RD=0,1 UZ=-3.694,-3.415
ADD=34 RD=0,1 UZ=-3.415,-3.082
ADD=35 RD=0,1 UZ=-3.082,-2.381
ADD=36 RD=0,1 UZ=-2.381,-1.858
ADD=37 RD=0,1 UZ=-1.858,-1.506
ADD=38 RD=0,1 UZ=-1.506,-1.307
ADD=39 RD=0,1 UZ=-1.307,-1.25
ADD=40 RD=0,1 UZ=-1.25,-1.307
ADD=41 RD=0,1 UZ=-1.307,-1.506
ADD=42 RD=0,1 UZ=-1.506,-3.5628
ADD=43 RD=0,1 UZ=-3.5628,-2.381
ADD=44 RD=0,1 UZ=-2.381,-3.082
ADD=45 RD=0,1 UZ=-3.082,-3.415
ADD=46 RD=0,1 UZ=-3.415,-3.694
ADD=47 RD=0,1 UZ=-3.694,-4.11
ADD=48 RD=0,1 UZ=-4.11,-4.543
ADD=49 RD=0,1 UZ=-4.543,-4.969
ADD=50 RD=0,1 UZ=-4.969,-5.622
ADD=52 RD=0,1 UZ=-5.622,-6.276
ADD=53 RD=0,1 UZ=-6.276,-6.929
ADD=102 RD=0,1 UZ=-9.014,-8.302
ADD=101 RD=0,1 UZ=-8.302,-6.929
ADD=302 RD=0,1 UZ=-9.188,-9.875
ADD=301 RD=0,1 UZ=-6.929,-9.188
ADD=400 RD=0,1 UZ=9.714,9.714
ADD=401 RD=0,1 UZ=9.714,9.727
ADD=402 RD=0,1 UZ=9.727,9.754
ADD=403 RD=0,1 UZ=9.754,9.78
ADD=404 RD=0,1 UZ=9.78,9.807
ADD=405 RD=0,1 UZ=9.807,9.833
ADD=406 RD=0,1 UZ=9.833,9.86
ADD=407 RD=0,1 UZ=9.86,9.886
ADD=408 RD=0,1 UZ=9.886,9.913
ADD=409 RD=0,1 UZ=9.913,9.939
ADD=410 RD=0,1 UZ=9.939,9.966
ADD=411 RD=0,1 UZ=9.966,9.992
ADD=412 RD=0,1 UZ=9.992,10.019

ADD=413 RD=0,1 UZ=10.019,10.048
ADD=414 RD=0,1 UZ=10.048,10.072
ADD=415 RD=0,1 UZ=10.072,10.098
ADD=416 RD=0,1 UZ=10.098,10.125
ADD=417 RD=0,1 UZ=10.125,10.144
ADD=418 RD=0,1 UZ=10.144,10.164
ADD=419 RD=0,1 UZ=10.164,10.191
ADD=420 RD=0,1 UZ=10.191,10.217
ADD=421 RD=0,1 UZ=10.217,10.241
ADD=422 RD=0,1 UZ=10.241,10.27
ADD=423 RD=0,1 UZ=10.27,10.297
ADD=424 RD=0,1 UZ=10.297,10.323
ADD=425 RD=0,1 UZ=10.323,10.35
ADD=426 RD=0,1 UZ=10.35,10.376
ADD=427 RD=0,1 UZ=10.376,10.403
ADD=428 RD=0,1 UZ=10.403,10.429
ADD=429 RD=0,1 UZ=10.429,10.456
ADD=430 RD=0,1 UZ=10.456,10.482
ADD=431 RD=0,1 UZ=10.482,10.509
ADD=432 RD=0,1 UZ=10.509,10.535
ADD=433 RD=0,1 UZ=10.535,10.562
ADD=434 RD=0,1 UZ=10.562,10.575
ADD=435 RD=0,1 UZ=10.575,10.575

NAME=PL

TYPE=CONCENTRATED SPAN

ADD=415 RD=.755 UZ=-9.6
ADD=413 RD=.717 UZ=-9.6
ADD=412 RD=.415 UZ=-9.6
ADD=410 RD=.321 UZ=-9.6
ADD=408 RD=.962 UZ=-9.6
ADD=406 RD=.925 UZ=-9.6
ADD=420 RD=.245 UZ=-9.6
ADD=422 RD=.283 UZ=-9.6
ADD=423 RD=.642 UZ=-9.6
ADD=425 RD=.679 UZ=-9.6
ADD=427 RD=.038 UZ=-9.6
ADD=429 RD=.076 UZ=-9.6

NAME=PVL

TYPE=DISTRIBUTED SPAN

ADD=5 RD=0,1 UZ=-1.186,-1.186
ADD=6 RD=0,1 UZ=-1.186,-1.186
ADD=7 RD=0,1 UZ=-1.186,-1.186
ADD=8 RD=0,1 UZ=-1.186,-1.186
ADD=9 RD=0,1 UZ=-1.186,-1.186
ADD=10 RD=0,1 UZ=-1.186,-1.186
ADD=11 RD=0,1 UZ=-1.186,-1.186
ADD=12 RD=0,1 UZ=-1.186,-1.186
ADD=13 RD=0,1 UZ=-1.186,-1.186
ADD=14 RD=0,1 UZ=-1.186,-1.186
ADD=15 RD=0,1 UZ=-1.186,-1.186
ADD=16 RD=0,1 UZ=-1.186,-1.186
ADD=17 RD=0,1 UZ=-1.186,-1.186
ADD=18 RD=0,1 UZ=-1.186,-1.186
ADD=19 RD=0,1 UZ=-1.186,-1.186
ADD=20 RD=0,1 UZ=-1.186,-1.186
ADD=21 RD=0,1 UZ=-1.186,-1.186
ADD=22 RD=0,1 UZ=-1.186,-1.186
ADD=31 RD=0,1 UZ=-1.186,-1.186
ADD=32 RD=0,1 UZ=-1.186,-1.186
ADD=33 RD=0,1 UZ=-1.186,-1.186
ADD=34 RD=0,1 UZ=-1.186,-1.186
ADD=35 RD=0,1 UZ=-1.186,-1.186
ADD=36 RD=0,1 UZ=-1.186,-1.186
ADD=37 RD=0,1 UZ=-1.186,-1.186
ADD=38 RD=0,1 UZ=-1.186,-1.186
ADD=39 RD=0,1 UZ=-1.186,-1.186
ADD=40 RD=0,1 UZ=-1.186,-1.186
ADD=41 RD=0,1 UZ=-1.186,-1.186
ADD=42 RD=0,1 UZ=-1.186,-1.186
ADD=43 RD=0,1 UZ=-1.186,-1.186
ADD=44 RD=0,1 UZ=-1.186,-1.186
ADD=45 RD=0,1 UZ=-1.186,-1.186
ADD=46 RD=0,1 UZ=-1.186,-1.186
ADD=47 RD=0,1 UZ=-1.186,-1.186
ADD=48 RD=0,1 UZ=-1.186,-1.186

COMBO

NAME=COMB1

LOAD=SW SF=1.3
LOAD=PV SF=1.5
LOAD=PH SF=1.7

NAME=COMB2

LOAD=SW SF=1.3
LOAD=PV SF=1.5
LOAD=PH SF=.65

NAME=COMB3

LOAD=SW SF=1.3
LOAD=PVW SF=1.5
LOAD=PHW SF=1.7
LOAD=PW SF=1.3

NAME=COMB4

LOAD=SW SF=1.3
LOAD=PVW SF=1.5
LOAD=PHW SF=.65
LOAD=PW SF=1.3

NAME=COMB5

LOAD=SW SF=1.3
LOAD=PV SF=1.5
LOAD=PH SF=1.7
LOAD=PVL SF=1.3

NAME=COMB6

LOAD=SW SF=1.3
LOAD=PV SF=1.5
LOAD=PH SF=.65
LOAD=PVL SF=1.3

NAME=COMB7

LOAD=SW SF=1
LOAD=PV SF=1
LOAD=PH SF=1

NAME=COMB8

LOAD=SW SF=1
LOAD=PV SF=1
LOAD=PH SF=1
LOAD=PL SF=1

NAME=COMB9

LOAD=SW SF=1
LOAD=PV SF=1
LOAD=PH SF=.5

NAME=COMB10

LOAD=SW SF=1
LOAD=PV SF=1
LOAD=PH SF=.5
LOAD=PL SF=1

NAME=COMB11

LOAD=SW SF=1
LOAD=PVW SF=1
LOAD=PHW SF=1

NAME=COMB12

LOAD=SW SF=1
LOAD=PVW SF=1
LOAD=PHW SF=1
LOAD=PL SF=1

OUTPUT

; No Output Requested

END

; The following data is used for graphics, design and pushover analysis.

; If changes are made to the analysis data above, then the following data

; should be checked for consistency.

SAP2000 V7.10 SUPPLEMENTAL DATA

GRID GLOBAL X "1" -15.25
GRID GLOBAL Y "2" 0
GRID GLOBAL Z "3" -8.625
GRID GLOBAL X "4" 0
GRID GLOBAL Z "5" 0
GRID GLOBAL X "6" 15.25
MATERIAL STEEL FY 25310.51
MATERIAL CONC FYREBAR 40000 FYSHEAR 28122.79 FC
4000 FCSHEAR 2812.279
MATERIAL RIGID FYREBAR 40000 FYSHEAR 28122.79
FC 4000 FCSHEAR 2812.279
MATERIAL CONC1 FYREBAR 40000 FYSHEAR 28122.79
FC 4000 FCSHEAR 2812.279
CONCRETESECTION T1 COLUMN COVER .05 REBAR
RR-3-3
CONCRETESECTION T2 COLUMN COVER .0542 REBAR
RR-3-3
CONCRETESECTION T3 COLUMN COVER .0675 REBAR
RR-3-3
CONCRETESECTION T4 COLUMN COVER .0916 REBAR
RR-3-3
CONCRETESECTION T5 COLUMN COVER .068 REBAR
RR-3-3
CONCRETESECTION T6 COLUMN COVER .0553 REBAR
RR-3-3
CONCRETESECTION T7 COLUMN COVER .0511 REBAR
RR-3-3
CONCRETESECTION T8 COLUMN COVER .05 REBAR
RR-3-3
CONCRETESECTION FOOT COLUMN COVER .14 REBAR
RR-3-3
CONCRETESECTION WALL COLUMN COVER .085 REBAR
RR-3-3
CONCRETESECTION RIGID COLUMN COVER 1 REBAR
RR-3-3
CONCRETESECTION WALL1 COLUMN COVER .13 REBAR

RR-3-3
STATICLOAD SW TYPE DEAD
STATICLOAD PV TYPE DEAD
STATICLOAD PH TYPE DEAD
STATICLOAD PVW TYPE DEAD
STATICLOAD PHW TYPE DEAD
STATICLOAD PW TYPE DEAD
STATICLOAD PL TYPE DEAD
STATICLOAD PVL TYPE DEAD
END SUPPLEMENTAL DATA

; File D:\SAP2000DATA\만영개확식터널\MAT6.\$2k
saved 10-9-02 10:17:26 in Ton-m

SYSTEM

DOF=UX,UZ,RV LENGTH=m FORCE=Ton LINES=59

JOINT

```
1 X=-14.25 Y=0 Z=-5.679
2 X=-14.25 Y=0 Z=-5.026
3 X=-14.25 Y=0 Z=-4.372
4 X=-14.25 Y=0 Z=-3.719
5 X=-14.23 Y=0 Z=-3.293
6 X=-14.166 Y=0 Z=-2.86
7 X=-14.107 Y=0 Z=-2.444
8 X=-13.748 Y=0 Z=-2.165
9 X=-13.294 Y=0 Z=-1.832
10 X=-12.092 Y=0 Z=-1.131
11 X=-10.887 Y=0 Z=-.608
12 X=-9.683 Y=0 Z=-.256
13 X=-8.479 Y=0 Z=-.057
14 X=-7.275 Y=0 Z=0
15 X=-6.071 Y=0 Z=-.057
16 X=-4.867 Y=0 Z=-.256
17 X=-3.663 Y=0 Z=-.608
18 X=-2.458 Y=0 Z=-1.131
19 X=-1.256 Y=0 Z=-1.832
20 X=-.795 Y=0 Z=-2.165
21 X=-.443 Y=0 Z=-2.444
22 X=-.369 Y=0 Z=-2.86
23 X=-.318 Y=0 Z=-3.293
24 X=-.3 Y=0 Z=-3.719
25 X=-.3 Y=0 Z=-4.372
26 X=-.3 Y=0 Z=-5.026
27 X=-.3 Y=0 Z=-5.679
28 X=.3 Y=0 Z=-5.679
29 X=.3 Y=0 Z=-5.026
30 X=.3 Y=0 Z=-4.372
31 X=.3 Y=0 Z=-3.719
32 X=.318 Y=0 Z=-3.293
33 X=.369 Y=0 Z=-2.86
34 X=.443 Y=0 Z=-2.444
35 X=.795 Y=0 Z=-2.165
36 X=1.256 Y=0 Z=-1.832
37 X=2.458 Y=0 Z=-1.131
38 X=3.663 Y=0 Z=-.608
39 X=4.867 Y=0 Z=-.256
40 X=6.071 Y=0 Z=-.057
41 X=7.275 Y=0 Z=0
42 X=8.479 Y=0 Z=-.057
43 X=9.683 Y=0 Z=-.256
44 X=10.887 Y=0 Z=-.608
45 X=12.092 Y=0 Z=-1.131
46 X=13.294 Y=0 Z=-1.832
47 X=13.748 Y=0 Z=-2.165
48 X=14.107 Y=0 Z=-2.444
49 X=14.166 Y=0 Z=-2.86
50 X=14.23 Y=0 Z=-3.293
51 X=14.25 Y=0 Z=-3.719
52 X=14.25 Y=0 Z=-4.372
53 X=14.25 Y=0 Z=-5.026
54 X=14.25 Y=0 Z=-5.679
101 X=-14.325 Y=0 Z=-5.679
102 X=-14.325 Y=0 Z=-7.052
201 X=0 Y=0 Z=-5.679
202 X=0 Y=0 Z=-7.475
301 X=14.325 Y=0 Z=-5.679
302 X=14.325 Y=0 Z=-7.938
401 X=-15.25 Y=0 Z=-7.764
402 X=-14.325 Y=0 Z=-7.764
403 X=-13.9 Y=0 Z=-7.777
404 X=-13.017 Y=0 Z=-7.804
405 X=-12.133 Y=0 Z=-7.83
406 X=-11.25 Y=0 Z=-7.857
407 X=-10.367 Y=0 Z=-7.883
408 X=-9.484 Y=0 Z=-7.91
409 X=-8.6 Y=0 Z=-7.936
410 X=-7.717 Y=0 Z=-7.963
411 X=-6.834 Y=0 Z=-7.989
412 X=-5.95 Y=0 Z=-8.016
413 X=-5.067 Y=0 Z=-8.042
414 X=-4.184 Y=0 Z=-8.069
415 X=-3.3 Y=0 Z=-8.098
416 X=-2.417 Y=0 Z=-8.122
417 X=-1.534 Y=0 Z=-8.148
418 X=-.65 Y=0 Z=-8.175
419 X=0 Y=0 Z=-8.194
420 X=.65 Y=0 Z=-8.214
421 X=1.534 Y=0 Z=-8.241
```

```
422 X=2.417 Y=0 Z=-8.267
423 X=3.3 Y=0 Z=-8.291
424 X=4.184 Y=0 Z=-8.32
425 X=5.067 Y=0 Z=-8.347
426 X=5.95 Y=0 Z=-8.373
427 X=6.834 Y=0 Z=-8.4
428 X=7.717 Y=0 Z=-8.426
429 X=8.6 Y=0 Z=-8.453
430 X=9.484 Y=0 Z=-8.479
431 X=10.367 Y=0 Z=-8.506
432 X=11.25 Y=0 Z=-8.532
433 X=12.133 Y=0 Z=-8.559
434 X=13.017 Y=0 Z=-8.585
435 X=13.9 Y=0 Z=-8.612
436 X=14.325 Y=0 Z=-8.625
437 X=15.25 Y=0 Z=-8.625
```

PATTERN

NAME=TEMP
NAME=PRES

SPRING

```
ADD=401 U3=201064.2
ADD=402 U3=293445
ADD=403 U3=284315.6
ADD=404 U3=384087
ADD=405 U3=384087
ADD=406 U3=383869.6
ADD=407 U3=383869.6
ADD=408 U3=384087
ADD=409 U3=384087
ADD=410 U3=383869.6
ADD=411 U3=384087
ADD=412 U3=384087
ADD=413 U3=383869.6
ADD=414 U3=384087
ADD=415 U3=384087
ADD=416 U3=383869.6
ADD=417 U3=384087
ADD=418 U3=333440.5
ADD=419 U1=10000 U3=282576.7
ADD=420 U3=333440.5
ADD=421 U3=384087
ADD=422 U3=383869.6
ADD=423 U3=384087
ADD=424 U3=384087
ADD=425 U3=383869.6
ADD=426 U3=384087
ADD=427 U3=384087
ADD=428 U3=383869.6
ADD=429 U3=384087
ADD=430 U3=384087
ADD=433 U3=384087
ADD=434 U3=384087
ADD=435 U3=284315.6
ADD=436 U3=293445
ADD=437 U3=201064.2
```

MATERIAL

```
NAME=CONC IDES=C M=.2448 W=2.5
T=0 E=2800000 U=.2 A=.00001
NAME=STEEL IDES=S
T=0 E=2E+10 U=.3 A=.0000117 FY=25310.51
NAME=RIGID IDES=C
T=0 E=2464750 U=.3 A=.00001
NAME=CONC1 IDES=C M=.2448 W=2.5
T=0 E=2464750 U=.2 A=.00001
```

FRAME SECTION

```
NAME=T1 MAT=CONC SH=R T=.5,1 A=.5
J=2.861003E-02 I=1.041667E-02,4.897667E-02
AS=.4166667,.4166667
NAME=T2 MAT=CONC SH=R T=.542,1 A=.542
J=3.508126E-02 I=1.326834E-02,4.516667E-02
AS=.4516667,.4516667
NAME=T3 MAT=CONC SH=R T=.675,1 A=.675
J=5.967503E-02 I=2.562891E-02,.05625
AS=.5625,.5625
NAME=T4 MAT=CONC SH=R T=.916,1 A=.916
J=.1170223 I=6.404794E-02,7.633334E-02
AS=.7633333,.7633333
NAME=T5 MAT=CONC SH=R T=.68,1 A=.68
J=6.070982E-02 I=2.620267E-02,5.666667E-02
AS=.5666667,.5666667
NAME=T6 MAT=CONC SH=R T=.553,1 A=.553
J=3.688483E-02 I=.0140927,4.608333E-02
AS=.4608333,.4608333
NAME=T7 MAT=CONC SH=R T=.511,1 A=.511
J=3.024029E-02 I=.0111194,4.258334E-02
AS=.4258333,.4258333
```

NAME=T8 MAT=CONC SH=R T=.5,1 A=.5
J=2.861003E-02 I=1.041667E-02,4.897667E-02
AS=.4166667,.4166667
NAME=FOOT MAT=CONC1 SH=R T=1.4,1 A=1.4
J=.2612221 I=.2286666,.1166667
AS=1.166667,1.166667
NAME=WALL MAT=CONC1 SH=R T=.85,1 A=.85
J=9.985562E-02 I=4.117709E-02,7.083333E-02
AS=.7083334,.7083334
NAME=RIGID MAT=RIGID SH=R T=10,10 A=100
J=1408.333 I=833.5623,833.5623
AS=83.56233,83.56233
NAME=WALL1 MAT=CONC1 SH=R T=1.3,1 A=1.3
J=.2294606 I=.1830833,.1083333
AS=1.083333,1.083333
NAME=VAR1 TYPE=NONPR
SEC=T1,T2 EIVAR=1,1 L=.426
NAME=VAR2 TYPE=NONPR
SEC=T2,T3 EIVAR=1,1 L=.436
NAME=VAR3 TYPE=NONPR
SEC=T3,T4 EIVAR=1,1 L=.422
NAME=VAR4 TYPE=NONPR
SEC=T4,T5 EIVAR=1,1 L=.455
NAME=VAR5 TYPE=NONPR
SEC=T5,T6 EIVAR=1,1 L=.563
NAME=VAR6 TYPE=NONPR
SEC=T6,T7 EIVAR=1,1 L=1.392
NAME=VAR7 TYPE=NONPR
SEC=T7,T8 EIVAR=1,1 L=1.313

FRAME

1 J=1,2 SEC=T1 NSEG=1 ANG=180 IREL=R3
2 J=2,3 SEC=T1 NSEG=1 ANG=180
3 J=3,4 SEC=T1 NSEG=1 ANG=180
4 J=4,5 SEC=VAR1 NSEG=1 ANG=0
5 J=5,6 SEC=VAR2 NSEG=1 ANG=0
6 J=6,7 SEC=VAR3 NSEG=1 ANG=0
7 J=7,8 SEC=VAR4 NSEG=1 ANG=0
8 J=8,9 SEC=VAR5 NSEG=1 ANG=0
9 J=9,10 SEC=VAR6 NSEG=1 ANG=0
10 J=10,11 SEC=VAR7 NSEG=1 ANG=0
11 J=11,12 SEC=T8 NSEG=1 ANG=0
12 J=12,13 SEC=T8 NSEG=1 ANG=0
13 J=13,14 SEC=T8 NSEG=1 ANG=0
14 J=14,15 SEC=T8 NSEG=1 ANG=0
15 J=15,16 SEC=T8 NSEG=1 ANG=0
16 J=16,17 SEC=T8 NSEG=1 ANG=0
17 J=17,18 SEC=VAR7 NSEG=1 ANG=0
18 J=18,19 SEC=VAR6 NSEG=1 ANG=0
19 J=19,20 SEC=VAR5 NSEG=1 ANG=0
20 J=20,21 SEC=VAR4 NSEG=1 ANG=0
21 J=21,22 SEC=VAR3 NSEG=1 ANG=0
22 J=22,23 SEC=VAR2 NSEG=1 ANG=0
23 J=23,24 SEC=VAR1 NSEG=1 ANG=0
24 J=24,25 SEC=T1 NSEG=1 ANG=0
25 J=25,26 SEC=T1 NSEG=1 ANG=0
26 J=26,27 SEC=T1 NSEG=1 ANG=0 JREL=R3
27 J=28,29 SEC=T1 NSEG=1 ANG=180 IREL=R3
28 J=29,30 SEC=T1 NSEG=1 ANG=180
29 J=30,31 SEC=T1 NSEG=1 ANG=180
30 J=31,32 SEC=VAR1 NSEG=1 ANG=0
31 J=32,33 SEC=VAR2 NSEG=1 ANG=0
32 J=33,34 SEC=VAR3 NSEG=1 ANG=0
33 J=34,35 SEC=VAR4 NSEG=1 ANG=0
34 J=35,36 SEC=VAR5 NSEG=1 ANG=0
35 J=36,37 SEC=VAR6 NSEG=1 ANG=0
36 J=37,38 SEC=VAR7 NSEG=1 ANG=0
37 J=38,39 SEC=T8 NSEG=1 ANG=0
38 J=39,40 SEC=T8 NSEG=1 ANG=0
39 J=40,41 SEC=T8 NSEG=1 ANG=0
40 J=41,42 SEC=T8 NSEG=1 ANG=0
41 J=42,43 SEC=T8 NSEG=1 ANG=0
42 J=43,44 SEC=T8 NSEG=1 ANG=0
43 J=44,45 SEC=VAR7 NSEG=1 ANG=0
44 J=45,46 SEC=VAR6 NSEG=1 ANG=0
45 J=46,47 SEC=VAR5 NSEG=1 ANG=0
46 J=47,48 SEC=VAR4 NSEG=1 ANG=0
47 J=48,49 SEC=VAR3 NSEG=1 ANG=0
48 J=49,50 SEC=VAR2 NSEG=1 ANG=0
49 J=50,51 SEC=VAR1 NSEG=1 ANG=0
50 J=51,52 SEC=T1 NSEG=1 ANG=0
52 J=52,53 SEC=T1 NSEG=1 ANG=0
53 J=53,54 SEC=T1 NSEG=1 ANG=0 JREL=R3
85 J=28,201 SEC=RIGID NSEG=1 ANG=0
86 J=201,27 SEC=RIGID NSEG=1 ANG=0
87 J=301,54 SEC=RIGID NSEG=1 ANG=0
88 J=1,101 SEC=RIGID NSEG=1 ANG=0
101 J=102,101 SEC=WALL NSEG=1 ANG=180
102 J=402,102 SEC=WALL NSEG=1 ANG=180
IOFF=.02475 RIGID=0

201 J=202,201 SEC=WALL1 NSEG=1 ANG=0
202 J=419,202 SEC=WALL1 NSEG=1 ANG=0
IOFF=.375 RIGID=0
301 J=301,302 SEC=WALL NSEG=1 ANG=0
302 J=302,436 SEC=WALL NSEG=1 ANG=0
JOFF=.4875 RIGID=0
400 J=401,402 SEC=FOOT NSEG=1 ANG=0
401 J=402,403 SEC=FOOT NSEG=1 ANG=0
IOFF=.075 RIGID=0
402 J=403,404 SEC=FOOT NSEG=1 ANG=0
403 J=404,405 SEC=FOOT NSEG=1 ANG=0
404 J=405,406 SEC=FOOT NSEG=1 ANG=0
405 J=406,407 SEC=FOOT NSEG=1 ANG=0
406 J=407,408 SEC=FOOT NSEG=1 ANG=0
407 J=408,409 SEC=FOOT NSEG=1 ANG=0
408 J=409,410 SEC=FOOT NSEG=1 ANG=0
409 J=410,411 SEC=FOOT NSEG=1 ANG=0
410 J=411,412 SEC=FOOT NSEG=1 ANG=0
411 J=412,413 SEC=FOOT NSEG=1 ANG=0
412 J=413,414 SEC=FOOT NSEG=1 ANG=0
413 J=414,415 SEC=FOOT NSEG=1 ANG=0
414 J=415,416 SEC=FOOT NSEG=1 ANG=0
415 J=416,417 SEC=FOOT NSEG=1 ANG=0
416 J=417,418 SEC=FOOT NSEG=1 ANG=0
417 J=418,419 SEC=FOOT NSEG=1 ANG=0
JOFF=.3 RIGID=0
418 J=419,420 SEC=FOOT NSEG=1 ANG=0
IOFF=.3 RIGID=0
419 J=420,421 SEC=FOOT NSEG=1 ANG=0
420 J=421,422 SEC=FOOT NSEG=1 ANG=0
421 J=422,423 SEC=FOOT NSEG=1 ANG=0
422 J=423,424 SEC=FOOT NSEG=1 ANG=0
423 J=424,425 SEC=FOOT NSEG=1 ANG=0
424 J=425,426 SEC=FOOT NSEG=1 ANG=0
425 J=426,427 SEC=FOOT NSEG=1 ANG=0
426 J=427,428 SEC=FOOT NSEG=1 ANG=0
427 J=428,429 SEC=FOOT NSEG=1 ANG=0
428 J=429,430 SEC=FOOT NSEG=1 ANG=0
429 J=430,431 SEC=FOOT NSEG=1 ANG=0
430 J=431,432 SEC=FOOT NSEG=1 ANG=0
431 J=432,433 SEC=FOOT NSEG=1 ANG=0
432 J=433,434 SEC=FOOT NSEG=1 ANG=0
433 J=434,435 SEC=FOOT NSEG=1 ANG=0
434 J=435,436 SEC=FOOT NSEG=1 ANG=0
JOFF=.075 RIGID=0
435 J=436,437 SEC=FOOT NSEG=1 ANG=0

LOAD

NAME=SW SW=1

NAME=PV

TYPE=DISTRIBUTED SPAN

ADD=5 RD=0,1 UZ=-12.459,-11.602
ADD=6 RD=0,1 UZ=-11.602,-10.778
ADD=7 RD=0,1 UZ=-10.778,-10.226
ADD=8 RD=0,1 UZ=-10.226,-9.566
ADD=9 RD=0,1 UZ=-9.566,-8.179
ADD=10 RD=0,1 UZ=-8.179,-7.143
ADD=11 RD=0,1 UZ=-7.143,-6.446
ADD=12 RD=0,1 UZ=-6.446,-6.052
ADD=13 RD=0,1 UZ=-6.052,-5.939
ADD=14 RD=0,1 UZ=-5.939,-6.052
ADD=15 RD=0,1 UZ=-6.052,-6.446
ADD=16 RD=0,1 UZ=-6.446,-7.143
ADD=17 RD=0,1 UZ=-7.143,-8.179
ADD=18 RD=0,1 UZ=-8.179,-9.566
ADD=19 RD=0,1 UZ=-9.566,-10.226
ADD=20 RD=0,1 UZ=-10.226,-10.778
ADD=21 RD=0,1 UZ=-10.778,-11.602
ADD=22 RD=0,1 UZ=-11.602,-12.459
ADD=31 RD=0,1 UZ=-12.459,-11.602
ADD=32 RD=0,1 UZ=-11.602,-10.778
ADD=33 RD=0,1 UZ=-10.778,-10.226
ADD=34 RD=0,1 UZ=-10.226,-9.566
ADD=35 RD=0,1 UZ=-9.566,-8.179
ADD=36 RD=0,1 UZ=-8.179,-7.143
ADD=37 RD=0,1 UZ=-7.143,-6.446
ADD=38 RD=0,1 UZ=-6.446,-6.052
ADD=39 RD=0,1 UZ=-6.052,-5.939
ADD=40 RD=0,1 UZ=-5.939,-6.052
ADD=41 RD=0,1 UZ=-6.052,-6.446
ADD=42 RD=0,1 UZ=-6.446,-7.143
ADD=43 RD=0,1 UZ=-7.143,-8.179
ADD=44 RD=0,1 UZ=-8.179,-9.566
ADD=45 RD=0,1 UZ=-9.566,-10.226
ADD=46 RD=0,1 UZ=-10.226,-10.778
ADD=47 RD=0,1 UZ=-10.778,-11.602
ADD=48 RD=0,1 UZ=-11.602,-12.459

NAME=PH

TYPE=DISTRIBUTED SPAN

ADD=102 RD=0,1 UX=10.463,9.787

ADD=101 RD=0,1 UX=9.787,8.483
ADD=1 RD=0,1 UX=8.483,7.862
ADD=2 RD=0,1 UX=7.862,7.241
ADD=3 RD=0,1 UX=7.241,6.621
ADD=4 RD=0,1 UX=6.621,6.216
ADD=5 RD=0,1 UX=6.216,5.805
ADD=6 RD=0,1 UX=5.805,5.409
ADD=7 RD=0,1 UX=5.409,5.144
ADD=8 RD=0,1 UX=5.144,4.828
ADD=9 RD=0,1 UX=4.828,4.162
ADD=10 RD=0,1 UX=4.162,3.665
ADD=11 RD=0,1 UX=3.665,3.331
ADD=12 RD=0,1 UX=3.331,3.142
ADD=13 RD=0,1 UX=3.142,3.088
ADD=14 RD=0,1 UX=-3.088,-3.142
ADD=15 RD=0,1 UX=-3.142,-3.331
ADD=16 RD=0,1 UX=-3.331,-3.665
ADD=17 RD=0,1 UX=-3.665,-4.162
ADD=18 RD=0,1 UX=-4.162,-4.828
ADD=19 RD=0,1 UX=-4.828,-5.144
ADD=20 RD=0,1 UX=-5.144,-5.409
ADD=21 RD=0,1 UX=-5.409,-5.805
ADD=22 RD=0,1 UX=-5.805,-6.216
ADD=23 RD=0,1 UX=-6.216,-6.621
ADD=24 RD=0,1 UX=-6.621,-7.241
ADD=25 RD=0,1 UX=-7.241,-7.862
ADD=26 RD=0,1 UX=-7.862,-8.483
ADD=27 RD=0,1 UX=8.483,7.862
ADD=28 RD=0,1 UX=7.862,7.241
ADD=29 RD=0,1 UX=7.241,6.621
ADD=30 RD=0,1 UX=6.621,6.216
ADD=31 RD=0,1 UX=6.216,5.805
ADD=32 RD=0,1 UX=5.805,5.409
ADD=33 RD=0,1 UX=5.409,5.144
ADD=34 RD=0,1 UX=5.144,4.828
ADD=35 RD=0,1 UX=4.828,4.162
ADD=36 RD=0,1 UX=4.162,3.665
ADD=37 RD=0,1 UX=3.665,3.331
ADD=38 RD=0,1 UX=3.331,3.142
ADD=39 RD=0,1 UX=3.142,3.088
ADD=40 RD=0,1 UX=-3.088,-3.142
ADD=41 RD=0,1 UX=-3.142,-3.331
ADD=42 RD=0,1 UX=-3.331,-3.665
ADD=43 RD=0,1 UX=-3.665,-4.162
ADD=44 RD=0,1 UX=-4.162,-4.828
ADD=45 RD=0,1 UX=-4.828,-5.144
ADD=46 RD=0,1 UX=-5.144,-5.409
ADD=47 RD=0,1 UX=-5.409,-5.805
ADD=48 RD=0,1 UX=-5.805,-6.216
ADD=49 RD=0,1 UX=-6.216,-6.621
ADD=50 RD=0,1 UX=-6.621,-7.241
ADD=52 RD=0,1 UX=-7.241,-7.862
ADD=53 RD=0,1 UX=-7.862,-8.483
ADD=301 RD=0,1 UX=-8.483,-10.629
ADD=302 RD=0,1 UX=-10.629,-11.281

NAME=PVW

TYPE=DISTRIBUTED SPAN

ADD=5 RD=0,1 UZ=-7.986,-7.58
ADD=6 RD=0,1 UZ=-7.58,-7.189
ADD=7 RD=0,1 UZ=-7.189,-6.928
ADD=8 RD=0,1 UZ=-6.928,-6.615
ADD=9 RD=0,1 UZ=-6.615,-5.958
ADD=10 RD=0,1 UZ=-5.958,-5.468
ADD=11 RD=0,1 UZ=-5.468,-5.137
ADD=12 RD=0,1 UZ=-5.137,-4.951
ADD=13 RD=0,1 UZ=-4.951,-4.897
ADD=14 RD=0,1 UZ=-4.897,-4.951
ADD=15 RD=0,1 UZ=-4.951,-5.137
ADD=16 RD=0,1 UZ=-5.137,-5.468
ADD=17 RD=0,1 UZ=-5.468,-5.958
ADD=18 RD=0,1 UZ=-5.958,-6.615
ADD=19 RD=0,1 UZ=-6.615,-6.928
ADD=20 RD=0,1 UZ=-6.928,-7.189
ADD=21 RD=0,1 UZ=-7.189,-7.58
ADD=22 RD=0,1 UZ=-7.58,-7.986
ADD=30 RD=0,1 UZ=-7.986,-7.58
ADD=31 RD=0,1 UZ=-7.58,-7.189
ADD=33 RD=0,1 UZ=-7.189,-6.928
ADD=34 RD=0,1 UZ=-6.928,-6.615
ADD=35 RD=0,1 UZ=-6.615,-5.958
ADD=36 RD=0,1 UZ=-5.958,-5.468
ADD=37 RD=0,1 UZ=-5.468,-5.137
ADD=38 RD=0,1 UZ=-5.137,-4.951
ADD=39 RD=0,1 UZ=-4.951,-4.897
ADD=40 RD=0,1 UZ=-4.897,-4.951
ADD=41 RD=0,1 UZ=-4.951,-5.137
ADD=42 RD=0,1 UZ=-5.137,-5.468
ADD=43 RD=0,1 UZ=-5.468,-5.958
ADD=44 RD=0,1 UZ=-5.958,-6.615
ADD=45 RD=0,1 UZ=-6.615,-6.928

ADD=46 RD=0,1 UZ=-6.928,-7.189
ADD=47 RD=0,1 UZ=-7.189,-7.58
ADD=48 RD=0,1 UZ=-7.58,-7.986

NAME=PHW

TYPE=DISTRIBUTED SPAN

ADD=1 RD=0,1 UX=5.018,4.724
ADD=2 RD=0,1 UX=4.724,4.43
ADD=3 RD=0,1 UX=4.43,4.136
ADD=4 RD=0,1 UX=4.136,3.944
ADD=5 RD=0,1 UX=3.944,3.75
ADD=6 RD=0,1 UX=3.75,3.562
ADD=7 RD=0,1 UX=3.562,3.437
ADD=8 RD=0,1 UX=3.437,3.287
ADD=9 RD=0,1 UX=3.287,2.971
ADD=10 RD=0,1 UX=2.971,2.736
ADD=11 RD=0,1 UX=2.736,2.578
ADD=12 RD=0,1 UX=2.578,2.488
ADD=13 RD=0,1 UX=2.488,2.463
ADD=14 RD=0,1 UX=-2.463,-2.488
ADD=15 RD=0,1 UX=-2.488,-2.578
ADD=16 RD=0,1 UX=-2.578,-2.736
ADD=17 RD=0,1 UX=-2.736,-2.971
ADD=18 RD=0,1 UX=-2.971,-3.287
ADD=19 RD=0,1 UX=-3.287,-3.437
ADD=20 RD=0,1 UX=-3.437,-3.562
ADD=21 RD=0,1 UX=-3.562,-3.75
ADD=22 RD=0,1 UX=-3.75,-3.944
ADD=23 RD=0,1 UX=-3.944,-4.136
ADD=24 RD=0,1 UX=-4.136,-4.43
ADD=25 RD=0,1 UX=-4.43,-4.724
ADD=26 RD=0,1 UX=-4.724,-5.018
ADD=102 RD=0,1 UX=5.956,5.636
ADD=302 RD=0,1 UX=-6.035,-6.344
ADD=101 RD=0,1 UX=5.636,5.018
ADD=301 RD=0,1 UX=-5.018,-6.035

NAME=PW

TYPE=DISTRIBUTED SPAN

ADD=1 RD=0,1 U2=-6.929,-6.276
ADD=2 RD=0,1 U2=-6.276,-5.622
ADD=3 RD=0,1 U2=-5.622,-4.969
ADD=4 RD=0,1 U2=-4.969,-4.543
ADD=5 RD=0,1 U2=-4.543,-4.11
ADD=6 RD=0,1 U2=-4.11,-3.694
ADD=7 RD=0,1 U2=-3.694,-3.415
ADD=8 RD=0,1 U2=-3.415,-3.082
ADD=9 RD=0,1 U2=-3.082,-2.381
ADD=10 RD=0,1 U2=-2.381,-1.858
ADD=11 RD=0,1 U2=-1.858,-1.506
ADD=12 RD=0,1 U2=-1.506,-1.307
ADD=13 RD=0,1 U2=-1.307,-1.25
ADD=14 RD=0,1 U2=-1.25,-1.307
ADD=15 RD=0,1 U2=-1.307,-1.506
ADD=16 RD=0,1 U2=-1.506,-1.858
ADD=17 RD=0,1 U2=-1.858,-2.381
ADD=18 RD=0,1 U2=-2.381,-3.082
ADD=19 RD=0,1 U2=-3.082,-3.415
ADD=20 RD=0,1 U2=-3.415,-3.694
ADD=33 RD=0,1 U2=-3.694,-3.415
ADD=34 RD=0,1 U2=-3.415,-3.082
ADD=35 RD=0,1 U2=-3.082,-2.381
ADD=36 RD=0,1 U2=-2.381,-1.858
ADD=37 RD=0,1 U2=-1.858,-1.506
ADD=38 RD=0,1 U2=-1.506,-1.307
ADD=39 RD=0,1 U2=-1.307,-1.25

ADD=40 RD=0,1 U2=-1.25,-1.307
ADD=41 RD=0,1 U2=-1.307,-1.506
ADD=42 RD=0,1 U2=-1.506,-3.5628
ADD=43 RD=0,1 U2=-3.5628,-2.381
ADD=44 RD=0,1 U2=-2.381,-3.082
ADD=45 RD=0,1 U2=-3.082,-3.415
ADD=46 RD=0,1 U2=-3.415,-3.694
ADD=47 RD=0,1 U2=-3.694,-4.11
ADD=48 RD=0,1 U2=-4.11,-4.543
ADD=49 RD=0,1 U2=-4.543,-4.969
ADD=50 RD=0,1 U2=-4.969,-5.622
ADD=52 RD=0,1 U2=-5.622,-6.276
ADD=53 RD=0,1 U2=-6.276,-6.929
ADD=102 RD=0,1 U2=-9.014,-8.302
ADD=101 RD=0,1 U2=-8.302,-6.929
ADD=302 RD=0,1 U2=-9.188,-9.875
ADD=301 RD=0,1 U2=-6.929,-9.188
ADD=400 RD=0,1 UZ=9.714,9.714
ADD=401 RD=0,1 UZ=9.714,9.727
ADD=402 RD=0,1 UZ=9.727,9.754
ADD=403 RD=0,1 UZ=9.754,9.78
ADD=404 RD=0,1 UZ=9.78,9.807
ADD=405 RD=0,1 UZ=9.807,9.833
ADD=406 RD=0,1 UZ=9.833,9.86
ADD=407 RD=0,1 UZ=9.86,9.886
ADD=408 RD=0,1 UZ=9.886,9.913
ADD=409 RD=0,1 UZ=9.913,9.939
ADD=410 RD=0,1 UZ=9.939,9.966
ADD=411 RD=0,1 UZ=9.966,9.992
ADD=412 RD=0,1 UZ=9.992,10.019
ADD=413 RD=0,1 UZ=10.019,10.048
ADD=414 RD=0,1 UZ=10.048,10.072
ADD=415 RD=0,1 UZ=10.072,10.098
ADD=416 RD=0,1 UZ=10.098,10.125
ADD=417 RD=0,1 UZ=10.125,10.144
ADD=418 RD=0,1 UZ=10.144,10.164
ADD=419 RD=0,1 UZ=10.164,10.191
ADD=420 RD=0,1 UZ=10.191,10.217
ADD=421 RD=0,1 UZ=10.217,10.241
ADD=422 RD=0,1 UZ=10.241,10.27
ADD=423 RD=0,1 UZ=10.27,10.297
ADD=424 RD=0,1 UZ=10.297,10.323
ADD=425 RD=0,1 UZ=10.323,10.35
ADD=426 RD=0,1 UZ=10.35,10.376
ADD=427 RD=0,1 UZ=10.376,10.403
ADD=428 RD=0,1 UZ=10.403,10.429
ADD=429 RD=0,1 UZ=10.429,10.456
ADD=430 RD=0,1 UZ=10.456,10.482
ADD=431 RD=0,1 UZ=10.482,10.509
ADD=432 RD=0,1 UZ=10.509,10.535
ADD=433 RD=0,1 UZ=10.535,10.562
ADD=434 RD=0,1 UZ=10.562,10.575
ADD=435 RD=0,1 UZ=10.575,10.575

NAME=PL

TYPE=CONCENTRATED SPAN

ADD=415 RD=.755 UZ=-9.6
ADD=413 RD=.717 UZ=-9.6
ADD=412 RD=.415 UZ=-9.6
ADD=410 RD=.321 UZ=-9.6
ADD=408 RD=.962 UZ=-9.6
ADD=406 RD=.925 UZ=-9.6
ADD=420 RD=.245 UZ=-9.6
ADD=422 RD=.283 UZ=-9.6
ADD=423 RD=.642 UZ=-9.6
ADD=425 RD=.679 UZ=-9.6
ADD=427 RD=.038 UZ=-9.6
ADD=429 RD=.076 UZ=-9.6

NAME=PVL

TYPE=DISTRIBUTED SPAN

ADD=5 RD=0,1 UZ=-1.186,-1.186
ADD=6 RD=0,1 UZ=-1.186,-1.186
ADD=7 RD=0,1 UZ=-1.186,-1.186
ADD=8 RD=0,1 UZ=-1.186,-1.186
ADD=9 RD=0,1 UZ=-1.186,-1.186
ADD=10 RD=0,1 UZ=-1.186,-1.186
ADD=11 RD=0,1 UZ=-1.186,-1.186
ADD=12 RD=0,1 UZ=-1.186,-1.186
ADD=13 RD=0,1 UZ=-1.186,-1.186
ADD=14 RD=0,1 UZ=-1.186,-1.186
ADD=15 RD=0,1 UZ=-1.186,-1.186
ADD=16 RD=0,1 UZ=-1.186,-1.186
ADD=17 RD=0,1 UZ=-1.186,-1.186
ADD=18 RD=0,1 UZ=-1.186,-1.186
ADD=19 RD=0,1 UZ=-1.186,-1.186
ADD=20 RD=0,1 UZ=-1.186,-1.186
ADD=21 RD=0,1 UZ=-1.186,-1.186
ADD=22 RD=0,1 UZ=-1.186,-1.186
ADD=31 RD=0,1 UZ=-1.186,-1.186
ADD=32 RD=0,1 UZ=-1.186,-1.186
ADD=33 RD=0,1 UZ=-1.186,-1.186

ADD=34 RD=0,1 UZ=-1.186,-1.186
ADD=35 RD=0,1 UZ=-1.186,-1.186
ADD=36 RD=0,1 UZ=-1.186,-1.186
ADD=37 RD=0,1 UZ=-1.186,-1.186
ADD=38 RD=0,1 UZ=-1.186,-1.186
ADD=39 RD=0,1 UZ=-1.186,-1.186
ADD=40 RD=0,1 UZ=-1.186,-1.186
ADD=41 RD=0,1 UZ=-1.186,-1.186
ADD=42 RD=0,1 UZ=-1.186,-1.186
ADD=43 RD=0,1 UZ=-1.186,-1.186
ADD=44 RD=0,1 UZ=-1.186,-1.186
ADD=45 RD=0,1 UZ=-1.186,-1.186
ADD=46 RD=0,1 UZ=-1.186,-1.186
ADD=47 RD=0,1 UZ=-1.186,-1.186
ADD=48 RD=0,1 UZ=-1.186,-1.186

COMBO

NAME=COMB1

LOAD=SW SF=1.3
LOAD=PV SF=1.5
LOAD=PH SF=1.7

NAME=COMB2

LOAD=SW SF=1.3
LOAD=PV SF=1.5
LOAD=PH SF=.65

NAME=COMB3

LOAD=SW SF=1.3
LOAD=PVW SF=1.5
LOAD=PHW SF=1.7
LOAD=PW SF=1.3

NAME=COMB4

LOAD=SW SF=1.3
LOAD=PVW SF=1.5
LOAD=PHW SF=.65
LOAD=PW SF=1.3

NAME=COMB5

LOAD=SW SF=1.3
LOAD=PV SF=1.5
LOAD=PH SF=1.7
LOAD=PVL SF=1.3

NAME=COMB6

LOAD=SW SF=1.3
LOAD=PV SF=1.5
LOAD=PH SF=.65
LOAD=PVL SF=1.3

NAME=COMB7

LOAD=SW SF=1
LOAD=PV SF=1
LOAD=PH SF=1

NAME=COMB8

LOAD=SW SF=1
LOAD=PV SF=1
LOAD=PH SF=1
LOAD=PL SF=1

NAME=COMB9

LOAD=SW SF=1
LOAD=PV SF=1
LOAD=PH SF=.5

NAME=COMB10

LOAD=SW SF=1
LOAD=PV SF=1
LOAD=PH SF=.5
LOAD=PL SF=1

NAME=COMB11

LOAD=SW SF=1
LOAD=PVW SF=1
LOAD=PHW SF=1

NAME=COMB12

LOAD=SW SF=1
LOAD=PVW SF=1
LOAD=PHW SF=1
LOAD=PL SF=1

OUTPUT

; No Output Requested

END

; The following data is used for graphics, design and pushover analysis.

; If changes are made to the analysis data above, then the following data should be checked for consistency.

SAP2000 V7.10 SUPPLEMENTAL DATA

GRID GLOBAL X "1" -15.25
GRID GLOBAL Y "2" 0
GRID GLOBAL Z "3" -8.625
GRID GLOBAL X "4" 0
GRID GLOBAL Z "5" 0
GRID GLOBAL X "6" 15.25

MATERIAL STEEL FY 25310.51
MATERIAL CONC FYREBAR 40000 FYSHEAR 28122.79 FC
4000 FCSHEAR 2812.279
MATERIAL RIGID FYREBAR 40000 FYSHEAR 28122.79
FC 4000 FCSHEAR 2812.279
MATERIAL CONCL FYREBAR 40000 FYSHEAR 28122.79
FC 4000 FCSHEAR 2812.279
CONCRETESECTION T1 COLUMN COVER .05 REBAR
RR-3-3
CONCRETESECTION T2 COLUMN COVER .0542 REBAR
RR-3-3
CONCRETESECTION T3 COLUMN COVER .0675 REBAR
RR-3-3
CONCRETESECTION T4 COLUMN COVER .0916 REBAR
RR-3-3
CONCRETESECTION T5 COLUMN COVER .068 REBAR
RR-3-3
CONCRETESECTION T6 COLUMN COVER .0553 REBAR
RR-3-3
CONCRETESECTION T7 COLUMN COVER .0511 REBAR
RR-3-3
CONCRETESECTION T8 COLUMN COVER .05 REBAR
RR-3-3
CONCRETESECTION FOOT COLUMN COVER .14 REBAR
RR-3-3
CONCRETESECTION WALL COLUMN COVER .085 REBAR
RR-3-3
CONCRETESECTION RIGID COLUMN COVER 1 REBAR
RR-3-3
CONCRETESECTION WALL1 COLUMN COVER .13 REBAR
RR-3-3
STATICLOAD SW TYPE DEAD
STATICLOAD PV TYPE DEAD
STATICLOAD PH TYPE DEAD
STATICLOAD PVW TYPE DEAD
STATICLOAD PHW TYPE DEAD
STATICLOAD PW TYPE DEAD
STATICLOAD PL TYPE DEAD
STATICLOAD PVL TYPE DEAD
END SUPPLEMENTAL DATA

SYSTEM

DOF=UX,UZ,RY LENGTH=m FORCE=Ton LINES=59

JOINT

1 X=-14.25 Y=0 Z=-5.679
2 X=-14.25 Y=0 Z=-5.026
3 X=-14.25 Y=0 Z=-4.372
4 X=-14.25 Y=0 Z=-3.719
5 X=-14.23 Y=0 Z=-3.293
6 X=-14.166 Y=0 Z=-2.86
7 X=-14.107 Y=0 Z=-2.444
8 X=-13.748 Y=0 Z=-2.165
9 X=-13.294 Y=0 Z=-1.832
10 X=-12.092 Y=0 Z=-1.131
11 X=-10.887 Y=0 Z=-.608
12 X=-9.683 Y=0 Z=-.256
13 X=-8.479 Y=0 Z=-.057
14 X=-7.275 Y=0 Z=0
15 X=-6.071 Y=0 Z=-.057
16 X=-4.867 Y=0 Z=-.256
17 X=-3.663 Y=0 Z=-.608
18 X=-2.458 Y=0 Z=-1.131
19 X=-1.256 Y=0 Z=-1.832
20 X=-.795 Y=0 Z=-2.165
21 X=-.443 Y=0 Z=-2.444
22 X=-.369 Y=0 Z=-2.86
23 X=-.318 Y=0 Z=-3.293
24 X=-.3 Y=0 Z=-3.719
25 X=-.3 Y=0 Z=-4.372
26 X=-.3 Y=0 Z=-5.026
27 X=-.3 Y=0 Z=-5.679
28 X=.3 Y=0 Z=-5.679
29 X=.3 Y=0 Z=-5.026
30 X=.3 Y=0 Z=-4.372
31 X=.3 Y=0 Z=-3.719
32 X=.318 Y=0 Z=-3.293
33 X=.369 Y=0 Z=-2.86
34 X=.443 Y=0 Z=-2.444
35 X=.795 Y=0 Z=-2.165
36 X=1.256 Y=0 Z=-1.832
37 X=2.458 Y=0 Z=-1.131
38 X=3.663 Y=0 Z=-.608
39 X=4.867 Y=0 Z=-.256
40 X=6.071 Y=0 Z=-.057
41 X=7.275 Y=0 Z=0
42 X=8.479 Y=0 Z=-.057
43 X=9.683 Y=0 Z=-.256
44 X=10.887 Y=0 Z=-.608

45 X=12.092 Y=0 Z=-1.131
 46 X=13.294 Y=0 Z=-1.832
 47 X=13.748 Y=0 Z=-2.165
 48 X=14.107 Y=0 Z=-2.444
 49 X=14.166 Y=0 Z=-2.86
 50 X=14.23 Y=0 Z=-3.293
 51 X=14.25 Y=0 Z=-3.719
 52 X=14.25 Y=0 Z=-4.372
 53 X=14.25 Y=0 Z=-5.026
 54 X=14.25 Y=0 Z=-5.679
 101 X=-14.325 Y=0 Z=-5.679
 102 X=-14.325 Y=0 Z=-7.052
 201 X=0 Y=0 Z=-5.679
 202 X=0 Y=0 Z=-7.475
 301 X=14.325 Y=0 Z=-5.679
 302 X=14.325 Y=0 Z=-7.938
 401 X=-15.25 Y=0 Z=-7.764
 402 X=-14.325 Y=0 Z=-7.764
 403 X=-13.9 Y=0 Z=-7.777
 404 X=-13.017 Y=0 Z=-7.804
 405 X=-12.133 Y=0 Z=-7.83
 406 X=-11.25 Y=0 Z=-7.857
 407 X=-10.367 Y=0 Z=-7.883
 408 X=-9.484 Y=0 Z=-7.91
 409 X=-8.6 Y=0 Z=-7.936
 410 X=-7.717 Y=0 Z=-7.963
 411 X=-6.834 Y=0 Z=-7.989
 412 X=-5.95 Y=0 Z=-8.016
 413 X=-5.067 Y=0 Z=-8.042
 414 X=-4.184 Y=0 Z=-8.069
 415 X=-3.3 Y=0 Z=-8.098
 416 X=-2.417 Y=0 Z=-8.122
 417 X=-1.534 Y=0 Z=-8.148
 418 X=-.65 Y=0 Z=-8.175
 419 X=0 Y=0 Z=-8.194
 420 X=.65 Y=0 Z=-8.214
 421 X=1.534 Y=0 Z=-8.241
 422 X=2.417 Y=0 Z=-8.267
 423 X=3.3 Y=0 Z=-8.291
 424 X=4.184 Y=0 Z=-8.32
 425 X=5.067 Y=0 Z=-8.347
 426 X=5.95 Y=0 Z=-8.373
 427 X=6.834 Y=0 Z=-8.4
 428 X=7.717 Y=0 Z=-8.426
 429 X=8.6 Y=0 Z=-8.453
 430 X=9.484 Y=0 Z=-8.479
 431 X=10.367 Y=0 Z=-8.506
 432 X=11.25 Y=0 Z=-8.532
 433 X=12.133 Y=0 Z=-8.559
 434 X=13.017 Y=0 Z=-8.585

435 X=13.9 Y=0 Z=-8.612
436 X=14.325 Y=0 Z=-8.625
437 X=15.25 Y=0 Z=-8.625

PATTERN

NAME=TEMP

NAME=PRES

SPRING

ADD=401 U3=201064.2
ADD=402 U3=293445
ADD=403 U3=284315.6
ADD=404 U3=384087
ADD=405 U3=384087
ADD=406 U3=383869.6
ADD=407 U3=383869.6
ADD=408 U3=384087
ADD=409 U3=384087
ADD=410 U3=383869.6
ADD=411 U3=384087
ADD=412 U3=384087
ADD=413 U3=383869.6
ADD=414 U3=384087
ADD=415 U3=384087
ADD=416 U3=383869.6
ADD=417 U3=384087
ADD=418 U3=333440.5
ADD=419 U1=10000 U3=282576.7
ADD=420 U3=333440.5
ADD=421 U3=384087
ADD=422 U3=383869.6
ADD=423 U3=384087
ADD=424 U3=384087
ADD=425 U3=383869.6
ADD=426 U3=384087
ADD=427 U3=384087
ADD=428 U3=383869.6
ADD=429 U3=384087
ADD=430 U3=384087
ADD=431 U3=383869.6
ADD=432 U3=383869.6
ADD=433 U3=384087
ADD=434 U3=384087
ADD=435 U3=284315.6
ADD=436 U3=293445
ADD=437 U3=201064.2

MATERIAL

NAME=CONC IDES=C M=.2448 W=2.5

T=0 E=2800000 U=.2 A=.00001

NAME=STEEL IDES=S

T=0 E=2E+10 U=.3 A=.0000117 FY=25310.51

NAME=RIGID IDES=C

T=0 E=2464750 U=.3 A=.00001

NAME=CONC1 IDES=C M=.2448 W=2.5

T=0 E=2464750 U=.2 A=.00001

FRAME SECTION

NAME=T1 MAT=CONC SH=R T=.5,1 A=.5 J=2.861003E-02 I=1.041667E-02,4.897667E-02
AS=.4166667,.4166667

NAME=T2 MAT=CONC SH=R T=.542,1 A=.542 J=3.508126E-02 I=1.326834E-02,4.516667E-02
AS=.4516667,.4516667

NAME=T3 MAT=CONC SH=R T=.675,1 A=.675 J=5.967503E-02 I=2.562891E-02,.05625 AS=.5625,.5625

NAME=T4 MAT=CONC SH=R T=.916,1 A=.916 J=.1170223 I=6.404794E-02,7.633334E-02
AS=.7633333,.7633333

NAME=T5 MAT=CONC SH=R T=.68,1 A=.68 J=6.070982E-02 I=2.620267E-02,5.666667E-02
AS=.5666667,.5666667

NAME=T6 MAT=CONC SH=R T=.553,1 A=.553 J=3.688483E-02 I=.0140927,4.608333E-02
AS=.4608333,.4608333

NAME=T7 MAT=CONC SH=R T=.511,1 A=.511 J=3.024029E-02 I=.0111194,4.258334E-02
AS=.4258333,.4258333

NAME=T8 MAT=CONC SH=R T=.5,1 A=.5 J=2.861003E-02 I=1.041667E-02,4.897667E-02
AS=.4166667,.4166667

NAME=FOOT MAT=CONC1 SH=R T=1.4,1 A=1.4 J=.2612221 I=.2286666,.1166667 AS=1.166667,1.166667

NAME=WALL MAT=CONC1 SH=R T=.85,1 A=.85 J=9.985562E-02 I=4.117709E-02,7.083333E-02
AS=.7083334,.7083334

NAME=RIGID MAT=RIGID SH=R T=10,10 A=100 J=1408.333 I=833.5623,833.5623 AS=83.56233,83.56233

NAME=WALL1 MAT=CONC1 SH=R T=1.3,1 A=1.3 J=.2294606 I=.1830833,.1083333 AS=1.083333,1.083333

NAME=VAR1 TYPE=NONPR

SEC=T1,T2 EIVAR=1,1 L=.426

NAME=VAR2 TYPE=NONPR

SEC=T2,T3 EIVAR=1,1 L=.436

NAME=VAR3 TYPE=NONPR

SEC=T3,T4 EIVAR=1,1 L=.422

NAME=VAR4 TYPE=NONPR

SEC=T4,T5 EIVAR=1,1 L=.455

NAME=VAR5 TYPE=NONPR

SEC=T5,T6 EIVAR=1,1 L=.563

NAME=VAR6 TYPE=NONPR

SEC=T6,T7 EIVAR=1,1 L=1.392

NAME=VAR7 TYPE=NONPR

SEC=T7,T8 EIVAR=1,1 L=1.313

FRAME

1 J=1,2 SEC=T1 NSEG=1 ANG=180 IREL=R3

2 J=2,3 SEC=T1 NSEG=1 ANG=180

3 J=3,4 SEC=T1 NSEG=1 ANG=180

4 J=4,5 SEC=VAR1 NSEG=1 ANG=0

5 J=5,6 SEC=VAR2 NSEG=1 ANG=0

6 J=6,7 SEC=VAR3 NSEG=1 ANG=0

7 J=7,8 SEC=VAR4 NSEG=1 ANG=0
 8 J=8,9 SEC=VAR5 NSEG=1 ANG=0
 9 J=9,10 SEC=VAR6 NSEG=1 ANG=0
 10 J=10,11 SEC=VAR7 NSEG=1 ANG=0
 11 J=11,12 SEC=T8 NSEG=1 ANG=0
 12 J=12,13 SEC=T8 NSEG=1 ANG=0
 13 J=13,14 SEC=T8 NSEG=1 ANG=0
 14 J=14,15 SEC=T8 NSEG=1 ANG=0
 15 J=15,16 SEC=T8 NSEG=1 ANG=0
 16 J=16,17 SEC=T8 NSEG=1 ANG=0
 17 J=17,18 SEC=VAR7 NSEG=1 ANG=0
 18 J=18,19 SEC=VAR6 NSEG=1 ANG=0
 19 J=19,20 SEC=VAR5 NSEG=1 ANG=0
 20 J=20,21 SEC=VAR4 NSEG=1 ANG=0
 21 J=21,22 SEC=VAR3 NSEG=1 ANG=0
 22 J=22,23 SEC=VAR2 NSEG=1 ANG=0
 23 J=23,24 SEC=VAR1 NSEG=1 ANG=0
 24 J=24,25 SEC=T1 NSEG=1 ANG=0
 25 J=25,26 SEC=T1 NSEG=1 ANG=0
 26 J=26,27 SEC=T1 NSEG=1 ANG=0 JREL=R3
 27 J=28,29 SEC=T1 NSEG=1 ANG=180 IREL=R3
 28 J=29,30 SEC=T1 NSEG=1 ANG=180
 29 J=30,31 SEC=T1 NSEG=1 ANG=180
 30 J=31,32 SEC=VAR1 NSEG=1 ANG=0
 31 J=32,33 SEC=VAR2 NSEG=1 ANG=0
 32 J=33,34 SEC=VAR3 NSEG=1 ANG=0
 33 J=34,35 SEC=VAR4 NSEG=1 ANG=0
 34 J=35,36 SEC=VAR5 NSEG=1 ANG=0
 35 J=36,37 SEC=VAR6 NSEG=1 ANG=0
 36 J=37,38 SEC=VAR7 NSEG=1 ANG=0
 37 J=38,39 SEC=T8 NSEG=1 ANG=0
 38 J=39,40 SEC=T8 NSEG=1 ANG=0
 39 J=40,41 SEC=T8 NSEG=1 ANG=0
 40 J=41,42 SEC=T8 NSEG=1 ANG=0
 41 J=42,43 SEC=T8 NSEG=1 ANG=0
 42 J=43,44 SEC=T8 NSEG=1 ANG=0
 43 J=44,45 SEC=VAR7 NSEG=1 ANG=0
 44 J=45,46 SEC=VAR6 NSEG=1 ANG=0
 45 J=46,47 SEC=VAR5 NSEG=1 ANG=0
 46 J=47,48 SEC=VAR4 NSEG=1 ANG=0
 47 J=48,49 SEC=VAR3 NSEG=1 ANG=0
 48 J=49,50 SEC=VAR2 NSEG=1 ANG=0
 49 J=50,51 SEC=VAR1 NSEG=1 ANG=0
 50 J=51,52 SEC=T1 NSEG=1 ANG=0
 52 J=52,53 SEC=T1 NSEG=1 ANG=0
 53 J=53,54 SEC=T1 NSEG=1 ANG=0 JREL=R3
 85 J=28,201 SEC=RIGID NSEG=1 ANG=0
 86 J=201,27 SEC=RIGID NSEG=1 ANG=0
 87 J=301,54 SEC=RIGID NSEG=1 ANG=0
 88 J=1,101 SEC=RIGID NSEG=1 ANG=0

101 J=102,101 SEC=WALL NSEG=1 ANG=180
 102 J=402,102 SEC=WALL NSEG=1 ANG=180 IOFF=.02475 RIGID=0
 201 J=202,201 SEC=WALL1 NSEG=1 ANG=0
 202 J=419,202 SEC=WALL1 NSEG=1 ANG=0 IOFF=.375 RIGID=0
 301 J=301,302 SEC=WALL NSEG=1 ANG=0
 302 J=302,436 SEC=WALL NSEG=1 ANG=0 JOFF=.4875 RIGID=0
 400 J=401,402 SEC=FOOT NSEG=1 ANG=0
 401 J=402,403 SEC=FOOT NSEG=1 ANG=0 IOFF=.075 RIGID=0
 402 J=403,404 SEC=FOOT NSEG=1 ANG=0
 403 J=404,405 SEC=FOOT NSEG=1 ANG=0
 404 J=405,406 SEC=FOOT NSEG=1 ANG=0
 405 J=406,407 SEC=FOOT NSEG=1 ANG=0
 406 J=407,408 SEC=FOOT NSEG=1 ANG=0
 407 J=408,409 SEC=FOOT NSEG=1 ANG=0
 408 J=409,410 SEC=FOOT NSEG=1 ANG=0
 409 J=410,411 SEC=FOOT NSEG=1 ANG=0
 410 J=411,412 SEC=FOOT NSEG=1 ANG=0
 411 J=412,413 SEC=FOOT NSEG=1 ANG=0
 412 J=413,414 SEC=FOOT NSEG=1 ANG=0
 413 J=414,415 SEC=FOOT NSEG=1 ANG=0
 414 J=415,416 SEC=FOOT NSEG=1 ANG=0
 415 J=416,417 SEC=FOOT NSEG=1 ANG=0
 416 J=417,418 SEC=FOOT NSEG=1 ANG=0
 417 J=418,419 SEC=FOOT NSEG=1 ANG=0 JOFF=.3 RIGID=0
 418 J=419,420 SEC=FOOT NSEG=1 ANG=0 IOFF=.3 RIGID=0
 419 J=420,421 SEC=FOOT NSEG=1 ANG=0
 420 J=421,422 SEC=FOOT NSEG=1 ANG=0
 421 J=422,423 SEC=FOOT NSEG=1 ANG=0
 422 J=423,424 SEC=FOOT NSEG=1 ANG=0
 423 J=424,425 SEC=FOOT NSEG=1 ANG=0
 424 J=425,426 SEC=FOOT NSEG=1 ANG=0
 425 J=426,427 SEC=FOOT NSEG=1 ANG=0
 426 J=427,428 SEC=FOOT NSEG=1 ANG=0
 427 J=428,429 SEC=FOOT NSEG=1 ANG=0
 428 J=429,430 SEC=FOOT NSEG=1 ANG=0
 429 J=430,431 SEC=FOOT NSEG=1 ANG=0
 430 J=431,432 SEC=FOOT NSEG=1 ANG=0
 431 J=432,433 SEC=FOOT NSEG=1 ANG=0
 432 J=433,434 SEC=FOOT NSEG=1 ANG=0
 433 J=434,435 SEC=FOOT NSEG=1 ANG=0
 434 J=435,436 SEC=FOOT NSEG=1 ANG=0 JOFF=.075 RIGID=0
 435 J=436,437 SEC=FOOT NSEG=1 ANG=0

LOAD

NAME=SW SW=1

NAME=PH

TYPE=DISTRIBUTED SPAN

ADD=1 RD=0,1 UX=3.07,2.45

ADD=2 RD=0,1 UX=2.45,1.83

ADD=3 RD=0,1 UX=1.83,1.21

ADD=4 RD=0,1 UX=1.21,.81
 ADD=5 RD=0,1 UX=.81,.4
 ADD=6 RD=0,1 UX=.4,0
 ADD=53 RD=0,1 UX=-2.45,-3.07
 ADD=52 RD=0,1 UX=-1.83,-2.45
 ADD=50 RD=0,1 UX=-1.21,-1.83
 ADD=49 RD=0,1 UX=-.81,-1.21
 ADD=48 RD=0,1 UX=-.4,-.81
 ADD=47 RD=0,1 UX=0,-.4
 ADD=102 RD=0,1 UX=5.05,4.38
 ADD=101 RD=0,1 UX=4.38,3.07
 ADD=302 RD=0,1 UX=-5.22,-5.87
 ADD=301 RD=0,1 UX=-3.07,-5.22

NAME=PVL

TYPE=DISTRIBUTED SPAN

ADD=1 RD=0,1 UX=.5,.5
 ADD=2 RD=0,1 UX=.5,.5
 ADD=3 RD=0,1 UX=.5,.5
 ADD=4 RD=0,1 UX=.5,.5
 ADD=5 RD=0,1 UX=.5,.5
 ADD=6 RD=0,1 UX=.5,.5
 ADD=88 RD=0,1 UX=.5,.5
 ADD=101 RD=0,1 UX=.5,.5
 ADD=102 RD=0,1 UX=.5,.5
 ADD=47 RD=0,1 UX=-.5,-.5
 ADD=48 RD=0,1 UX=-.5,-.5
 ADD=49 RD=0,1 UX=-.5,-.5
 ADD=50 RD=0,1 UX=-.5,-.5
 ADD=52 RD=0,1 UX=-.5,-.5
 ADD=53 RD=0,1 UX=-.5,-.5
 ADD=87 RD=0,1 UX=-.5,-.5
 ADD=301 RD=0,1 UX=-.5,-.5
 ADD=302 RD=0,1 UX=-.5,-.5

COMBO

NAME=COMB1

LOAD=SW SF=1.3
 LOAD=PH SF=1.7
 LOAD=PVL SF=1.3

NAME=COMB2

LOAD=SW SF=1.3
 LOAD=PH SF=.65
 LOAD=PVL SF=1.3

NAME=COMB3

LOAD=SW SF=1
 LOAD=PH SF=1
 LOAD=PVL SF=1

NAME=COMB4

LOAD=SW SF=1
 LOAD=PH SF=.5

LOAD=PVL SF=1
NAME=COMB5 TYPE=ENVE
COMB=COMB1 SF=1
COMB=COMB2 SF=1
NAME=COMB6 TYPE=ENVE
COMB=COMB3 SF=1
COMB=COMB4 SF=1

OUTPUT

; No Output Requested

END

; The following data is used for graphics, design and pushover analysis.
; If changes are made to the analysis data above, then the following data
; should be checked for consistency.

SAP2000 V7.10 SUPPLEMENTAL DATA

GRID GLOBAL X "1" -15.25
GRID GLOBAL Y "2" 0
GRID GLOBAL Z "3" -8.625
GRID GLOBAL X "4" 0
GRID GLOBAL Z "5" 0
GRID GLOBAL X "6" 15.25
MATERIAL STEEL FY 25310.51
MATERIAL CONC FYREBAR 40000 FYSHEAR 28122.79 FC 4000 FCSHEAR 2812.279
MATERIAL RIGID FYREBAR 40000 FYSHEAR 28122.79 FC 4000 FCSHEAR 2812.279
MATERIAL CONC1 FYREBAR 40000 FYSHEAR 28122.79 FC 4000 FCSHEAR 2812.279
CONCRETESECTION T1 COLUMN COVER .05 REBAR RR-3-3
CONCRETESECTION T2 COLUMN COVER .0542 REBAR RR-3-3
CONCRETESECTION T3 COLUMN COVER .0675 REBAR RR-3-3
CONCRETESECTION T4 COLUMN COVER .0916 REBAR RR-3-3
CONCRETESECTION T5 COLUMN COVER .068 REBAR RR-3-3
CONCRETESECTION T6 COLUMN COVER .0553 REBAR RR-3-3
CONCRETESECTION T7 COLUMN COVER .0511 REBAR RR-3-3
CONCRETESECTION T8 COLUMN COVER .05 REBAR RR-3-3
CONCRETESECTION FOOT COLUMN COVER .14 REBAR RR-3-3
CONCRETESECTION WALL COLUMN COVER .085 REBAR RR-3-3
CONCRETESECTION RIGID COLUMN COVER 1 REBAR RR-3-3
CONCRETESECTION WALL1 COLUMN COVER .13 REBAR RR-3-3
STATICLOAD SW TYPE DEAD
STATICLOAD PH TYPE DEAD
STATICLOAD PVL TYPE DEAD
END SUPPLEMENTAL DATA

4. SAP2000 INPUT DATA 첨부

CASE1	활하중영향검토토1.\$2K
CASE2	활하중영향검토토2.\$2K
CASE3	활하중영향검토토3.\$2K

; File D:\W\SAP2000\DATA\W개착식터널\W활하중영향검토토1.\$2k saved 11-25-02 13:32:32 in Ton-m

SYSTEM

DOF=UX,UZ,RY LENGTH=m FORCE=Ton LINES=59

JOINT

```

1 X=-14.25 Y=0 Z=-5.679
2 X=-14.25 Y=0 Z=-5.026
3 X=-14.25 Y=0 Z=-4.372
4 X=-14.25 Y=0 Z=-3.719
5 X=-14.23 Y=0 Z=-3.293
6 X=-14.166 Y=0 Z=-2.86
7 X=-14.107 Y=0 Z=-2.444
8 X=-13.748 Y=0 Z=-2.165
9 X=-13.294 Y=0 Z=-1.832
10 X=-12.092 Y=0 Z=-1.131
11 X=-10.887 Y=0 Z=-.608
12 X=-9.683 Y=0 Z=-.256
13 X=-8.479 Y=0 Z=-.057
14 X=-7.275 Y=0 Z=0
15 X=-6.071 Y=0 Z=-.057
16 X=-4.867 Y=0 Z=-.256
17 X=-3.663 Y=0 Z=-.608
18 X=-2.458 Y=0 Z=-1.131
19 X=-1.256 Y=0 Z=-1.832
20 X=-.795 Y=0 Z=-2.165
21 X=-.443 Y=0 Z=-2.444
22 X=-.369 Y=0 Z=-2.86
23 X=-.318 Y=0 Z=-3.293
24 X=-.3 Y=0 Z=-3.719
25 X=-.3 Y=0 Z=-4.372
26 X=-.3 Y=0 Z=-5.026
27 X=-.3 Y=0 Z=-5.679
28 X=.3 Y=0 Z=-5.679
29 X=.3 Y=0 Z=-5.026
30 X=.3 Y=0 Z=-4.372
31 X=.3 Y=0 Z=-3.719
32 X=.318 Y=0 Z=-3.293
33 X=.369 Y=0 Z=-2.86
34 X=.443 Y=0 Z=-2.444
35 X=.795 Y=0 Z=-2.165
36 X=1.256 Y=0 Z=-1.832

```

37 X=2.458 Y=0 Z=-1.131

38 X=3.663 Y=0 Z=-.608
 39 X=4.867 Y=0 Z=-.256
 40 X=6.071 Y=0 Z=-.057
 41 X=7.275 Y=0 Z=0
 42 X=8.479 Y=0 Z=-.057
 43 X=9.683 Y=0 Z=-.256
 44 X=10.887 Y=0 Z=-.608
 45 X=12.092 Y=0 Z=-1.131
 46 X=13.294 Y=0 Z=-1.832
 47 X=13.748 Y=0 Z=-2.165
 48 X=14.107 Y=0 Z=-2.444
 49 X=14.166 Y=0 Z=-2.86
 50 X=14.23 Y=0 Z=-3.293
 51 X=14.25 Y=0 Z=-3.719
 52 X=14.25 Y=0 Z=-4.372
 53 X=14.25 Y=0 Z=-5.026
 54 X=14.25 Y=0 Z=-5.679
 101 X=-14.325 Y=0 Z=-5.679
 102 X=-14.325 Y=0 Z=-7.789
 201 X=0 Y=0 Z=-5.679
 202 X=0 Y=0 Z=-7.789
 301 X=14.325 Y=0 Z=-5.679
 302 X=14.325 Y=0 Z=-7.789
 401 X=-15.25 Y=0 Z=-8.489
 402 X=-14.325 Y=0 Z=-8.489
 403 X=-13.9 Y=0 Z=-8.489
 404 X=-13.017 Y=0 Z=-8.489
 405 X=-12.133 Y=0 Z=-8.489
 406 X=-11.25 Y=0 Z=-8.489
 407 X=-10.367 Y=0 Z=-8.489
 408 X=-9.484 Y=0 Z=-8.489
 409 X=-8.6 Y=0 Z=-8.489
 410 X=-7.717 Y=0 Z=-8.489
 411 X=-6.834 Y=0 Z=-8.489
 412 X=-5.95 Y=0 Z=-8.489
 413 X=-5.067 Y=0 Z=-8.489
 414 X=-4.184 Y=0 Z=-8.489
 415 X=-3.3 Y=0 Z=-8.489
 416 X=-2.417 Y=0 Z=-8.489
 417 X=-1.534 Y=0 Z=-8.489
 418 X=-.65 Y=0 Z=-8.489
 419 X=0 Y=0 Z=-8.489
 420 X=.65 Y=0 Z=-8.489
 421 X=1.534 Y=0 Z=-8.489
 422 X=2.417 Y=0 Z=-8.489
 423 X=3.3 Y=0 Z=-8.489
 424 X=4.184 Y=0 Z=-8.489
 425 X=5.067 Y=0 Z=-8.489
 426 X=5.95 Y=0 Z=-8.489
 427 X=6.834 Y=0 Z=-8.489
 428 X=7.717 Y=0 Z=-8.489
 429 X=8.6 Y=0 Z=-8.489
 430 X=9.484 Y=0 Z=-8.489
 431 X=10.367 Y=0 Z=-8.489
 432 X=11.25 Y=0 Z=-8.489
 433 X=12.133 Y=0 Z=-8.489

434 X=13.017 Y=0 Z=-8.489
435 X=13.9 Y=0 Z=-8.489
436 X=14.325 Y=0 Z=-8.489
437 X=15.25 Y=0 Z=-8.489

PATTERN

NAME=TEMP
NAME=PRES

SPRING

ADD=405 U3=384087
ADD=406 U3=383869.6
ADD=407 U3=383869.6
ADD=408 U3=384087
ADD=409 U3=384087
ADD=410 U3=383869.6
ADD=411 U3=384087
ADD=412 U3=384087
ADD=413 U3=383869.6
ADD=414 U3=384087
ADD=415 U3=384087
ADD=416 U3=383869.6
ADD=417 U3=384087
ADD=419 U1=10000
ADD=421 U3=384087
ADD=422 U3=383869.6
ADD=423 U3=384087
ADD=424 U3=384087
ADD=425 U3=383869.6
ADD=426 U3=384087
ADD=427 U3=384087
ADD=428 U3=383869.6
ADD=429 U3=384087
ADD=430 U3=384087
ADD=431 U3=383869.6
ADD=432 U3=383869.6
ADD=433 U3=384087

MATERIAL

NAME=CONC IDES=C M=.2448 W=2.5
T=0 E=2800000 U=.2 A=.00001
NAME=STEEL IDES=S
T=0 E=2E+10 U=.3 A=.0000117 FY=25310.51
NAME=RIGID IDES=C
T=0 E=2464750 U=.3 A=.00001
NAME=CONC1 IDES=C M=.2448 W=2.5
T=0 E=2464750 U=.2 A=.00001

FRAME SECTION

NAME=T1 MAT=CONC SH=R T=.5,1 A=.5 J=2.861003E-02 I=1.041667E-02,4.897667E-02
AS=.4166667,.4166667
NAME=T2 MAT=CONC SH=R T=.542,1 A=.542 J=3.508126E-02 I=1.326834E-02,4.516667E-02
AS=.4516667,.4516667
NAME=T3 MAT=CONC SH=R T=.675,1 A=.675 J=5.967503E-02 I=2.562891E-02,.05625 AS=.5625,.5625
NAME=T4 MAT=CONC SH=R T=.916,1 A=.916 J=.1170223 I=6.404794E-02,7.633334E-02
AS=.7633333,.7633333

NAME=T5 MAT=CONC SH=R T=.68,1 A=.68 J=6.070982E-02 I=2.620267E-02,5.666667E-02
AS=.5666667,.5666667
NAME=T6 MAT=CONC SH=R T=.553,1 A=.553 J=3.688483E-02 I=.0140927,4.608333E-02
AS=.4608333,.4608333
NAME=T7 MAT=CONC SH=R T=.511,1 A=.511 J=3.024029E-02 I=.0111194,4.258334E-02
AS=.4258333,.4258333
NAME=T8 MAT=CONC SH=R T=.5,1 A=.5 J=2.861003E-02 I=1.041667E-02,4.897667E-02
AS=.4166667,.4166667
NAME=FOOT MAT=CONC1 SH=R T=1.4,1 A=1.4 J=.2612221 I=.2286666,.1166667 AS=1.166667,1.166667
NAME=WALL MAT=CONC1 SH=R T=.85,1 A=.85 J=9.985562E-02 I=4.117709E-02,7.083333E-02
AS=.7083334,.7083334
NAME=RIGID MAT=RIGID SH=R T=10,10 A=100 J=1408.333 I=833.5623,833.5623 AS=83.56233,83.56233
NAME=WALL1 MAT=CONC1 SH=R T=1.3,1 A=1.3 J=.2294606 I=.1830833,.1083333
AS=1.083333,1.083333
NAME=VAR1 TYPE=NONPR
SEC=T1,T2 EIVAR=1,1 L=.426
NAME=VAR2 TYPE=NONPR
SEC=T2,T3 EIVAR=1,1 L=.436
NAME=VAR3 TYPE=NONPR
SEC=T3,T4 EIVAR=1,1 L=.422
NAME=VAR4 TYPE=NONPR
SEC=T4,T5 EIVAR=1,1 L=.455
NAME=VAR5 TYPE=NONPR
SEC=T5,T6 EIVAR=1,1 L=.563
NAME=VAR6 TYPE=NONPR
SEC=T6,T7 EIVAR=1,1 L=1.392
NAME=VAR7 TYPE=NONPR
SEC=T7,T8 EIVAR=1,1 L=1.313

FRAME

1 J=1,2 SEC=T1 NSEG=1 ANG=180 IREL=R3
2 J=2,3 SEC=T1 NSEG=1 ANG=180
3 J=3,4 SEC=T1 NSEG=1 ANG=180
4 J=4,5 SEC=VAR1 NSEG=1 ANG=0
5 J=5,6 SEC=VAR2 NSEG=1 ANG=0
6 J=6,7 SEC=VAR3 NSEG=1 ANG=0
7 J=7,8 SEC=VAR4 NSEG=1 ANG=0
8 J=8,9 SEC=VAR5 NSEG=1 ANG=0
9 J=9,10 SEC=VAR6 NSEG=1 ANG=0
10 J=10,11 SEC=VAR7 NSEG=1 ANG=0
11 J=11,12 SEC=T8 NSEG=1 ANG=0
12 J=12,13 SEC=T8 NSEG=1 ANG=0
13 J=13,14 SEC=T8 NSEG=1 ANG=0
14 J=14,15 SEC=T8 NSEG=1 ANG=0
15 J=15,16 SEC=T8 NSEG=1 ANG=0
16 J=16,17 SEC=T8 NSEG=1 ANG=0
17 J=17,18 SEC=VAR7 NSEG=1 ANG=0
18 J=18,19 SEC=VAR6 NSEG=1 ANG=0
19 J=19,20 SEC=VAR5 NSEG=1 ANG=0
20 J=20,21 SEC=VAR4 NSEG=1 ANG=0
21 J=21,22 SEC=VAR3 NSEG=1 ANG=0
22 J=22,23 SEC=VAR2 NSEG=1 ANG=0
23 J=23,24 SEC=VAR1 NSEG=1 ANG=0
24 J=24,25 SEC=T1 NSEG=1 ANG=0
25 J=25,26 SEC=T1 NSEG=1 ANG=0
26 J=26,27 SEC=T1 NSEG=1 ANG=0 JREL=R3

27 J=28,29 SEC=T1 NSEG=1 ANG=180 IREL=R3
28 J=29,30 SEC=T1 NSEG=1 ANG=180
29 J=30,31 SEC=T1 NSEG=1 ANG=180
30 J=31,32 SEC=VAR1 NSEG=1 ANG=0
31 J=32,33 SEC=VAR2 NSEG=1 ANG=0
32 J=33,34 SEC=VAR3 NSEG=1 ANG=0
33 J=34,35 SEC=VAR4 NSEG=1 ANG=0
34 J=35,36 SEC=VAR5 NSEG=1 ANG=0
35 J=36,37 SEC=VAR6 NSEG=1 ANG=0
36 J=37,38 SEC=VAR7 NSEG=1 ANG=0
37 J=38,39 SEC=T8 NSEG=1 ANG=0
38 J=39,40 SEC=T8 NSEG=1 ANG=0
39 J=40,41 SEC=T8 NSEG=1 ANG=0
40 J=41,42 SEC=T8 NSEG=1 ANG=0
41 J=42,43 SEC=T8 NSEG=1 ANG=0
42 J=43,44 SEC=T8 NSEG=1 ANG=0
43 J=44,45 SEC=VAR7 NSEG=1 ANG=0
44 J=45,46 SEC=VAR6 NSEG=1 ANG=0
45 J=46,47 SEC=VAR5 NSEG=1 ANG=0
46 J=47,48 SEC=VAR4 NSEG=1 ANG=0
47 J=48,49 SEC=VAR3 NSEG=1 ANG=0
48 J=49,50 SEC=VAR2 NSEG=1 ANG=0
49 J=50,51 SEC=VAR1 NSEG=1 ANG=0
50 J=51,52 SEC=T1 NSEG=1 ANG=0
52 J=52,53 SEC=T1 NSEG=1 ANG=0
53 J=53,54 SEC=T1 NSEG=1 ANG=0 JREL=R3
85 J=28,201 SEC=RIGID NSEG=1 ANG=0
86 J=201,27 SEC=RIGID NSEG=1 ANG=0
87 J=301,54 SEC=RIGID NSEG=1 ANG=0
88 J=1,101 SEC=RIGID NSEG=1 ANG=0
101 J=102,101 SEC=WALL NSEG=1 ANG=180
102 J=402,102 SEC=WALL NSEG=1 ANG=180 IOFF=.4875 RIGID=0
201 J=202,201 SEC=WALL1 NSEG=1 ANG=0
202 J=419,202 SEC=WALL1 NSEG=1 ANG=0 IOFF=.375 RIGID=0
301 J=301,302 SEC=WALL NSEG=1 ANG=0
302 J=302,436 SEC=WALL NSEG=1 ANG=0 JOFF=.4875 RIGID=0
400 J=401,402 SEC=FOOT NSEG=1 ANG=0
401 J=402,403 SEC=FOOT NSEG=1 ANG=0 IOFF=.075 RIGID=0
402 J=403,404 SEC=FOOT NSEG=1 ANG=0
403 J=404,405 SEC=FOOT NSEG=1 ANG=0
404 J=405,406 SEC=FOOT NSEG=1 ANG=0
405 J=406,407 SEC=FOOT NSEG=1 ANG=0
406 J=407,408 SEC=FOOT NSEG=1 ANG=0
407 J=408,409 SEC=FOOT NSEG=1 ANG=0
408 J=409,410 SEC=FOOT NSEG=1 ANG=0
409 J=410,411 SEC=FOOT NSEG=1 ANG=0
410 J=411,412 SEC=FOOT NSEG=1 ANG=0
411 J=412,413 SEC=FOOT NSEG=1 ANG=0
412 J=413,414 SEC=FOOT NSEG=1 ANG=0
413 J=414,415 SEC=FOOT NSEG=1 ANG=0
414 J=415,416 SEC=FOOT NSEG=1 ANG=0
415 J=416,417 SEC=FOOT NSEG=1 ANG=0
416 J=417,418 SEC=FOOT NSEG=1 ANG=0
417 J=418,419 SEC=FOOT NSEG=1 ANG=0 JOFF=.3 RIGID=0
418 J=419,420 SEC=FOOT NSEG=1 ANG=0 IOFF=.3 RIGID=0
419 J=420,421 SEC=FOOT NSEG=1 ANG=0

420 J=421,422 SEC=FOOT NSEG=1 ANG=0
 421 J=422,423 SEC=FOOT NSEG=1 ANG=0
 422 J=423,424 SEC=FOOT NSEG=1 ANG=0
 423 J=424,425 SEC=FOOT NSEG=1 ANG=0
 424 J=425,426 SEC=FOOT NSEG=1 ANG=0
 425 J=426,427 SEC=FOOT NSEG=1 ANG=0
 426 J=427,428 SEC=FOOT NSEG=1 ANG=0
 427 J=428,429 SEC=FOOT NSEG=1 ANG=0
 428 J=429,430 SEC=FOOT NSEG=1 ANG=0
 429 J=430,431 SEC=FOOT NSEG=1 ANG=0
 430 J=431,432 SEC=FOOT NSEG=1 ANG=0
 431 J=432,433 SEC=FOOT NSEG=1 ANG=0
 432 J=433,434 SEC=FOOT NSEG=1 ANG=0
 433 J=434,435 SEC=FOOT NSEG=1 ANG=0
 434 J=435,436 SEC=FOOT NSEG=1 ANG=0 JOFF=.075 RIGID=0
 435 J=436,437 SEC=FOOT NSEG=1 ANG=0

LOAD

NAME=PVL1

TYPE=CONCENTRATED SPAN

ADD=414 RD=.057 UZ=-9.6
 ADD=412 RD=.019 UZ=-9.6
 ADD=410 RD=.661 UZ=-9.6
 ADD=408 RD=.623 UZ=-9.6
 ADD=407 RD=.265 UZ=-9.6
 ADD=405 RD=.227 UZ=-9.6
 ADD=421 RD=.943 UZ=-9.6
 ADD=423 RD=.981 UZ=-9.6
 ADD=425 RD=.339 UZ=-9.6
 ADD=427 RD=.377 UZ=-9.6
 ADD=428 RD=.735 UZ=-9.6
 ADD=430 RD=.773 UZ=-9.6

COMBO

NAME=COMB1

LOAD=PVL1 SF=2.15

OUTPUT

; No Output Requested

END

; File D:\WSAP2000DATA\개착식터널\활하중영향검토2.\$2k saved 11-25-02 13:22:43 in Ton-m

SYSTEM

DOF=UX,UZ,RY LENGTH=m FORCE=Ton LINES=59

JOINT

1 X=-14.25 Y=0 Z=-5.679
 2 X=-14.25 Y=0 Z=-5.026
 3 X=-14.25 Y=0 Z=-4.372
 4 X=-14.25 Y=0 Z=-3.719
 5 X=-14.23 Y=0 Z=-3.293
 6 X=-14.166 Y=0 Z=-2.86

7 X=-14.107 Y=0 Z=-2.444
 8 X=-13.748 Y=0 Z=-2.165
 9 X=-13.294 Y=0 Z=-1.832
 10 X=-12.092 Y=0 Z=-1.131
 11 X=-10.887 Y=0 Z=-.608
 12 X=-9.683 Y=0 Z=-.256
 13 X=-8.479 Y=0 Z=-.057
 14 X=-7.275 Y=0 Z=0
 15 X=-6.071 Y=0 Z=-.057
 16 X=-4.867 Y=0 Z=-.256
 17 X=-3.663 Y=0 Z=-.608
 18 X=-2.458 Y=0 Z=-1.131
 19 X=-1.256 Y=0 Z=-1.832
 20 X=-.795 Y=0 Z=-2.165
 21 X=-.443 Y=0 Z=-2.444
 22 X=-.369 Y=0 Z=-2.86
 23 X=-.318 Y=0 Z=-3.293
 24 X=-.3 Y=0 Z=-3.719
 25 X=-.3 Y=0 Z=-4.372
 26 X=-.3 Y=0 Z=-5.026
 27 X=-.3 Y=0 Z=-5.679
 28 X=.3 Y=0 Z=-5.679
 29 X=.3 Y=0 Z=-5.026
 30 X=.3 Y=0 Z=-4.372
 31 X=.3 Y=0 Z=-3.719
 32 X=.318 Y=0 Z=-3.293
 33 X=.369 Y=0 Z=-2.86
 34 X=.443 Y=0 Z=-2.444
 35 X=.795 Y=0 Z=-2.165
 36 X=1.256 Y=0 Z=-1.832
 37 X=2.458 Y=0 Z=-1.131
 38 X=3.663 Y=0 Z=-.608
 39 X=4.867 Y=0 Z=-.256
 40 X=6.071 Y=0 Z=-.057
 41 X=7.275 Y=0 Z=0
 42 X=8.479 Y=0 Z=-.057
 43 X=9.683 Y=0 Z=-.256
 44 X=10.887 Y=0 Z=-.608
 45 X=12.092 Y=0 Z=-1.131
 46 X=13.294 Y=0 Z=-1.832
 47 X=13.748 Y=0 Z=-2.165
 48 X=14.107 Y=0 Z=-2.444
 49 X=14.166 Y=0 Z=-2.86
 50 X=14.23 Y=0 Z=-3.293
 51 X=14.25 Y=0 Z=-3.719
 52 X=14.25 Y=0 Z=-4.372
 53 X=14.25 Y=0 Z=-5.026
 54 X=14.25 Y=0 Z=-5.679
 101 X=-14.325 Y=0 Z=-5.679
 102 X=-14.325 Y=0 Z=-7.789
 201 X=0 Y=0 Z=-5.679
 202 X=0 Y=0 Z=-7.789
 301 X=14.325 Y=0 Z=-5.679
 302 X=14.325 Y=0 Z=-7.789
 401 X=-15.25 Y=0 Z=-8.489
 402 X=-14.325 Y=0 Z=-8.489

403 X=-13.9 Y=0 Z=-8.489
 404 X=-13.017 Y=0 Z=-8.489
 405 X=-12.133 Y=0 Z=-8.489
 406 X=-11.25 Y=0 Z=-8.489
 407 X=-10.367 Y=0 Z=-8.489
 408 X=-9.484 Y=0 Z=-8.489
 409 X=-8.6 Y=0 Z=-8.489
 410 X=-7.717 Y=0 Z=-8.489
 411 X=-6.834 Y=0 Z=-8.489
 412 X=-5.95 Y=0 Z=-8.489
 413 X=-5.067 Y=0 Z=-8.489
 414 X=-4.184 Y=0 Z=-8.489
 415 X=-3.3 Y=0 Z=-8.489
 416 X=-2.417 Y=0 Z=-8.489
 417 X=-1.534 Y=0 Z=-8.489
 418 X=-.65 Y=0 Z=-8.489
 419 X=0 Y=0 Z=-8.489
 420 X=.65 Y=0 Z=-8.489
 421 X=1.534 Y=0 Z=-8.489
 422 X=2.417 Y=0 Z=-8.489
 423 X=3.3 Y=0 Z=-8.489
 424 X=4.184 Y=0 Z=-8.489
 425 X=5.067 Y=0 Z=-8.489
 426 X=5.95 Y=0 Z=-8.489
 427 X=6.834 Y=0 Z=-8.489
 428 X=7.717 Y=0 Z=-8.489
 429 X=8.6 Y=0 Z=-8.489
 430 X=9.484 Y=0 Z=-8.489
 431 X=10.367 Y=0 Z=-8.489
 432 X=11.25 Y=0 Z=-8.489
 433 X=12.133 Y=0 Z=-8.489
 434 X=13.017 Y=0 Z=-8.489
 435 X=13.9 Y=0 Z=-8.489
 436 X=14.325 Y=0 Z=-8.489
 437 X=15.25 Y=0 Z=-8.489

PATTERN

NAME=TEMP
 NAME=PRES

SPRING

ADD=406 U3=383869.6
 ADD=407 U3=383869.6
 ADD=408 U3=384087
 ADD=409 U3=384087
 ADD=410 U3=383869.6
 ADD=411 U3=384087
 ADD=412 U3=384087
 ADD=413 U3=383869.6
 ADD=414 U3=384087
 ADD=415 U3=384087
 ADD=416 U3=383869.6
 ADD=417 U3=384087
 ADD=418 U3=333440.5
 ADD=419 U1=10000 U3=282576.7
 ADD=420 U3=333440.5

ADD=421 U3=384087
 ADD=422 U3=383869.6
 ADD=423 U3=384087
 ADD=424 U3=384087
 ADD=425 U3=383869.6
 ADD=426 U3=384087
 ADD=427 U3=384087
 ADD=428 U3=383869.6
 ADD=429 U3=384087
 ADD=430 U3=384087
 ADD=431 U3=383869.6
 ADD=432 U3=383869.6

MATERIAL

NAME=CONC IDES=C M=.2448 W=2.5
 T=0 E=2800000 U=.2 A=.00001
 NAME=STEEL IDES=S
 T=0 E=2E+10 U=.3 A=.0000117 FY=25310.51
 NAME=RIGID IDES=C
 T=0 E=2464750 U=.3 A=.00001
 NAME=CONC1 IDES=C M=.2448 W=2.5
 T=0 E=2464750 U=.2 A=.00001

FRAME SECTION

NAME=T1 MAT=CONC SH=R T=.5,1 A=.5 J=2.861003E-02 I=1.041667E-02,4.897667E-02
 AS=.4166667,.4166667
 NAME=T2 MAT=CONC SH=R T=.542,1 A=.542 J=3.508126E-02 I=1.326834E-02,4.516667E-02
 AS=.4516667,.4516667
 NAME=T3 MAT=CONC SH=R T=.675,1 A=.675 J=5.967503E-02 I=2.562891E-02,.05625 AS=.5625,.5625
 NAME=T4 MAT=CONC SH=R T=.916,1 A=.916 J=.1170223 I=6.404794E-02,7.633334E-02
 AS=.7633333,.7633333
 NAME=T5 MAT=CONC SH=R T=.68,1 A=.68 J=6.070982E-02 I=2.620267E-02,5.666667E-02
 AS=.5666667,.5666667
 NAME=T6 MAT=CONC SH=R T=.553,1 A=.553 J=3.688483E-02 I=.0140927,4.608333E-02
 AS=.4608333,.4608333
 NAME=T7 MAT=CONC SH=R T=.511,1 A=.511 J=3.024029E-02 I=.0111194,4.258334E-02
 AS=.4258333,.4258333
 NAME=T8 MAT=CONC SH=R T=.5,1 A=.5 J=2.861003E-02 I=1.041667E-02,4.897667E-02
 AS=.4166667,.4166667
 NAME=FOOT MAT=CONC1 SH=R T=1.4,1 A=1.4 J=.2612221 I=.2286666,.1166667 AS=1.166667,1.166667
 NAME=WALL MAT=CONC1 SH=R T=.85,1 A=.85 J=9.985562E-02 I=4.117709E-02,7.083333E-02
 AS=.7083334,.7083334
 NAME=RIGID MAT=RIGID SH=R T=10,10 A=100 J=1408.333 I=833.5623,833.5623 AS=83.56233,83.56233
 NAME=WALL1 MAT=CONC1 SH=R T=1.3,1 A=1.3 J=.2294606 I=.1830833,.1083333
 AS=1.083333,1.083333
 NAME=VAR1 TYPE=NONPR
 SEC=T1,T2 EIVAR=1,1 L=.426
 NAME=VAR2 TYPE=NONPR
 SEC=T2,T3 EIVAR=1,1 L=.436
 NAME=VAR3 TYPE=NONPR
 SEC=T3,T4 EIVAR=1,1 L=.422
 NAME=VAR4 TYPE=NONPR
 SEC=T4,T5 EIVAR=1,1 L=.455
 NAME=VAR5 TYPE=NONPR
 SEC=T5,T6 EIVAR=1,1 L=.563
 NAME=VAR6 TYPE=NONPR

SEC=T6,T7 EIVAR=1,1 L=1.392
NAME=VAR7 TYPE=NONPR
SEC=T7,T8 EIVAR=1,1 L=1.313

FRAME

1 J=1,2 SEC=T1 NSEG=1 ANG=180 IREL=R3
2 J=2,3 SEC=T1 NSEG=1 ANG=180
3 J=3,4 SEC=T1 NSEG=1 ANG=180
4 J=4,5 SEC=VAR1 NSEG=1 ANG=0
5 J=5,6 SEC=VAR2 NSEG=1 ANG=0
6 J=6,7 SEC=VAR3 NSEG=1 ANG=0
7 J=7,8 SEC=VAR4 NSEG=1 ANG=0
8 J=8,9 SEC=VAR5 NSEG=1 ANG=0
9 J=9,10 SEC=VAR6 NSEG=1 ANG=0
10 J=10,11 SEC=VAR7 NSEG=1 ANG=0
11 J=11,12 SEC=T8 NSEG=1 ANG=0
12 J=12,13 SEC=T8 NSEG=1 ANG=0
13 J=13,14 SEC=T8 NSEG=1 ANG=0
14 J=14,15 SEC=T8 NSEG=1 ANG=0
15 J=15,16 SEC=T8 NSEG=1 ANG=0
16 J=16,17 SEC=T8 NSEG=1 ANG=0
17 J=17,18 SEC=VAR7 NSEG=1 ANG=0
18 J=18,19 SEC=VAR6 NSEG=1 ANG=0
19 J=19,20 SEC=VAR5 NSEG=1 ANG=0
20 J=20,21 SEC=VAR4 NSEG=1 ANG=0
21 J=21,22 SEC=VAR3 NSEG=1 ANG=0
22 J=22,23 SEC=VAR2 NSEG=1 ANG=0
23 J=23,24 SEC=VAR1 NSEG=1 ANG=0
24 J=24,25 SEC=T1 NSEG=1 ANG=0
25 J=25,26 SEC=T1 NSEG=1 ANG=0
26 J=26,27 SEC=T1 NSEG=1 ANG=0 JREL=R3
27 J=28,29 SEC=T1 NSEG=1 ANG=180 IREL=R3
28 J=29,30 SEC=T1 NSEG=1 ANG=180
29 J=30,31 SEC=T1 NSEG=1 ANG=180
30 J=31,32 SEC=VAR1 NSEG=1 ANG=0
31 J=32,33 SEC=VAR2 NSEG=1 ANG=0
32 J=33,34 SEC=VAR3 NSEG=1 ANG=0
33 J=34,35 SEC=VAR4 NSEG=1 ANG=0
34 J=35,36 SEC=VAR5 NSEG=1 ANG=0
35 J=36,37 SEC=VAR6 NSEG=1 ANG=0
36 J=37,38 SEC=VAR7 NSEG=1 ANG=0
37 J=38,39 SEC=T8 NSEG=1 ANG=0
38 J=39,40 SEC=T8 NSEG=1 ANG=0
39 J=40,41 SEC=T8 NSEG=1 ANG=0
40 J=41,42 SEC=T8 NSEG=1 ANG=0
41 J=42,43 SEC=T8 NSEG=1 ANG=0
42 J=43,44 SEC=T8 NSEG=1 ANG=0
43 J=44,45 SEC=VAR7 NSEG=1 ANG=0
44 J=45,46 SEC=VAR6 NSEG=1 ANG=0
45 J=46,47 SEC=VAR5 NSEG=1 ANG=0
46 J=47,48 SEC=VAR4 NSEG=1 ANG=0
47 J=48,49 SEC=VAR3 NSEG=1 ANG=0
48 J=49,50 SEC=VAR2 NSEG=1 ANG=0
49 J=50,51 SEC=VAR1 NSEG=1 ANG=0
50 J=51,52 SEC=T1 NSEG=1 ANG=0
52 J=52,53 SEC=T1 NSEG=1 ANG=0

53 J=53,54 SEC=T1 NSEG=1 ANG=0 JREL=R3
 85 J=28,201 SEC=RIGID NSEG=1 ANG=0
 86 J=201,27 SEC=RIGID NSEG=1 ANG=0
 87 J=301,54 SEC=RIGID NSEG=1 ANG=0
 88 J=1,101 SEC=RIGID NSEG=1 ANG=0
 101 J=102,101 SEC=WALL NSEG=1 ANG=180
 102 J=402,102 SEC=WALL NSEG=1 ANG=180 IOFF=.4875 RIGID=0
 201 J=202,201 SEC=WALL1 NSEG=1 ANG=0
 202 J=419,202 SEC=WALL1 NSEG=1 ANG=0 IOFF=.375 RIGID=0
 301 J=301,302 SEC=WALL NSEG=1 ANG=0
 302 J=302,436 SEC=WALL NSEG=1 ANG=0 JOFF=.4875 RIGID=0
 400 J=401,402 SEC=FOOT NSEG=1 ANG=0
 401 J=402,403 SEC=FOOT NSEG=1 ANG=0 IOFF=.075 RIGID=0
 402 J=403,404 SEC=FOOT NSEG=1 ANG=0
 403 J=404,405 SEC=FOOT NSEG=1 ANG=0
 404 J=405,406 SEC=FOOT NSEG=1 ANG=0
 405 J=406,407 SEC=FOOT NSEG=1 ANG=0
 406 J=407,408 SEC=FOOT NSEG=1 ANG=0
 407 J=408,409 SEC=FOOT NSEG=1 ANG=0
 408 J=409,410 SEC=FOOT NSEG=1 ANG=0
 409 J=410,411 SEC=FOOT NSEG=1 ANG=0
 410 J=411,412 SEC=FOOT NSEG=1 ANG=0
 411 J=412,413 SEC=FOOT NSEG=1 ANG=0
 412 J=413,414 SEC=FOOT NSEG=1 ANG=0
 413 J=414,415 SEC=FOOT NSEG=1 ANG=0
 414 J=415,416 SEC=FOOT NSEG=1 ANG=0
 415 J=416,417 SEC=FOOT NSEG=1 ANG=0
 416 J=417,418 SEC=FOOT NSEG=1 ANG=0
 417 J=418,419 SEC=FOOT NSEG=1 ANG=0 JOFF=.3 RIGID=0
 418 J=419,420 SEC=FOOT NSEG=1 ANG=0 IOFF=.3 RIGID=0
 419 J=420,421 SEC=FOOT NSEG=1 ANG=0
 420 J=421,422 SEC=FOOT NSEG=1 ANG=0
 421 J=422,423 SEC=FOOT NSEG=1 ANG=0
 422 J=423,424 SEC=FOOT NSEG=1 ANG=0
 423 J=424,425 SEC=FOOT NSEG=1 ANG=0
 424 J=425,426 SEC=FOOT NSEG=1 ANG=0
 425 J=426,427 SEC=FOOT NSEG=1 ANG=0
 426 J=427,428 SEC=FOOT NSEG=1 ANG=0
 427 J=428,429 SEC=FOOT NSEG=1 ANG=0
 428 J=429,430 SEC=FOOT NSEG=1 ANG=0
 429 J=430,431 SEC=FOOT NSEG=1 ANG=0
 430 J=431,432 SEC=FOOT NSEG=1 ANG=0
 431 J=432,433 SEC=FOOT NSEG=1 ANG=0
 432 J=433,434 SEC=FOOT NSEG=1 ANG=0
 433 J=434,435 SEC=FOOT NSEG=1 ANG=0
 434 J=435,436 SEC=FOOT NSEG=1 ANG=0 JOFF=.075 RIGID=0
 435 J=436,437 SEC=FOOT NSEG=1 ANG=0

LOAD

NAME=PVL2

TYPE=CONCENTRATED SPAN

ADD=415 RD=.216 UZ=-9.6

ADD=413 RD=.717 UZ=-9.6

ADD=412 RD=.359 UZ=-9.6

ADD=410 RD=.321 UZ=-9.6

ADD=408 RD=.963 UZ=-9.6

ADD=406 RD=.925 UZ=-9.6
 ADD=420 RD=.784 UZ=-9.6
 ADD=422 RD=.283 UZ=-9.6
 ADD=423 RD=.641 UZ=-9.6
 ADD=425 RD=.679 UZ=-9.6
 ADD=427 RD=.037 UZ=-9.6
 ADD=429 RD=.075 UZ=-9.6

COMBO

NAME=COMB1

LOAD=PVL2 SF=2.15

OUTPUT

; No Output Requested

END

; File D:\WSAP2000DATA\W개착식터널\W활하중영향검토3.\$2k saved 11-25-02 13:22:56 in Ton-m

SYSTEM

DOF=UX,UZ,RY LENGTH=m FORCE=Ton LINES=59

JOINT

1 X=-14.25 Y=0 Z=-5.679
 2 X=-14.25 Y=0 Z=-5.026
 3 X=-14.25 Y=0 Z=-4.372
 4 X=-14.25 Y=0 Z=-3.719
 5 X=-14.23 Y=0 Z=-3.293
 6 X=-14.166 Y=0 Z=-2.86
 7 X=-14.107 Y=0 Z=-2.444
 8 X=-13.748 Y=0 Z=-2.165
 9 X=-13.294 Y=0 Z=-1.832
 10 X=-12.092 Y=0 Z=-1.131
 11 X=-10.887 Y=0 Z=-.608
 12 X=-9.683 Y=0 Z=-.256
 13 X=-8.479 Y=0 Z=-.057
 14 X=-7.275 Y=0 Z=0
 15 X=-6.071 Y=0 Z=-.057
 16 X=-4.867 Y=0 Z=-.256
 17 X=-3.663 Y=0 Z=-.608
 18 X=-2.458 Y=0 Z=-1.131
 19 X=-1.256 Y=0 Z=-1.832
 20 X=-.795 Y=0 Z=-2.165
 21 X=-.443 Y=0 Z=-2.444
 22 X=-.369 Y=0 Z=-2.86
 23 X=-.318 Y=0 Z=-3.293
 24 X=-.3 Y=0 Z=-3.719
 25 X=-.3 Y=0 Z=-4.372
 26 X=-.3 Y=0 Z=-5.026
 27 X=-.3 Y=0 Z=-5.679
 28 X=.3 Y=0 Z=-5.679
 29 X=.3 Y=0 Z=-5.026
 30 X=.3 Y=0 Z=-4.372
 31 X=.3 Y=0 Z=-3.719

32 X=.318 Y=0 Z=-3.293
 33 X=.369 Y=0 Z=-2.86
 34 X=.443 Y=0 Z=-2.444
 35 X=.795 Y=0 Z=-2.165
 36 X=1.256 Y=0 Z=-1.832
 37 X=2.458 Y=0 Z=-1.131
 38 X=3.663 Y=0 Z=-.608
 39 X=4.867 Y=0 Z=-.256
 40 X=6.071 Y=0 Z=-.057
 41 X=7.275 Y=0 Z=0
 42 X=8.479 Y=0 Z=-.057
 43 X=9.683 Y=0 Z=-.256
 44 X=10.887 Y=0 Z=-.608
 45 X=12.092 Y=0 Z=-1.131
 46 X=13.294 Y=0 Z=-1.832
 47 X=13.748 Y=0 Z=-2.165
 48 X=14.107 Y=0 Z=-2.444
 49 X=14.166 Y=0 Z=-2.86
 50 X=14.23 Y=0 Z=-3.293
 51 X=14.25 Y=0 Z=-3.719
 52 X=14.25 Y=0 Z=-4.372
 53 X=14.25 Y=0 Z=-5.026
 54 X=14.25 Y=0 Z=-5.679
 101 X=-14.325 Y=0 Z=-5.679
 102 X=-14.325 Y=0 Z=-7.789
 201 X=0 Y=0 Z=-5.679
 202 X=0 Y=0 Z=-7.789
 301 X=14.325 Y=0 Z=-5.679
 302 X=14.325 Y=0 Z=-7.789
 401 X=-15.25 Y=0 Z=-8.489
 402 X=-14.325 Y=0 Z=-8.489
 403 X=-13.9 Y=0 Z=-8.489
 404 X=-13.017 Y=0 Z=-8.489
 405 X=-12.133 Y=0 Z=-8.489
 406 X=-11.25 Y=0 Z=-8.489
 407 X=-10.367 Y=0 Z=-8.489
 408 X=-9.484 Y=0 Z=-8.489
 409 X=-8.6 Y=0 Z=-8.489
 410 X=-7.717 Y=0 Z=-8.489
 411 X=-6.834 Y=0 Z=-8.489
 412 X=-5.95 Y=0 Z=-8.489
 413 X=-5.067 Y=0 Z=-8.489
 414 X=-4.184 Y=0 Z=-8.489
 415 X=-3.3 Y=0 Z=-8.489
 416 X=-2.417 Y=0 Z=-8.489
 417 X=-1.534 Y=0 Z=-8.489
 418 X=-.65 Y=0 Z=-8.489
 419 X=0 Y=0 Z=-8.489
 420 X=.65 Y=0 Z=-8.489
 421 X=1.534 Y=0 Z=-8.489
 422 X=2.417 Y=0 Z=-8.489
 423 X=3.3 Y=0 Z=-8.489
 424 X=4.184 Y=0 Z=-8.489
 425 X=5.067 Y=0 Z=-8.489
 426 X=5.95 Y=0 Z=-8.489
 427 X=6.834 Y=0 Z=-8.489

428 X=7.717 Y=0 Z=-8.489
429 X=8.6 Y=0 Z=-8.489
430 X=9.484 Y=0 Z=-8.489
431 X=10.367 Y=0 Z=-8.489
432 X=11.25 Y=0 Z=-8.489
433 X=12.133 Y=0 Z=-8.489
434 X=13.017 Y=0 Z=-8.489
435 X=13.9 Y=0 Z=-8.489
436 X=14.325 Y=0 Z=-8.489
437 X=15.25 Y=0 Z=-8.489

PATTERN

NAME=TEMP
NAME=PRES

SPRING

ADD=402 U3=293445
ADD=403 U3=284315.6
ADD=404 U3=384087
ADD=405 U3=384087
ADD=406 U3=383869.6
ADD=407 U3=383869.6
ADD=408 U3=384087
ADD=409 U3=384087
ADD=410 U3=383869.6
ADD=411 U3=384087
ADD=412 U3=384087
ADD=413 U3=383869.6
ADD=414 U3=384087
ADD=415 U3=384087
ADD=419 U1=10000
ADD=423 U3=384087
ADD=424 U3=384087
ADD=425 U3=383869.6
ADD=426 U3=384087
ADD=427 U3=384087
ADD=428 U3=383869.6
ADD=429 U3=384087
ADD=430 U3=384087
ADD=431 U3=383869.6
ADD=432 U3=383869.6
ADD=433 U3=384087
ADD=434 U3=384087
ADD=435 U3=284315.6
ADD=436 U3=293445

MATERIAL

NAME=CONC IDES=C M=.2448 W=2.5
T=0 E=2800000 U=.2 A=.00001
NAME=STEEL IDES=S
T=0 E=2E+10 U=.3 A=.0000117 FY=25310.51
NAME=RIGID IDES=C
T=0 E=2464750 U=.3 A=.00001
NAME=CONC1 IDES=C M=.2448 W=2.5
T=0 E=2464750 U=.2 A=.00001

FRAME SECTION

NAME=T1 MAT=CONC SH=R T=.5,1 A=.5 J=2.861003E-02 I=1.041667E-02,4.897667E-02
AS=.4166667,.4166667
NAME=T2 MAT=CONC SH=R T=.542,1 A=.542 J=3.508126E-02 I=1.326834E-02,4.516667E-02
AS=.4516667,.4516667
NAME=T3 MAT=CONC SH=R T=.675,1 A=.675 J=5.967503E-02 I=2.562891E-02,.05625 AS=.5625,.5625
NAME=T4 MAT=CONC SH=R T=.916,1 A=.916 J=.1170223 I=6.404794E-02,7.633334E-02
AS=.7633333,.7633333
NAME=T5 MAT=CONC SH=R T=.68,1 A=.68 J=6.070982E-02 I=2.620267E-02,5.666667E-02
AS=.5666667,.5666667
NAME=T6 MAT=CONC SH=R T=.553,1 A=.553 J=3.688483E-02 I=.0140927,4.608333E-02
AS=.4608333,.4608333
NAME=T7 MAT=CONC SH=R T=.511,1 A=.511 J=3.024029E-02 I=.0111194,4.258334E-02
AS=.4258333,.4258333
NAME=T8 MAT=CONC SH=R T=.5,1 A=.5 J=2.861003E-02 I=1.041667E-02,4.897667E-02
AS=.4166667,.4166667
NAME=FOOT MAT=CONC1 SH=R T=1.4,1 A=1.4 J=.2612221 I=.2286666,.1166667 AS=1.166667,1.166667
NAME=WALL MAT=CONC1 SH=R T=.85,1 A=.85 J=9.985562E-02 I=4.117709E-02,7.083333E-02
AS=.7083334,.7083334
NAME=RIGID MAT=RIGID SH=R T=10,10 A=100 J=1408.333 I=833.5623,833.5623 AS=83.56233,83.56233
NAME=WALL1 MAT=CONC1 SH=R T=1.3,1 A=1.3 J=.2294606 I=.1830833,.1083333
AS=1.083333,1.083333
NAME=VAR1 TYPE=NONPR
SEC=T1,T2 EIVAR=1,1 L=.426
NAME=VAR2 TYPE=NONPR
SEC=T2,T3 EIVAR=1,1 L=.436
NAME=VAR3 TYPE=NONPR
SEC=T3,T4 EIVAR=1,1 L=.422
NAME=VAR4 TYPE=NONPR
SEC=T4,T5 EIVAR=1,1 L=.455
NAME=VAR5 TYPE=NONPR
SEC=T5,T6 EIVAR=1,1 L=.563
NAME=VAR6 TYPE=NONPR
SEC=T6,T7 EIVAR=1,1 L=1.392
NAME=VAR7 TYPE=NONPR
SEC=T7,T8 EIVAR=1,1 L=1.313

FRAME

1 J=1,2 SEC=T1 NSEG=1 ANG=180 IREL=R3
2 J=2,3 SEC=T1 NSEG=1 ANG=180
3 J=3,4 SEC=T1 NSEG=1 ANG=180
4 J=4,5 SEC=VAR1 NSEG=1 ANG=0
5 J=5,6 SEC=VAR2 NSEG=1 ANG=0
6 J=6,7 SEC=VAR3 NSEG=1 ANG=0
7 J=7,8 SEC=VAR4 NSEG=1 ANG=0
8 J=8,9 SEC=VAR5 NSEG=1 ANG=0
9 J=9,10 SEC=VAR6 NSEG=1 ANG=0
10 J=10,11 SEC=VAR7 NSEG=1 ANG=0
11 J=11,12 SEC=T8 NSEG=1 ANG=0
12 J=12,13 SEC=T8 NSEG=1 ANG=0
13 J=13,14 SEC=T8 NSEG=1 ANG=0
14 J=14,15 SEC=T8 NSEG=1 ANG=0
15 J=15,16 SEC=T8 NSEG=1 ANG=0
16 J=16,17 SEC=T8 NSEG=1 ANG=0
17 J=17,18 SEC=VAR7 NSEG=1 ANG=0
18 J=18,19 SEC=VAR6 NSEG=1 ANG=0

19 J=19,20 SEC=VAR5 NSEG=1 ANG=0
 20 J=20,21 SEC=VAR4 NSEG=1 ANG=0
 21 J=21,22 SEC=VAR3 NSEG=1 ANG=0
 22 J=22,23 SEC=VAR2 NSEG=1 ANG=0
 23 J=23,24 SEC=VAR1 NSEG=1 ANG=0
 24 J=24,25 SEC=T1 NSEG=1 ANG=0
 25 J=25,26 SEC=T1 NSEG=1 ANG=0
 26 J=26,27 SEC=T1 NSEG=1 ANG=0 JREL=R3
 27 J=28,29 SEC=T1 NSEG=1 ANG=180 IREL=R3
 28 J=29,30 SEC=T1 NSEG=1 ANG=180
 29 J=30,31 SEC=T1 NSEG=1 ANG=180
 30 J=31,32 SEC=VAR1 NSEG=1 ANG=0
 31 J=32,33 SEC=VAR2 NSEG=1 ANG=0
 32 J=33,34 SEC=VAR3 NSEG=1 ANG=0
 33 J=34,35 SEC=VAR4 NSEG=1 ANG=0
 34 J=35,36 SEC=VAR5 NSEG=1 ANG=0
 35 J=36,37 SEC=VAR6 NSEG=1 ANG=0
 36 J=37,38 SEC=VAR7 NSEG=1 ANG=0
 37 J=38,39 SEC=T8 NSEG=1 ANG=0
 38 J=39,40 SEC=T8 NSEG=1 ANG=0
 39 J=40,41 SEC=T8 NSEG=1 ANG=0
 40 J=41,42 SEC=T8 NSEG=1 ANG=0
 41 J=42,43 SEC=T8 NSEG=1 ANG=0
 42 J=43,44 SEC=T8 NSEG=1 ANG=0
 43 J=44,45 SEC=VAR7 NSEG=1 ANG=0
 44 J=45,46 SEC=VAR6 NSEG=1 ANG=0
 45 J=46,47 SEC=VAR5 NSEG=1 ANG=0
 46 J=47,48 SEC=VAR4 NSEG=1 ANG=0
 47 J=48,49 SEC=VAR3 NSEG=1 ANG=0
 48 J=49,50 SEC=VAR2 NSEG=1 ANG=0
 49 J=50,51 SEC=VAR1 NSEG=1 ANG=0
 50 J=51,52 SEC=T1 NSEG=1 ANG=0
 52 J=52,53 SEC=T1 NSEG=1 ANG=0
 53 J=53,54 SEC=T1 NSEG=1 ANG=0 JREL=R3
 85 J=28,201 SEC=RIGID NSEG=1 ANG=0
 86 J=201,27 SEC=RIGID NSEG=1 ANG=0
 87 J=301,54 SEC=RIGID NSEG=1 ANG=0
 88 J=1,101 SEC=RIGID NSEG=1 ANG=0
 101 J=102,101 SEC=WALL NSEG=1 ANG=180
 102 J=402,102 SEC=WALL NSEG=1 ANG=180 IOFF=.4875 RIGID=0
 201 J=202,201 SEC=WALL1 NSEG=1 ANG=0
 202 J=419,202 SEC=WALL1 NSEG=1 ANG=0 IOFF=.375 RIGID=0
 301 J=301,302 SEC=WALL NSEG=1 ANG=0
 302 J=302,436 SEC=WALL NSEG=1 ANG=0 JOFF=.4875 RIGID=0
 400 J=401,402 SEC=FOOT NSEG=1 ANG=0
 401 J=402,403 SEC=FOOT NSEG=1 ANG=0 IOFF=.075 RIGID=0
 402 J=403,404 SEC=FOOT NSEG=1 ANG=0
 403 J=404,405 SEC=FOOT NSEG=1 ANG=0
 404 J=405,406 SEC=FOOT NSEG=1 ANG=0
 405 J=406,407 SEC=FOOT NSEG=1 ANG=0
 406 J=407,408 SEC=FOOT NSEG=1 ANG=0
 407 J=408,409 SEC=FOOT NSEG=1 ANG=0
 408 J=409,410 SEC=FOOT NSEG=1 ANG=0
 409 J=410,411 SEC=FOOT NSEG=1 ANG=0
 410 J=411,412 SEC=FOOT NSEG=1 ANG=0
 411 J=412,413 SEC=FOOT NSEG=1 ANG=0

412 J=413,414 SEC=FOOT NSEG=1 ANG=0
 413 J=414,415 SEC=FOOT NSEG=1 ANG=0
 414 J=415,416 SEC=FOOT NSEG=1 ANG=0
 415 J=416,417 SEC=FOOT NSEG=1 ANG=0
 416 J=417,418 SEC=FOOT NSEG=1 ANG=0
 417 J=418,419 SEC=FOOT NSEG=1 ANG=0 JOFF=.3 RIGID=0
 418 J=419,420 SEC=FOOT NSEG=1 ANG=0 IOFF=.3 RIGID=0
 419 J=420,421 SEC=FOOT NSEG=1 ANG=0
 420 J=421,422 SEC=FOOT NSEG=1 ANG=0
 421 J=422,423 SEC=FOOT NSEG=1 ANG=0
 422 J=423,424 SEC=FOOT NSEG=1 ANG=0
 423 J=424,425 SEC=FOOT NSEG=1 ANG=0
 424 J=425,426 SEC=FOOT NSEG=1 ANG=0
 425 J=426,427 SEC=FOOT NSEG=1 ANG=0
 426 J=427,428 SEC=FOOT NSEG=1 ANG=0
 427 J=428,429 SEC=FOOT NSEG=1 ANG=0
 428 J=429,430 SEC=FOOT NSEG=1 ANG=0
 429 J=430,431 SEC=FOOT NSEG=1 ANG=0
 430 J=431,432 SEC=FOOT NSEG=1 ANG=0
 431 J=432,433 SEC=FOOT NSEG=1 ANG=0
 432 J=433,434 SEC=FOOT NSEG=1 ANG=0
 433 J=434,435 SEC=FOOT NSEG=1 ANG=0
 434 J=435,436 SEC=FOOT NSEG=1 ANG=0 JOFF=.075 RIGID=0
 435 J=436,437 SEC=FOOT NSEG=1 ANG=0

LOAD

NAME=PVL3

TYPE=CONCENTRATED SPAN

ADD=412 RD=.359 UZ=-9.6
 ADD=410 RD=.321 UZ=-9.6
 ADD=409 RD=.037 UZ=-9.6
 ADD=406 RD=.925 UZ=-9.6
 ADD=405 RD=.566 UZ=-9.6
 ADD=403 RD=.528 UZ=-9.6
 ADD=423 RD=.641 UZ=-9.6
 ADD=425 RD=.679 UZ=-9.6
 ADD=426 RD=.963 UZ=-9.6
 ADD=429 RD=.075 UZ=-9.6
 ADD=430 RD=.434 UZ=-9.6
 ADD=432 RD=.472 UZ=-9.6

COMBO

NAME=COMB1

LOAD=PVL3 SF=2.15

OUTPUT

; No Output Requested

END

; File D:\PAB
BAK\SAP2000(FEM)\개확식터널마감벽\WING1.\$2k saved
9-27-02 9:05:21 in Ton-mm

SYSTEM

DOF=UX,UY,UZ,RX,RY,RZ LENGTH=mm FORCE=Ton
LINES=59

JOINT

1 X=-3663 Y=0 Z=9456
2 X=-2759 Y=0 Z=9456
3 X=-1856 Y=0 Z=9456
4 X=-953 Y=0 Z=9456
5 X=0 Y=0 Z=9456
6 X=953 Y=0 Z=9456
7 X=1856 Y=0 Z=9456
8 X=2759 Y=0 Z=9456
9 X=3663 Y=0 Z=9456
10 X=4566 Y=0 Z=9456
11 X=9984 Y=0 Z=9456
12 X=14749 Y=0 Z=9456
13 X=14500 Y=0 Z=9456
14 X=-16056.33 Y=0 Z=889
15 X=-16056.33 Y=0 Z=1991
16 X=-15249 Y=0 Z=889
17 X=10888 Y=0 Z=9456
18 X=11791 Y=0 Z=9456
19 X=-15249 Y=0 Z=1991
20 X=-16056.33 Y=0 Z=2911
21 X=-14749 Y=0 Z=7131
22 X=-15249 Y=0 Z=2911
23 X=-16056.33 Y=0 Z=3831
24 X=-14749 Y=0 Z=9590
26 X=-15249 Y=0 Z=3831
27 X=-14749 Y=0 Z=11236
28 X=-16056.33 Y=0 Z=9456
29 X=-16056.33 Y=0 Z=9590
30 X=-15249 Y=0 Z=9456
31 X=-14749 Y=0 Z=1991
32 X=-15249 Y=0 Z=9590
33 X=-16056.33 Y=0 Z=4656
34 X=-14749 Y=0 Z=9456
35 X=-14500 Y=0 Z=9456
36 X=-13597 Y=0 Z=9456
37 X=14749 Y=0 Z=7131
38 X=-15249 Y=0 Z=4656
39 X=-14749 Y=0 Z=2911
40 X=14749 Y=0 Z=9590
41 X=-16056.33 Y=0 Z=5481
42 X=-15249 Y=0 Z=5481
43 X=14749 Y=0 Z=11236
44 X=-16056.33 Y=0 Z=6306
45 X=-15249 Y=0 Z=6306
46 X=-16056.33 Y=0 Z=9000
47 X=-15249 Y=0 Z=9000
48 X=14749 Y=0 Z=1071
49 X=-12694 Y=0 Z=9456
50 X=-11791 Y=0 Z=9456
51 X=-10888 Y=0 Z=9456
52 X=-16056.33 Y=0 Z=7131
53 X=14749 Y=0 Z=1991
54 X=-15249 Y=0 Z=7131
55 X=14749 Y=0 Z=2911
56 X=-4566 Y=0 Z=9456
57 X=12694 Y=0 Z=9456
58 X=-14500 Y=0 Z=7131
59 X=-14500 Y=0 Z=9590
60 X=-14500 Y=0 Z=11236
61 X=-16056.33 Y=0 Z=8174
62 X=-12694 Y=0 Z=8174
63 X=-12694 Y=0 Z=9590
64 X=-12694 Y=0 Z=11236
65 X=-15249 Y=0 Z=8174
66 X=-10888 Y=0 Z=9000
67 X=-10888 Y=0 Z=9590
68 X=-10888 Y=0 Z=11236
69 X=-16056.33 Y=0 Z=10138.67
70 X=-9081 Y=0 Z=9456
71 X=-9081 Y=0 Z=9590
72 X=-9081 Y=0 Z=11236
73 X=-15249 Y=0 Z=10138.67
74 X=-7275 Y=0 Z=9590
75 X=-7275 Y=0 Z=11236
76 X=-16056.33 Y=0 Z=10687.33
77 X=-5469 Y=0 Z=9456
78 X=-5469 Y=0 Z=9590
79 X=-5469 Y=0 Z=11236
80 X=-15249 Y=0 Z=10687.33

81 X=-3663 Y=0 Z=9000
82 X=-3663 Y=0 Z=9590
83 X=-3663 Y=0 Z=11236
84 X=-16056.33 Y=0 Z=11236
85 X=-1856 Y=0 Z=8174
86 X=-1856 Y=0 Z=9590
87 X=-1856 Y=0 Z=11236
88 X=-15249 Y=0 Z=11236
89 X=0 Y=0 Z=7107
90 X=0 Y=0 Z=9590
91 X=0 Y=0 Z=11236
92 X=15249 Y=0 Z=9000
93 X=1856 Y=0 Z=8174
94 X=1856 Y=0 Z=9590
95 X=1856 Y=0 Z=11236
96 X=15249 Y=0 Z=9456
97 X=3663 Y=0 Z=9000
98 X=3663 Y=0 Z=9590
99 X=3663 Y=0 Z=11236
100 X=16096.33 Y=0 Z=9000
101 X=5469 Y=0 Z=9456
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104 X=16096.33 Y=0 Z=9456
105 X=7275 Y=0 Z=9590
106 X=7275 Y=0 Z=11236
107 X=15249 Y=0 Z=0
108 X=9081 Y=0 Z=9456
109 X=9081 Y=0 Z=9590
110 X=9081 Y=0 Z=11236
111 X=15249 Y=0 Z=1071
112 X=10888 Y=0 Z=9000
113 X=10888 Y=0 Z=9590
114 X=10888 Y=0 Z=11236
115 X=16096.33 Y=0 Z=0
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117 X=12694 Y=0 Z=9590
118 X=12694 Y=0 Z=11236
119 X=16096.33 Y=0 Z=1071
120 X=13597 Y=0 Z=9456
121 X=15249 Y=0 Z=1991
122 X=14500 Y=0 Z=7131
123 X=14500 Y=0 Z=9590
124 X=14500 Y=0 Z=11236
125 X=16096.33 Y=0 Z=1991
126 X=-11791 Y=0 Z=9000
127 X=15249 Y=0 Z=2911
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129 X=15249 Y=0 Z=3831
130 X=16096.33 Y=0 Z=3831
131 X=15249 Y=0 Z=9590
132 X=16096.33 Y=0 Z=9590
133 X=-14749 Y=0 Z=9000
134 X=-14500 Y=0 Z=9000
135 X=-13597 Y=0 Z=9000
136 X=-12694 Y=0 Z=9000
137 X=-2759 Y=0 Z=9000
138 X=-1856 Y=0 Z=9000
139 X=-953 Y=0 Z=9000
140 X=0 Y=0 Z=9000
141 X=953 Y=0 Z=9000
142 X=1856 Y=0 Z=9000
143 X=2759 Y=0 Z=9000
144 X=14749 Y=0 Z=9000
145 X=14500 Y=0 Z=9000
146 X=15249 Y=0 Z=7131
147 X=15249 Y=0 Z=8174
148 X=16096.33 Y=0 Z=7131
149 X=16096.33 Y=0 Z=8174
150 X=15249 Y=0 Z=4656
151 X=16096.33 Y=0 Z=4656
152 X=15249 Y=0 Z=5481
153 X=16096.33 Y=0 Z=5481
154 X=15249 Y=0 Z=6306
155 X=16096.33 Y=0 Z=6306
156 X=15249 Y=0 Z=10138.68
157 X=-14749 Y=0 Z=3831
158 X=16096.33 Y=0 Z=10138.69
159 X=15249 Y=0 Z=10687.32
160 X=-14500 Y=0 Z=3831
161 X=11791 Y=0 Z=9000
162 X=14749 Y=0 Z=8174
163 X=12694 Y=0 Z=9000
164 X=13597 Y=0 Z=9000
165 X=-9984 Y=0 Z=9456
166 X=14500 Y=0 Z=8174
167 X=16096.33 Y=0 Z=10687.31
168 X=15249 Y=0 Z=11236
169 X=16096.33 Y=0 Z=11236
170 X=-953 Y=0 Z=8174

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172 X=0 Y=0 Z=8174
173 X=953 Y=0 Z=8174
176 X=13597 Y=0 Z=8174
177 X=12694 Y=0 Z=9392
180 X=14749 Y=0 Z=3831
181 X=14500 Y=0 Z=3831
183 X=0 Y=0 Z=295
184 X=0 Y=0 Z=3831
187 X=0 Y=0 Z=4805
188 X=0 Y=0 Z=1603.5
195 X=-13597 Y=0 Z=7651
196 X=-13597 Y=0 Z=9590
197 X=-13597 Y=0 Z=11236
199 X=-11791 Y=0 Z=8638
200 X=-11791 Y=0 Z=9590
201 X=-11791 Y=0 Z=11236
203 X=-9984 Y=0 Z=9270
204 X=-9984 Y=0 Z=9590
205 X=-9984 Y=0 Z=11236
207 X=-8178 Y=0 Z=9562
208 X=-8178 Y=0 Z=9590
209 X=-8178 Y=0 Z=11236
211 X=-6372 Y=0 Z=9562
212 X=-6372 Y=0 Z=9590
213 X=-6372 Y=0 Z=11236
215 X=-4566 Y=0 Z=9270
216 X=-4566 Y=0 Z=9590
217 X=-4566 Y=0 Z=11236
219 X=-2759 Y=0 Z=8638
220 X=-2759 Y=0 Z=9590
221 X=-2759 Y=0 Z=11236
223 X=-953 Y=0 Z=7651
224 X=-953 Y=0 Z=9590
225 X=-953 Y=0 Z=11236
227 X=953 Y=0 Z=7651
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229 X=953 Y=0 Z=11236
231 X=2759 Y=0 Z=8638
232 X=2759 Y=0 Z=9590
233 X=2759 Y=0 Z=11236
235 X=4566 Y=0 Z=9270
236 X=4566 Y=0 Z=9590
237 X=4566 Y=0 Z=11236
239 X=6372 Y=0 Z=9562
240 X=6372 Y=0 Z=9590
241 X=6372 Y=0 Z=11236
243 X=8178 Y=0 Z=9562
244 X=8178 Y=0 Z=9590
245 X=8178 Y=0 Z=11236
247 X=9984 Y=0 Z=9270
248 X=9984 Y=0 Z=9590
249 X=9984 Y=0 Z=11236
251 X=11791 Y=0 Z=8638
252 X=11791 Y=0 Z=9590
253 X=11791 Y=0 Z=11236
255 X=13597 Y=0 Z=7651
256 X=13597 Y=0 Z=9590
257 X=13597 Y=0 Z=11236
259 X=-14749 Y=0 Z=8174
260 X=-14500 Y=0 Z=8174
261 X=-13597 Y=0 Z=8174
263 X=1856 Y=0 Z=9392
271 X=-14749 Y=0 Z=4656
272 X=-14749 Y=0 Z=5481
273 X=-14749 Y=0 Z=6306
274 X=-14500 Y=0 Z=4656
275 X=-14500 Y=0 Z=5481
276 X=-14500 Y=0 Z=6306
277 X=14749 Y=0 Z=4656
278 X=14500 Y=0 Z=4656
279 X=14749 Y=0 Z=5481
280 X=14500 Y=0 Z=5481
281 X=14749 Y=0 Z=6306
282 X=14500 Y=0 Z=6306
333 X=16770 Y=0 Z=9000
334 X=16770 Y=0 Z=9456
340 X=-16710 Y=0 Z=889
342 X=-16710 Y=0 Z=1991
344 X=-16710 Y=0 Z=2911
346 X=-16710 Y=0 Z=3831
349 X=-16710 Y=0 Z=9456
350 X=-16710 Y=0 Z=9590
351 X=16770 Y=0 Z=0
352 X=16770 Y=0 Z=1071
355 X=16770 Y=0 Z=1991
357 X=16770 Y=0 Z=2911
359 X=16770 Y=0 Z=3831
361 X=16770 Y=0 Z=9590
364 X=-16710 Y=0 Z=4656
366 X=-16710 Y=0 Z=5481

```

```

368 X=-16710 Y=0 Z=6306
370 X=-16710 Y=0 Z=9000
372 X=-16710 Y=0 Z=7131
373 X=16770 Y=0 Z=7131
374 X=16770 Y=0 Z=8174
378 X=-16710 Y=0 Z=8174
379 X=16770 Y=0 Z=4656
381 X=16770 Y=0 Z=5481
383 X=16770 Y=0 Z=6306
386 X=-16710 Y=0 Z=10138.67
388 X=-16710 Y=0 Z=10687.33
390 X=-16710 Y=0 Z=11236
391 X=16770 Y=0 Z=10138.7
393 X=16770 Y=0 Z=10687.3
395 X=16770 Y=0 Z=11236
469 X=-14500 Y=0 Z=10138.67
470 X=-14749 Y=0 Z=10138.67
471 X=-14500 Y=0 Z=10687.33
472 X=-14749 Y=0 Z=10687.33
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474 X=14500 Y=0 Z=10138.67
475 X=14749 Y=0 Z=10687.33
476 X=14500 Y=0 Z=10687.33
481 X=-13597 Y=0 Z=10138.67
482 X=-13597 Y=0 Z=10687.33
483 X=-12694 Y=0 Z=10138.67
484 X=-12694 Y=0 Z=10687.33
485 X=-11791 Y=0 Z=10138.67
486 X=-11791 Y=0 Z=10687.33
487 X=-10888 Y=0 Z=10138.67
488 X=-10888 Y=0 Z=10687.33
489 X=-9984 Y=0 Z=10138.67
490 X=-9984 Y=0 Z=10687.33
491 X=-9081 Y=0 Z=10138.67
492 X=-9081 Y=0 Z=10687.33
493 X=-8178 Y=0 Z=10138.67
494 X=-8178 Y=0 Z=10687.33
495 X=-7275 Y=0 Z=10138.67
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501 X=-4566 Y=0 Z=10138.67
502 X=-4566 Y=0 Z=10687.33
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504 X=-3663 Y=0 Z=10687.33
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506 X=-2759 Y=0 Z=10687.33
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508 X=-1856 Y=0 Z=10687.33
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510 X=-953 Y=0 Z=10687.33
511 X=0 Y=0 Z=10138.67
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514 X=953 Y=0 Z=10687.33
515 X=1856 Y=0 Z=10138.67
516 X=1856 Y=0 Z=10687.33
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520 X=3663 Y=0 Z=10687.33
521 X=4566 Y=0 Z=10138.67
522 X=4566 Y=0 Z=10687.33
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524 X=5469 Y=0 Z=10687.33
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526 X=6372 Y=0 Z=10687.33
527 X=7275 Y=0 Z=10138.67
528 X=7275 Y=0 Z=10687.33
529 X=8178 Y=0 Z=10138.67
530 X=8178 Y=0 Z=10687.33
531 X=9081 Y=0 Z=10138.67
532 X=9081 Y=0 Z=10687.33
533 X=9984 Y=0 Z=10138.67
534 X=9984 Y=0 Z=10687.33
535 X=10888 Y=0 Z=10138.67
536 X=10888 Y=0 Z=10687.33
541 X=11791 Y=0 Z=10138.67
542 X=11791 Y=0 Z=10687.33
543 X=12694 Y=0 Z=10138.67
544 X=12694 Y=0 Z=10687.33
545 X=13597 Y=0 Z=10138.67
546 X=13597 Y=0 Z=10687.33

```

RESTRAINT

```

ADD=16 DOF=U1, U2, U3, R1, R2, R3
ADD=19 DOF=U1, U2, U3, R1, R2, R3
ADD=31 DOF=U1, U2, U3, R1, R2, R3

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ADD=39 DOF=U1,U2,U3,R1,R2,R3
ADD=48 DOF=U1,U2,U3,R1,R2,R3
ADD=53 DOF=U1,U2,U3,R1,R2,R3
ADD=55 DOF=U1,U2,U3,R1,R2,R3
ADD=58 DOF=U2,R1,R3
ADD=62 DOF=U2,R1,R3
ADD=66 DOF=U2,R1,R3
ADD=70 DOF=U2,R1,R3
ADD=74 DOF=U2,R1,R3
ADD=77 DOF=U2,R1,R3
ADD=81 DOF=U2,R1,R3
ADD=85 DOF=U2,R1,R3
ADD=89 DOF=U2,R1,R3
ADD=93 DOF=U2,R1,R3
ADD=97 DOF=U2,R1,R3
ADD=101 DOF=U2,R1,R3
ADD=105 DOF=U2,R1,R3
ADD=107 DOF=U1,U2,U3,R1,R2,R3
ADD=108 DOF=U2,R1,R3
ADD=111 DOF=U1,U2,U3,R1,R2,R3
ADD=112 DOF=U2,R1,R3
ADD=116 DOF=U2,R1,R3
ADD=122 DOF=U2,R1,R3
ADD=157 DOF=U1,U2,U3,R1,R2,R3
ADD=160 DOF=U2,R1,R3
ADD=180 DOF=U1,U2,U3,R1,R2,R3
ADD=181 DOF=U2,R1,R3
ADD=183 DOF=U1,U2,U3,R1,R2,R3
ADD=195 DOF=U2,R1,R3
ADD=199 DOF=U2,R1,R3
ADD=203 DOF=U2,R1,R3
ADD=207 DOF=U2,R1,R3
ADD=211 DOF=U2,R1,R3
ADD=215 DOF=U2,R1,R3
ADD=219 DOF=U2,R1,R3
ADD=223 DOF=U2,R1,R3
ADD=227 DOF=U2,R1,R3
ADD=231 DOF=U2,R1,R3
ADD=235 DOF=U2,R1,R3
ADD=239 DOF=U2,R1,R3
ADD=243 DOF=U2,R1,R3
ADD=247 DOF=U2,R1,R3
ADD=251 DOF=U2,R1,R3
ADD=255 DOF=U2,R1,R3
ADD=274 DOF=U2,R1,R3
ADD=275 DOF=U2,R1,R3
ADD=276 DOF=U2,R1,R3
ADD=278 DOF=U2,R1,R3
ADD=280 DOF=U2,R1,R3
ADD=282 DOF=U2,R1,R3

PATTERN

NAME=EARTH
ADD=1 V=2.623107
ADD=2 V=2.623107
ADD=3 V=2.623107
ADD=4 V=2.623107
ADD=5 V=2.623107
ADD=6 V=2.623107
ADD=7 V=2.623107
ADD=8 V=2.623107
ADD=9 V=2.623107
ADD=10 V=2.623107
ADD=11 V=2.623107
ADD=12 V=2.623107
ADD=13 V=2.623107
ADD=14 V=15.27057
ADD=15 V=13.64369
ADD=16 V=15.27057
ADD=17 V=2.623107
ADD=18 V=2.623107
ADD=19 V=13.64369
ADD=20 V=12.28549
ADD=21 V=6.055505
ADD=22 V=12.28549
ADD=23 V=10.92729
ADD=24 V=2.425283
ADD=26 V=10.92729
ADD=27 V=-.0047068
ADD=28 V=2.623107
ADD=29 V=2.425283
ADD=30 V=2.623107
ADD=31 V=13.64369
ADD=32 V=2.425283
ADD=33 V=9.709347
ADD=34 V=2.623107
ADD=35 V=2.623107
ADD=36 V=2.623107
ADD=37 V=6.055505
ADD=38 V=9.709347

ADD=39 V=12.28549
ADD=40 V=2.425283
ADD=41 V=8.4914
ADD=42 V=8.4914
ADD=43 V=-.0047068
ADD=44 V=7.273452
ADD=45 V=7.273452
ADD=46 V=3.2963
ADD=47 V=3.2963
ADD=48 V=15.00188
ADD=49 V=2.623107
ADD=50 V=2.623107
ADD=51 V=2.623107
ADD=52 V=6.055505
ADD=53 V=13.64369
ADD=54 V=6.055505
ADD=55 V=12.28549
ADD=56 V=2.623107
ADD=57 V=2.623107
ADD=58 V=6.055505
ADD=59 V=2.425283
ADD=60 V=-.0047068
ADD=61 V=4.515724
ADD=62 V=4.515724
ADD=63 V=2.425283
ADD=64 V=-.0047068
ADD=65 V=4.515724
ADD=66 V=3.2963
ADD=67 V=2.425283
ADD=68 V=-.0047068
ADD=69 V=1.615281
ADD=70 V=2.623107
ADD=71 V=2.425283
ADD=72 V=-.0047068
ADD=73 V=1.615281
ADD=74 V=2.425283
ADD=75 V=-.0047068
ADD=76 V=.8052947
ADD=77 V=2.623107
ADD=78 V=2.425283
ADD=79 V=-.0047068
ADD=80 V=.8052947
ADD=81 V=3.2963
ADD=82 V=2.425283
ADD=83 V=-.0047068
ADD=84 V=-.0047068
ADD=85 V=4.515724
ADD=86 V=2.425283
ADD=87 V=-.0047068
ADD=88 V=-.0047068
ADD=89 V=6.090936
ADD=90 V=2.425283
ADD=91 V=-.0047068
ADD=92 V=3.2963
ADD=93 V=4.515724
ADD=94 V=2.425283
ADD=95 V=-.0047068
ADD=96 V=2.623107
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ADD=98 V=2.425283
ADD=99 V=-.0047068
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ADD=102 V=2.425283
ADD=103 V=-.0047068
ADD=104 V=2.623107
ADD=105 V=2.425283
ADD=106 V=-.0047068
ADD=107 V=16.583
ADD=108 V=2.623107
ADD=109 V=2.425283
ADD=110 V=-.0047068
ADD=111 V=15.00188
ADD=112 V=3.2963
ADD=113 V=2.425283
ADD=114 V=-.0047068
ADD=115 V=16.583
ADD=116 V=4.515724
ADD=117 V=2.425283
ADD=118 V=-.0047068
ADD=119 V=15.00188
ADD=120 V=2.623107
ADD=121 V=13.64369
ADD=122 V=6.055505
ADD=123 V=2.425283
ADD=124 V=-.0047068
ADD=125 V=13.64369
ADD=126 V=3.2963
ADD=127 V=12.28549
ADD=128 V=12.28549

ADD=129 V=10.92729
ADD=130 V=10.92729
ADD=131 V=2.425283
ADD=132 V=2.425283
ADD=133 V=3.2963
ADD=134 V=3.2963
ADD=135 V=3.2963
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ADD=146 V=6.055505
ADD=147 V=4.515724
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ADD=150 V=9.709347
ADD=151 V=9.709347
ADD=152 V=8.4914
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NAME=STEEL IDES=S M=7.98142E-13
W=7.833414E-09
T=0 E=20.38902 U=.3 A=.0000117
FY=2.531051E-02
NAME=CONC IDES=C M=2.448E-13 W=2.4026E-09
T=0 E=2.46475 U=.2 A=.0000099

FRAME SECTION

NAME=1 MAT=CONC WPL=.0025 SH=R T=500,1000
A=500000 J=2.861003E+10
I=1.041667E+10,4.166667E+10 AS=416666.7,416666.7
NAME=2 MAT=CONC WPL=.0025 SH=R T=500,1000
A=500000 J=2.861003E+10
I=1.041667E+10,4.166667E+10 AS=416666.7,416666.7
NAME=3 MAT=CONC WPL=.0025 SH=R T=1000,1000
A=1000000 J=1.408333E+11
I=8.333334E+10,8.333334E+10 AS=833333.3,833333.3
NAME=4 MAT=CONC SH=R T=1300,1000 A=1300000
J=2.294606E+11 I=1.830833E+11,1.083333E+11
AS=1083333,1083333

SHELL SECTION

NAME=1 MAT=CONC TYPE=Shell,Thick TH=850
THB=1000

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31 J=275,276 SEC=1 NSEG=4 ANG=180
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46 J=89,187 SEC=3 NSEG=4 ANG=0

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48 J=184,188 SEC=4 NSEG=4 ANG=0

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ELEM=SHELL TYPE=STRESS COMB=2

END

; The following data is used for graphics, design
and pushover analysis.
; If changes are made to the analysis data above,
then the following data
; should be checked for consistency.

SAP2000 V7.10 SUPPLEMENTAL DATA

GRID GLOBAL X "1" -12950
GRID GLOBAL Y "2" 0
GRID GLOBAL Z "3" 0
GRID GLOBAL X "4" 0
GRID GLOBAL X "5" 12950
GRID GLOBAL Z "6" 9739
MATERIAL STEEL FY 2.531051E-02
MATERIAL CONC FYREBAR 4.218418E-02 FYSHEAR
2.812279E-02 FC 2.812279E-03 FCSHEAR 2.812279E-03
CONCRETESECTION 1 COLUMN COVER 100 REBAR
RR-3-3
CONCRETESECTION 2 COLUMN COVER 206.2 REBAR
RR-3-3
CONCRETESECTION 3 COLUMN COVER 150 REBAR
RR-3-3
CONCRETESECTION 4 COLUMN COVER 140 REBAR
RR-3-3
STATICLOAD 1 TYPE DEAD
STATICLOAD 2 TYPE DEAD
END SUPPLEMENTAL DATA

; File D:\SAP2000DATA\개작식터널\설치.\$2k saved
9-14-02 14:26:33 in Ton-mm

SYSTEM

DOF=UX,UZ LENGTH=mm FORCE=Ton LINES=59

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RESTRAINT

ADD=400 DOP=U1,U2,U3,R1,R2,R3

PATTERN

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NAME=PRES

MATERIAL

NAME=STEEL IDES=S M=7.981E-13
T=0 E=20.38902 U=.3 A=.0000117
FY=2.531051E-02
NAME=CONC IDES=C M=2.448E-13 W=2.5E-09
T=0 E=3 U=.2 A=.0000099

FRAME SECTION

NAME=FSEC1 MAT=CONC SH=R T=500,300 A=672500
J=2.817371E+09 I=3.125E+09,1.125E+09
AS=125000,125000
NAME=CABLE MAT=STEEL SH=P T=30,14 A=703.7167
J=79519.99 I=39759.99,39759.99
AS=614.5792,614.5792

FRAME

1 J=400,125 SEC=CABLE NSEG=2 ANG=-44.34524
IREL=R2,R3

2 J=400,225 SEC=CABLE NSEG=2 ANG=44.34524
IREL=R2,R3
3 J=400,158 SEC=CABLE NSEG=2 ANG=-73.48468
IREL=R2,R3
4 J=400,258 SEC=CABLE NSEG=2 ANG=73.48468
IREL=R2,R3

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OUTPUT
; No Output Requested
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END
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; The following data is used for graphics, design
and pushover analysis.
; If changes are made to the analysis data above,
then the following data
; should be checked for consistency.
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SAP2000 V7.10 SUPPLEMENTAL DATA
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GRID GLOBAL X "3" 2790
GRID GLOBAL Y "4" -1200
GRID GLOBAL Y "5" -819
GRID GLOBAL Y "6" -381
GRID GLOBAL Y "7" 0
GRID GLOBAL Z "8" 0
GRID GLOBAL Z "9" 1200
MATERIAL STEEL FY 2.531051E-02
MATERIAL CONC FYREBAR .04 FYSHEAR 2.812279E-02
FC .004 FCSHEAR 2.812279E-03
CONCRETESECTION FSEC1 COLUMN COVER 50 REBAR
RR-3-3
STATICLOAD LOAD1 TYPE DEAD
END SUPPLEMENTAL DATA
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; File D:\SAP2000DATA\개착식터널\인양.\$2k saved
9-27-02 9:12:46 in Kgf-cm

SYSTEM

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T=0 E=2038902 U=.3 A=.0000117 FY=2531.051
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OUTPUT
; No Output Requested

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END

; The following data is used for graphics, design and pushover analysis.
; If changes are made to the analysis data above, then the following data
; should be checked for consistency.

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SAP2000 V7.10 SUPPLEMENTAL DATA
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GRID GLOBAL X "2" 0
GRID GLOBAL X "3" 279
GRID GLOBAL Y "4" -120
GRID GLOBAL Y "5" -81.9
GRID GLOBAL Y "6" -38.1
GRID GLOBAL Y "7" 0
GRID GLOBAL Z "8" 0
GRID GLOBAL Z "9" 120
MATERIAL STEEL FY 2531.051
MATERIAL CONC FYREBAR 4000 FYSHEAR 2812.279 FC
400 FCSHEAR 281.2279
CONCRETESECTION FSEC1 COLUMN COVER 5 REBAR
RR-3-3
STATICLOAD LOAD1 TYPE DEAD
END SUPPLEMENTAL DATA

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